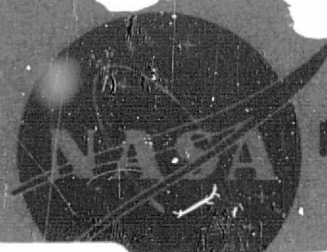


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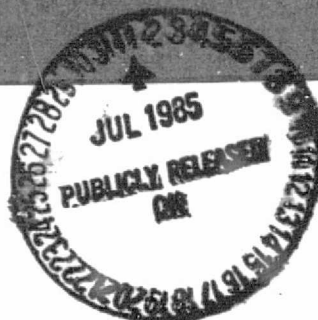
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ADDITION OF FLEXIBLE BODY OPTION TO THE TOLA COMPUTER PROGRAM

Part I - Final Report

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Prepared by

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ABSTRACT

This report describes a flexible body option that was developed and added to the Takeoff and Landing Analysis (TOLA) computer program. The addition of the flexible body option to TOLA allows it to be used to study essentially any conventional type airplane in the ground operating environment. It provides the capability to predict the total motion of selected points on an aircraft including the effects of the elastic motion of the airplane. The analytical methods incorporated in the program and operating instructions for the option are described. A program listing is included along with several example problems to aid in interpretation of the operating instructions and to illustrate program usage.

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1. INTRODUCTION

This report describes the flexible body option of the airplane Takeoff and Landing Analysis (TOLA) computer program. This option was developed by McDonnell Douglas Astronautics Company-East under NASA Contract NAS1-13259 for investigation of aircraft response in a ground operating environment. The response data provided can be used for evaluation of structural fatigue life, ground handling characteristics, passenger comfort and vehicle loads.

The original TOLA computer program was developed by Air Force Flight Dynamics Laboratory personnel and is described in References (1) through (4). This formulation provides a complete simulation of the aircraft takeoff and landing problem. Effects simulated include aircraft control and performance during glide slope, flare, landing roll and takeoff roll for an aircraft with a rigid airframe.

The flexible body option added to TOLA provides the additional capability to predict the total motion of desired points on the aircraft including the effects of the elastic motion of the airframe in the ground operating environment. A block diagram of the TOLA computer program with the flexible body option is shown in Figure 1-1.

This report describes: the analytical methods used to formulate the flexible body effects; the changes and additions made to the TOLA computer program; the use of the revised program; and the check cases run to verify program results.

User's and programmer's documentation (Reference 5) provides additional information about the TOLA program flexible body option.

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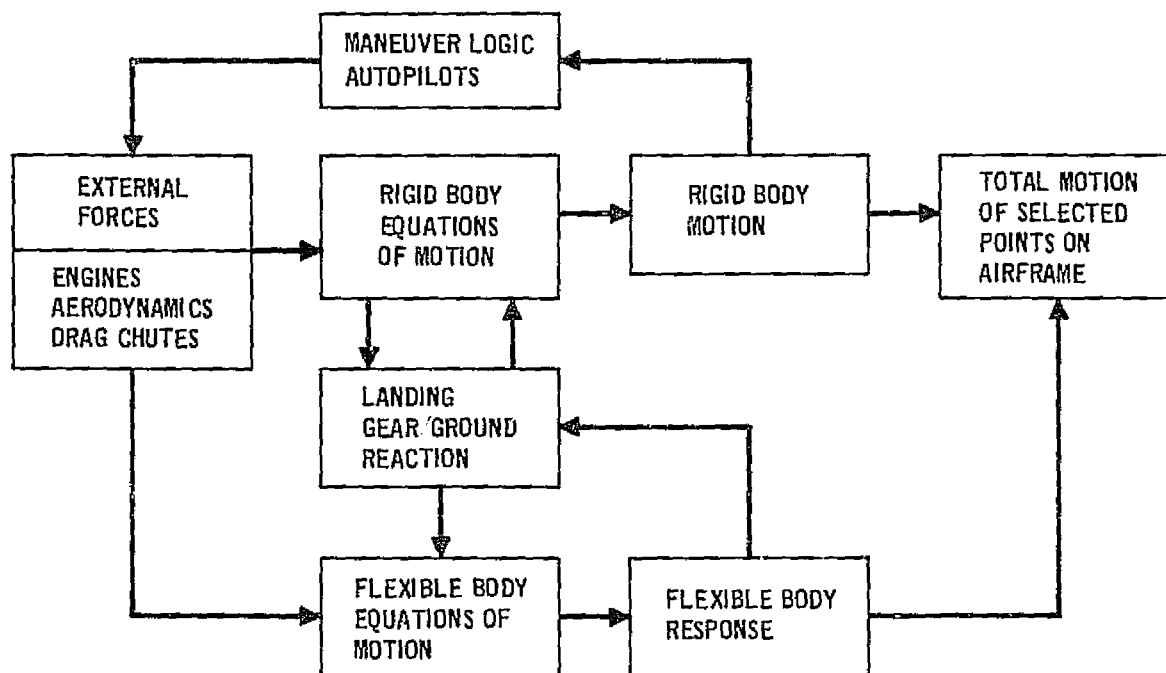


FIGURE 1-1 BLOCK DIAGRAM OF TOLA COMPUTER PROGRAM
WITH FLEXIBLE BODY OPTION

2. FLEXIBLE BODY OPTION CAPABILITIES

The TOLA computer program permits a comprehensive simulation of the airplane takeoff and landing problem. The addition of the flexible body option to TOLA allows it to be used to study essentially any type of aircraft in the ground operating environment. TOLA's capabilities, assuming a rigid aircraft, are discussed in detail in Reference (4). All of those capabilities are retained in the modified version of TOLA. For the sake of completeness, most of them are repeated in the description of the flexible body option below.

2.1 Aircraft Simulation - The flexible body option version of TOLA can simulate an aircraft with up to four engines and a maximum of five landing gears. The airframe, defined as the airplane minus its landing gears, may be idealized as either a rigid body or a flexible body. Basically, this modified version of TOLA has two options; a rigid airframe option and a flexible airframe option. In the flexible airframe option, the flexibility is represented by the superposition of free-free vibratory modes on the rigid body motion. From one to twenty modes may be included to represent the airframe flexibility. These modal data must be input to the program. Airframe time history data printed out include 1) rigid body displacements, velocities and accelerations at the center of mass; 2) elastic body displacements, velocities and accelerations at up to 20 points on the airframe; and 3) total (rigid body plus elastic body) velocities and accelerations at these same points.

The dynamic effects of a maximum of five independent landing gears are simulated. The landing gear idealized, shown in Figure 2-1, is a double air chamber oleo strut with balloon tires, similar to that used on the C-5A aircraft; the secondary piston and air chamber can be eliminated from the problem, if desired. Each of the struts must lie in a plane parallel to the aircraft plane of symmetry, but the strut axis may be nonperpendicular to the longitudinal aircraft axis. The position and velocity of each strut and secondary piston are obtained by numerical integration subject to position constraints (for example, the main strut must move within the limits of the fully extended position and strut bottom position). Orifice coefficients can depend on the direction of oil flow through the orifice. Wing-gear root

friction (i.e., binding friction between moving strut and its support at the wing) is also included. Tire forces depend upon tire deflection and a coefficient of friction which is a function of "percent skid", the ratio of tire footprint velocity to axle velocity. The simulation is designed to consider that the gears may bounce off and back onto the runway. Complete information on the dynamic state of the landing gears is printed out by TOLA.

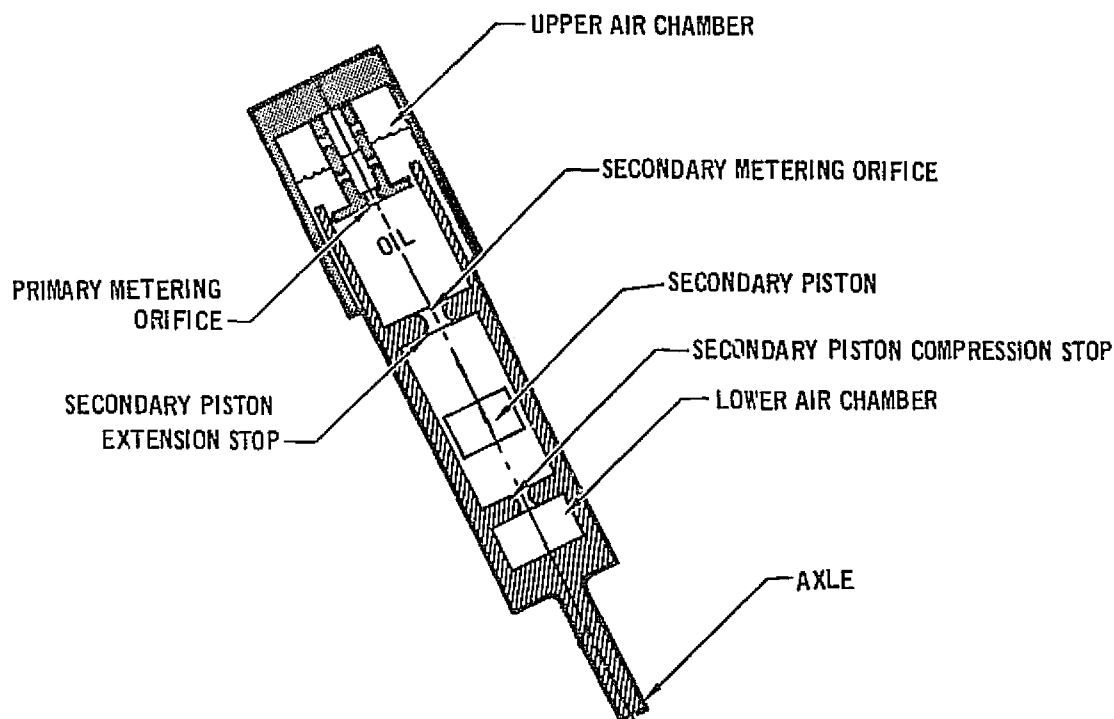


FIGURE 2-1 LANDING GEAR STRUT CONFIGURATION

The simulated aircraft, as represented by the airframe rigid and flexible body equations of motion and the strut, strut secondary piston and wheel equations of motion, may be subjected to time varying forces, ground reactions and maneuver commands.

Forces in the problem simulation include engine thrust, aerodynamics including ground effects, drag chute forces, landing gear tire-ground reaction and braking forces. These forces may be varied and/or staged within the aircraft's capability by the maneuver logic and autopilot simulations discussed in the next section.

2.2 Autopilot Simulation - The function of the autopilot is to specify the aircraft's control variable magnitudes that result in the required aircraft performance during glide slope, flare, landing roll, and takeoff roll. The autopilot simulation is described in detail in Reference (2). Since the capabilities of the autopilot are not changed in the flexible body option of TOLA, they will be only summarized here.

Figure 2-2 shows a simplified block diagram of the autopilot simulation. The maneuver logic utilizes information on the state of the aircraft obtained from solution of the airplane equations of motion to compute state errors. If necessary, it defines a corrective maneuver by specifying, for example, angle of attack, roll angle, thrust levels, and braking values. The maneuver logic also specifies the staging of events such as spoiler activation, kill power, engine failure, thrust reversal, drag chute deployment, brake activation and brake failure.

The maneuver logic output is used by the pitch, yaw, roll, throttle and braking autopilot to determine desired values of the control variables. These values, after adjustment for simulated control system lags, become the actual control variable magnitudes that determine the aircraft response. Complete information on the state of the maneuver logic, the five autopilots and the control response are printed.

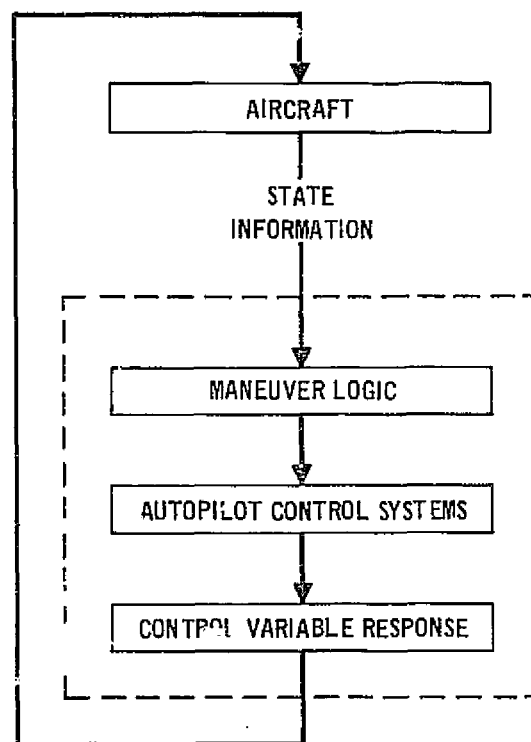


FIGURE 2-2 AUTOPILOT SIMULATION

3. FLEXIBLE BODY OPTION

The flexible body option version of TOLA provides the capability to predict the total motion of an aircraft including airframe elastic effects and landing gear dynamics. It can simulate an aircraft with up to five landing gears and four engines considering the airframe to be either rigid or flexible. The analytical methods used to develop the computer program are presented in Section 3.1. Organization of the computer program is presented in Section 3.2, operating instructions in Section 3.3 and demonstration and verification problems are presented in Section 3.4. A listing of the program is given in Appendix A.

3.1 Analytical Methods - Analytical methods used to develop the TOLA flexible body option are presented below. Included are discussions of coordinate systems, equations of motion, and simplifying assumptions.

3.1.1 Coordinate Systems - Four types of coordinate systems, as shown in Figure 3-1, are used to locate the aircraft as a function of time. These consist of two coordinate systems fixed relative to the earth, and two systems moving with the airplane. These right-handed, orthogonal axes systems are defined as follows:

Inertial Coordinate System (X_g, Y_g, Z_g) - This is a coordinate system fixed relative to the earth's local acceleration of gravity vector. The Z_g axis is directed along the local gravitational vector with the X_g and Y_g axes perpendicular to it.

Runway Coordinate System (X_R, Y_R, Z_R) - This is an earth fixed coordinate system located a distance R_{gR} along the X_g axis. Y_R is parallel to Y_g and the runway has an elevation angle, E_R , relative to the X_g axis. The runway length is R_L .

Body Coordinate System (X_o, Y_o, Z_o) - This is a coordinate system moving with the airplane and fixed at the center of mass. The mass center is located Y_o is positive outboard in the right wing direction and Z_o is positive downward. The airplane's angular positions are defined in terms of the three Euler angles Ψ , Θ , and ϕ . Definition of the aircraft's angular position relative to the inertial axes system is based on a specific order for the Euler angle rotations. The order required for these rotations consists of an initial rotation, Ψ , about the Z_g axis, followed by a rotation, Θ , about the displaced Y_g axis and finally by a rotation, ϕ , about the direction of the

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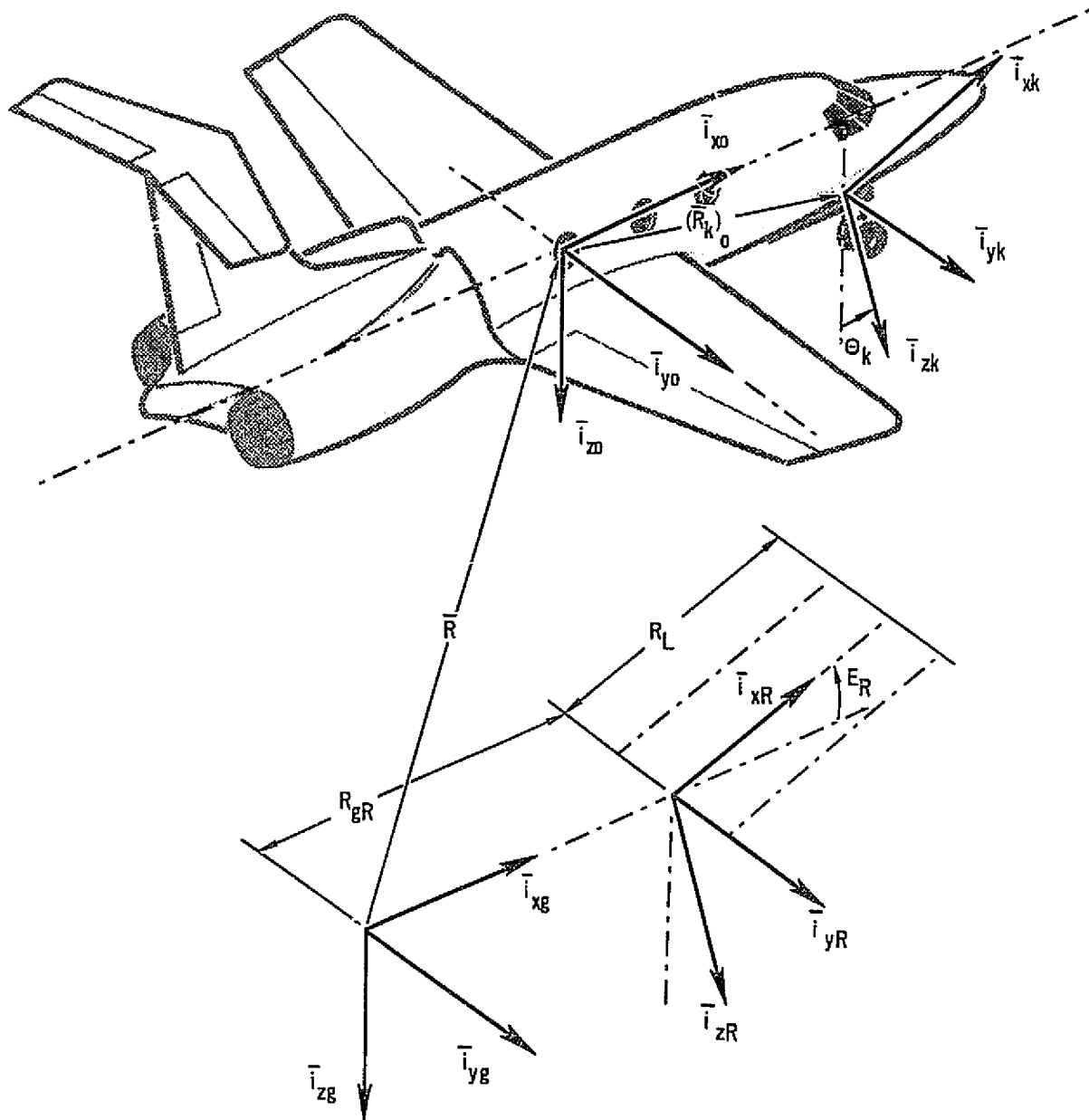


FIGURE 3-1 COORDINATE SYSTEMS

displaced X_0 axis resulting from the two previous rotations. When all three of the Euler angles are zero, the airplane or body coordinate system is aligned with the inertial coordinate system.

Strut Coordinate Systems (X_k, Y_k, Z_k) - These are coordinate systems moving with the airplane and located relative to the body coordinate system by the vector $(\bar{R}_k)_0$. Y_k is parallel to Y_0 . Z_k and X_k are rotated about the positive Y_0 axis by the angle θ_k such that the direction of gear movement is along the Z_k direction.

The runway coordinate system is related to the inertial coordinate system by the following relationships:

$$\begin{pmatrix} X_R \\ Y_R \\ Z_R \end{pmatrix} = \begin{bmatrix} R_{G11} & 0 & R_{G13} \\ 0 & 1 & 0 \\ R_{G31} & 0 & R_{G33} \end{bmatrix} \begin{pmatrix} X_g \\ Y_g \\ Z_g \end{pmatrix} \quad (3-1)$$

where $R_{G11} = \cos E_R$

$R_{G13} = -\sin E_R$

$R_{G31} = \sin E_R$

$R_{G33} = \cos E_R$

The body coordinate system is related to the inertial coordinate system by the following relationships:

$$\begin{pmatrix} X_0 \\ Y_0 \\ Z_0 \end{pmatrix} = \begin{bmatrix} l_1 & l_2 & l_3 \\ m_1 & m_2 & m_3 \\ n_1 & n_2 & n_3 \end{bmatrix} \begin{pmatrix} X_g \\ Y_g \\ Z_g \end{pmatrix} \quad (3-2)$$

where $l_1 = \cos \theta \cos \psi$

$l_2 = \cos \theta \sin \psi$

$l_3 = -\sin \theta$

$m_1 = \sin \phi \sin \theta \cos \psi - \cos \phi \sin \psi$

$m_2 = \sin \phi \sin \theta \cos \psi + \cos \phi \cos \psi$

$m_3 = \sin \phi \cos \theta$

$$\begin{aligned}
n_1 &= \cos \phi \sin \Theta \cos \Psi + \sin \phi \sin \Psi \\
n_2 &= \cos \phi \sin \Theta \sin \Psi - \sin \phi \cos \Psi \\
n_3 &= \cos \phi \cos \Theta
\end{aligned}$$

The strut coordinate systems are related to the body coordinate system as follows:

$$\begin{pmatrix} X_k \\ Y_k \\ Z_k \end{pmatrix} = \begin{bmatrix} A_{k11} & 0 & A_{k13} \\ 0 & 1 & 0 \\ A_{k31} & 0 & A_{k33} \end{bmatrix} \begin{pmatrix} X_o \\ Y_o \\ Z_o \end{pmatrix} \quad (3-3)$$

where

$$\begin{aligned}
A_{k11} &= \cos \Theta_k \\
A_{k13} &= -\sin \Theta_k \\
A_{k31} &= \sin \Theta_k \\
A_{k33} &= \cos \Theta_k
\end{aligned}$$

3.1.2 Equations of Motion - The equations of motion are discussed in two parts. The equations of motion for the airplane are presented first. The second part discusses the landing gear equations which consist of the strut mass, strut secondary piston mass and the wheel equations.

3.1.2.1 Airplane Equations - The airplane rigid body and flexible body equations are developed in this section. The airplane main body is defined as the airplane less its landing gears. As such the airplane is represented by $K+1$ bodies: the aircraft main body is considered the 0^{th} body; a typical landing gear is considered the k^{th} body with K being the total number of gears. The landing gear struts are considered "rigid" in this development but allowed to move relative to the main body.

The dynamic motion of the main body is described using the normal mode method. In this method the main body motion is approximated by the combination of a limited number of vibratory modes plus the six rigid body modes. The main body's flexibility is represented by its free-free (unrestrained) vibratory modes. The rigid body modes were assumed to be the three translational displacements defining the position of the airplane's center of mass and three angular displacements defined in the body coordinate system.

In developing the airplane equations of motion, expressions defining the motion of an arbitrary point located on the landing gear and/or main body were obtained. These were used to evaluate the kinetic and potential energy of the airplane. The equations of motion were obtained by applying the Lagrangian equations to these energy expressions.

Using Figure 3-2, the total displacement of a point i is defined as

$$\bar{\rho}_{ki} = \bar{R} + (\bar{R}_k)_o + \bar{r}_{ki} \quad (3-4)$$

$\bar{\rho}_{ki}$ = position vector of point i relative to the inertial coordinate system.

\bar{R} = position vector of reference point on main or 0th body relative to inertial coordinate system.

$(\bar{R}_k)_o$ = position vector of kth body reference point relative to the body coordinate system.

\bar{r}_{ki} = position vector of point i relative to the strut or kth body coordinate system.

k = Subscript defining a specific body. The airplane minus its gears is the 0th body (k = 0). A typical landing gear is the kth body (k = 1, 2, 3...K).

Note that for k = 0, the point i is on the main or 0th body and $(\bar{R}_o)_o$ is identically zero. This gives

$$\bar{\rho}_{oi} = \bar{R} + \bar{r}_{oi} \quad (3-5)$$

\bar{r}_{oi} = position vector of point i relative to the 0th body coordinate system.

Differentiating the displacement vector given by equation (3-4) with respect to time to obtain the velocity required in the kinetic energy expression results in

$$\dot{\bar{\rho}}_{ki} = \dot{\bar{R}} + (\dot{\bar{R}}_k)_o + \bar{\omega}_o \times (\bar{R}_k)_o + \dot{\bar{r}}_{ki} + \bar{\omega}_k \times \bar{r}_{ki} \quad (3-6)$$

where $\dot{\bar{R}}$ = velocity vector of reference point on 0th body in the inertial coordinate system

$(\dot{\bar{R}}_k)_o$ = velocity vector of kth body reference point relative to 0th body coordinate system

$\bar{\omega}_o$ = angular velocity of 0th body in body coordinate system

$\dot{\bar{r}}_{ki}$ = velocity vector of point i relative to the strut coordinate system

$\bar{\omega}_k$ = angular velocity of the kth body relative to the strut coordinate system

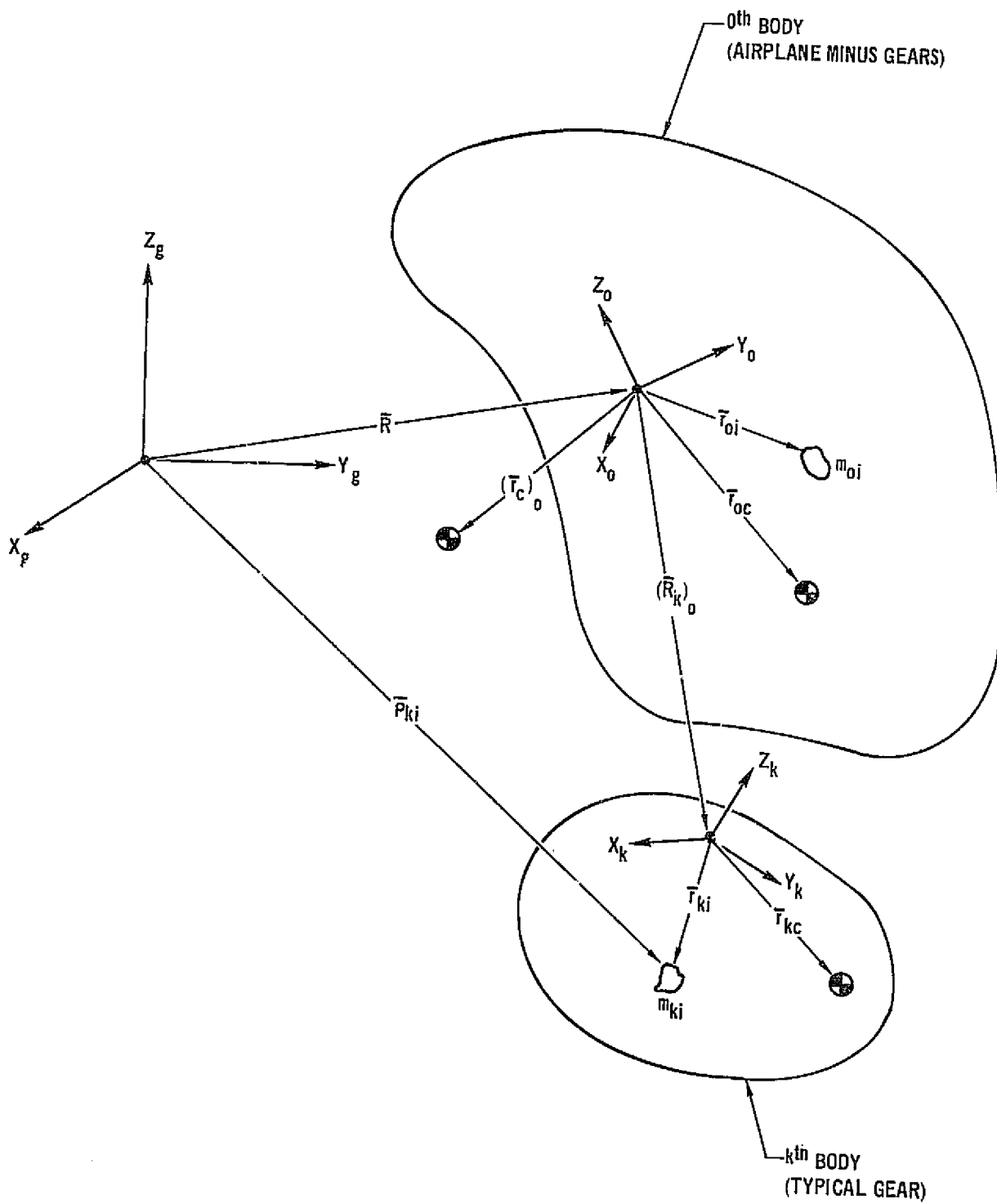


FIGURE 3-2 POSITION VECTORS

By locating the strut coordinate system reference point on the 0th body at the the strut attachment point, the angular velocities of the body and strut coordinate systems are the same. Therefore

$$\bar{\omega}_o = \bar{\omega}_k = \bar{\omega} \quad (3-7)$$

and the velocity vector may be written

$$\dot{\bar{r}}_{ki} = \dot{\bar{R}} + (\dot{\bar{R}}_k)_o + \dot{\bar{r}}_{ki} + \bar{\omega} \times [(\bar{R}_k)_o + \bar{r}_{ki}] \quad (3-8)$$

It is assumed that the position vectors $(\bar{R}_k)_o$ and \bar{r}_{ki} used to locate point i in equation (3-8) can be separated into terms which vary with time and terms which remain constant with time. Thus, these vectors may be written

$$(\bar{R}_k)_o = \bar{R}_{ks} + \bar{R}_{ke}(t) \quad (3-9)$$

$$\bar{r}_{ki} = \bar{r}_{kis} + \bar{r}_{kie}(t)$$

where \bar{R}_{ks} = undeformed position of kth body reference point in the body coordinate system

$\bar{R}_{ke}(t)$ = deformed position of kth body reference point in the body coordinate system measured from the undeformed position of that point

\bar{r}_{kis} = undeformed position of point i in the strut coordinate system.

$\bar{r}_{kie}(t)$ = deformed position of point i in the strut coordinate system measured from the undeformed position of that point

These position vectors are shown in Figure 3-3.

Since it is assumed that the elastic deformation of the airplane main body can be represented by the superposition of a limited number of vibratory modes, the terms of $(\bar{R}_k)_o$ and \bar{r}_{ki} that vary with time may be written as

$$\bar{R}_{ke}(t) = \sum_{n=1}^N \phi_n^{-k} q_n(t)$$

and for k=0

$$\bar{r}_{kie}(t) = \sum_{n=1}^N \bar{\phi}_n^i q_n(t)$$

(3-10)

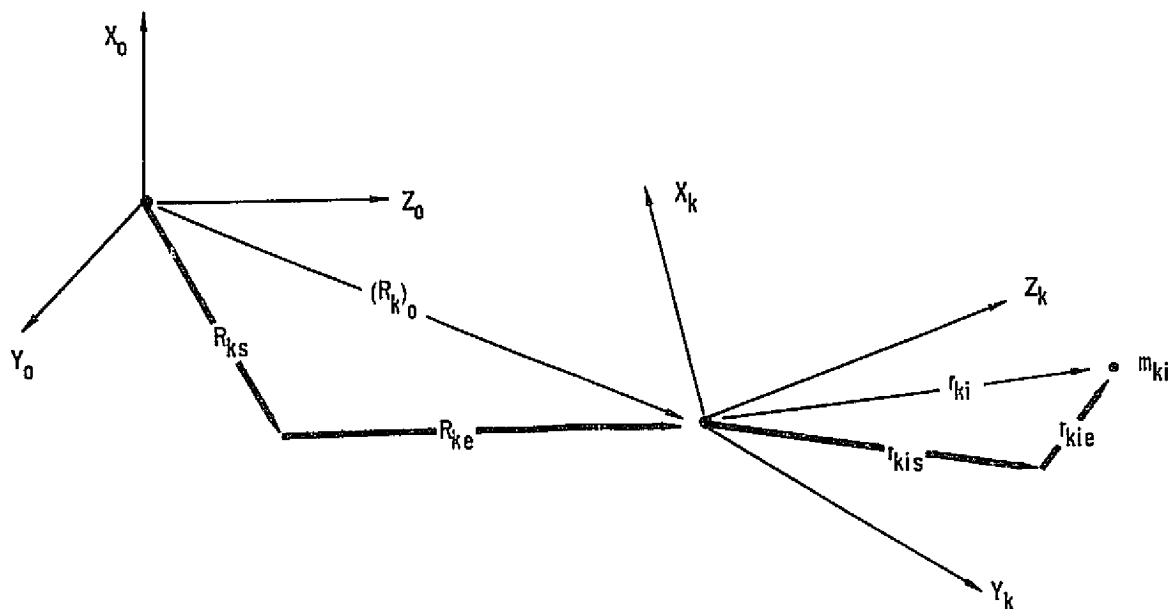


FIGURE 3-3 POSITION OF POINT I RELATIVE TO BODY COORDINATE SYSTEM

where N = number of vibratory modes included

ϕ_n^{-i}, ϕ_n^{-k} = magnitude of n^{th} elastic mode at points i and k respectively.
(k used to superscript refers to attachment point of k^{th} body ,
 $k = 1, 2, 3 \dots K$)

q_n = generalized coordinate associated with the n^{th} mode. These
are a function of time.

Using equations 3-8, 3-9 and 3-10, the velocity of point i may be written as
follows:

For point i on the k^{th} landing gear

$$\dot{\rho}_{ki} = \dot{\bar{R}} + \sum_{n=1}^N \phi_n^{-k} \dot{q}_n + \dot{\bar{r}}_{kie} + \bar{\omega} \times [\bar{R}_{ks} + \sum_{n=1}^N \phi_n^{-k} q_n + \bar{r}_{kis} + \bar{r}_{kie}] \quad (3-11)$$

For point i on the main or 0^{th} body

$$\dot{\rho}_{oi} = \dot{\bar{R}} + \sum_{n=1}^N \phi_n^{-i} \dot{q}_n + \bar{\omega} \times [\bar{r}_{ois} + \sum_{n=1}^N \phi_n^{-i} q_n] \quad (3-12)$$

The kinetic energy of the $K+1$ bodies, T , is obtained by summing the

kinetic energy of all points i in the system having a mass m_{ki}

$$T = \frac{1}{2} \sum_{k=0}^K \sum_{i=1}^I m_{ki} \dot{\rho}_{ki} \cdot \dot{\rho}_{ki} \quad (3-13)$$

where K is the total number of landing gears and I is the total number of mass points.

The 0th or elastic body kinetic energy may be separated from the strut kinetic energy to give

$$T = \frac{1}{2} \sum_{i=1}^I m_{oi} \dot{\rho}_{oi} \cdot \dot{\rho}_{oi} + \frac{1}{2} \sum_{k=1}^K \sum_{i=1}^I m_{ki} \dot{\rho}_{ki} \cdot \dot{\rho}_{ki} \quad (3-14)$$

Since the struts are considered rigid,

$$\sum_{i=1}^I m_{ki} \dot{\rho}_{ki} = m_k \dot{\rho}_{kc} \quad (3-15)$$

and the kinetic energy may be written

$$T = \frac{1}{2} \sum_{i=1}^I m_{oi} \dot{\rho}_{oi} \cdot \dot{\rho}_{oi} + \frac{1}{2} \sum_{k=1}^K m_k \dot{\rho}_{kc} \cdot \dot{\rho}_{kc} \quad (3-16)$$

In this expression m_k is the mass of the k^{th} strut and $\dot{\rho}_{kc}$, the velocity of the k^{th} strut mass center is given by

$$\dot{\rho}_{kc} = \dot{R} + \sum_{n=1}^N \phi_n^{-k} \dot{q}_n + \dot{r}_{kce} + \bar{\omega} \times [\bar{R}_{ks} + \sum_{n=1}^N \phi_n^{-k} q_n + \bar{r}_{kcs} + \bar{r}_{kce}] \quad (3-17)$$

in which the subscript c refers to the mass center of the k^{th} strut. Note that $\bar{r}_{kcs} + \bar{r}_{kce} = \bar{r}_{kc}$, the position vector of the k^{th} strut mass center relative to the strut coordinate system (See Figure 3-2).

The components of the vectors $\dot{\rho}_{oi}$ and $\dot{\rho}_{kc}$ in the kinetic energy expression (3-16) were used in applying the Lagrangian equations. The components of these vectors are defined below using the unit normal vectors ($\bar{i}_x, \bar{i}_y, \bar{i}_z$) for the coordinate system in which they are defined.

$$\begin{aligned}
\bar{R} &= X_g \bar{i}_{xg} + Y_g \bar{i}_{yg} + Z_g \bar{i}_{zg} \\
\phi_n^{-i} &= \phi_{xn}^i \bar{i}_{xo} + \phi_{yn}^i \bar{i}_{yo} + \phi_{zn}^i \bar{i}_{zo} \\
\bar{\omega} &= \omega_x \bar{i}_{xo} + \omega_y \bar{i}_{yo} + \omega_z \bar{i}_{zo} \\
\bar{R}_{ks} &= R_{ksx} \bar{i}_{xo} + R_{ksy} \bar{i}_{yo} + R_{ksz} \bar{i}_{zo} \\
\bar{r}_{kcs} &= r_{kcsx} \bar{i}_{xk} + r_{kcsy} \bar{i}_{yk} + r_{kcsz} \bar{i}_{zk} \\
\bar{r}_{kce} &= r_{kcex} \bar{i}_{xk} + r_{kcey} \bar{i}_{yk} + r_{kcez} \bar{i}_{zk} \\
\bar{r}_{ois} &= r_{oisx} \bar{i}_{xo} + r_{oisy} \bar{i}_{yo} + r_{oisz} \bar{i}_{zk}
\end{aligned} \tag{3-18}$$

The position vector

$$\bar{r}_{kc} = \bar{r}_{kcs} + \bar{r}_{kce} \tag{3-19}$$

defines the position of the k^{th} strut center of mass relative to the strut coordinate system in general terms. To incorporate the strut configuration modeled in TOLA, this vector was modified to reflect the actual strut displacements. Using Figure 3-4, which was adapted from Reference (1), the displacement, \bar{r}_{kc} , of the k^{th} moving strut mass is given by

$$\bar{r}_{kc} = (r_{Fk} - S_{kc} - S_k) \bar{i}_{zk} \tag{3-20}$$

where r_{Fk} = fully extended position of axle

S_{kc} = distance between strut axle and strut mass center

S_k = main strut displacement

Equation (3-20) is equation (26) of Reference 1. The quantities r_{Fk} and S_{kc} are reference lengths or distances and S_k is the time varying displacement restricted to move in the \bar{i}_{zk} direction. Therefore the components in equation (3-19) become

$$\begin{aligned}
\bar{r}_{kcs} &= (r_{Fk} - S_{kc}) \bar{i}_{zk} \\
\bar{r}_{kce} &= -S_k \bar{i}_{zk}
\end{aligned} \tag{3-21}$$

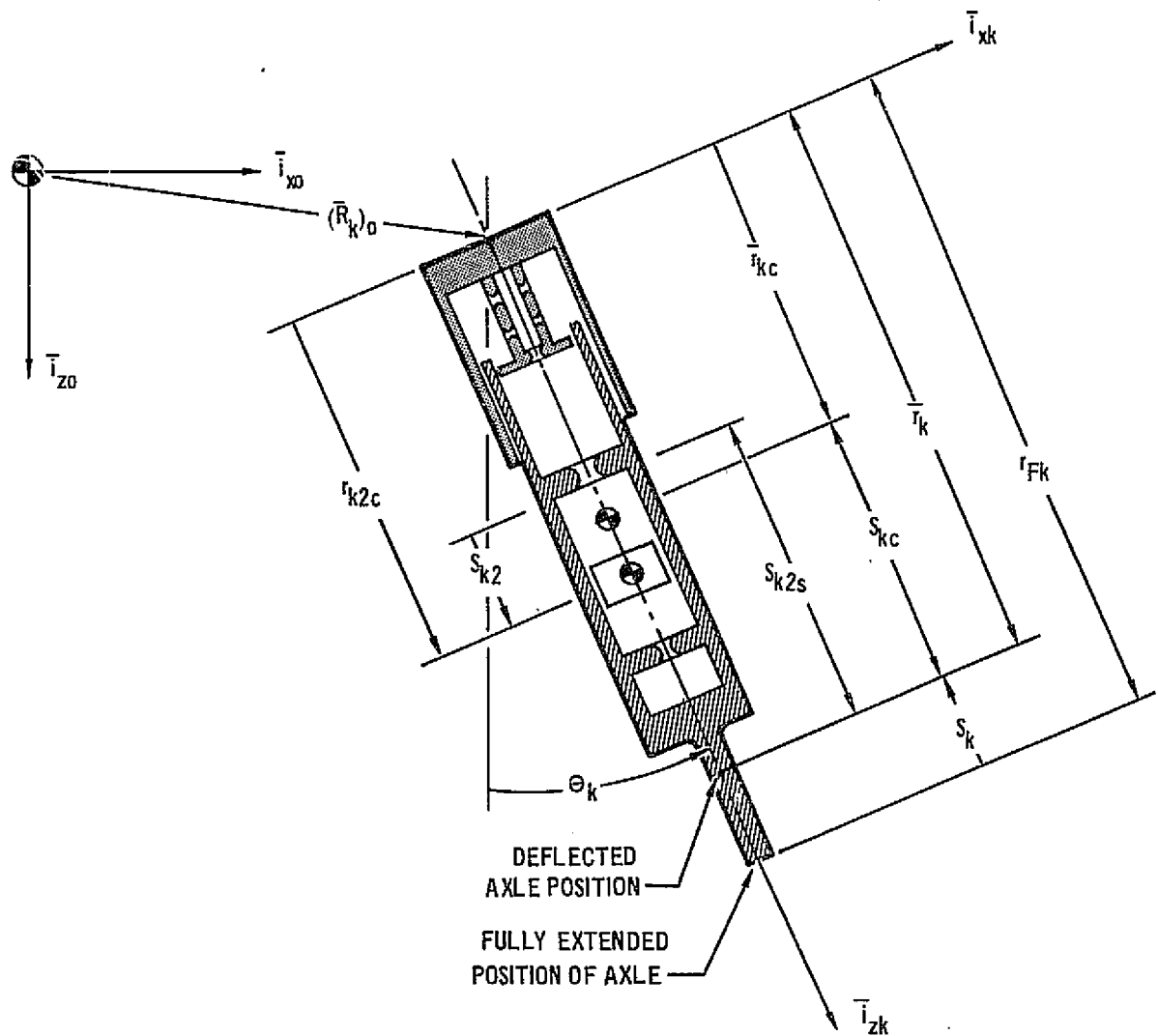


FIGURE 3-4 LANDING GEAR STRUT DISPLACEMENTS

The potential energy, U , due to the strain energy of the main or 0^{th} body is

$$U = \frac{1}{2} \sum_{n=1}^N \omega_n^2 m_n q_n^2 \quad (3-22)$$

where ω_n = the natural frequency of the n^{th} free-free mode

m_n = generalized mass of n^{th} elastic mode

The airplane's equations of motion were obtained by using the Lagrangian equations and the energy expressions of (3-16) and (3-22). The Lagrangian equations may be written

$$\frac{d}{dt} \left(\frac{\partial T}{\partial \dot{q}_p} \right) - \frac{\partial T}{\partial q_p} + \frac{\partial U}{\partial q_p} = Q_p \quad (3-23)$$

where q_p , \dot{q}_p = p^{th} generalized coordinate and generalized velocity respectively

Q_p = generalized force or moment in p^{th} mode

The resulting rigid body translational, rigid body rotational, and the flexible body equations of motion are given in Equations (3-24), (3-25) and (3-26) respectively. Insofar as practical, TOLA nomenclature (Reference 1) has been used. Therefore, the rigid body equations reflecting the effects of the 0^{th} body flexibility can be readily compared to the existing TOLA rigid body equations given in Reference (1) as Equations (157) and (158). The flexible body equations are coupled together and to the rigid body equations by the strut masses m_k . This results from the manner in which the airplane was idealized as a system of $K+1$ bodies. The struts (the k bodies) were considered "rigid" but allowed to move with respect to the main body or airframe. The airframe (0^{th} body) was considered flexible with its elastic effects represented by a limited number of free-free vibratory modes.

RIGID BODY TRANSLATIONAL EQUATIONS

$$\begin{aligned} \bar{F}_T = M_T \ddot{\bar{R}} - \sum_{k=1}^K m_k \ddot{S}_k [A_{k31} \bar{i}_{xo} + A_{k33} \bar{i}_{zo}] + \sum_{n=1}^N \sum_{k=1}^K m_k \dot{q}_n [\phi_{xn}^k \bar{i}_{xo} \\ + \phi_{yn}^k \bar{i}_{yo} + \phi_{zn}^k \bar{i}_{zo}] \end{aligned} \quad (3-24)$$

RIGID BODY ROTATIONAL EQUATIONS

$$\begin{aligned} \bar{M}_O = \bar{I} \cdot \dot{\bar{\omega}} + \bar{\omega} \times [\bar{I} \cdot \bar{\omega}] + \sum_{k=1}^K m_k \dot{S}_k [-A_{k11} R_{ksy} \bar{i}_{xo} + (A_{k13} R_{ksz} \\ + A_{k11} R_{ksx}) \bar{i}_{yo} - A_{k13} R_{ksy} \bar{i}_{zo}] \\ + \sum_{n=1}^N \sum_{k=1}^K m_k \dot{q}_n \left\{ [R_{ksy} \phi_{zn}^k - (R_{ksz} + A_{k11} (r_{Fk} - S_{kc})) \phi_{yn}^k] \bar{i}_{xo} \right. \quad (3-25) \\ + [(R_{ksz} + A_{k11} (r_{Fk} - S_{kc})) \phi_{xn}^k - (R_{ksx} - A_{k13} (r_{Fk} - S_{kc})) \phi_{zn}^k] \bar{i}_{yo} \\ \left. + [(R_{ksx} - A_{k13} (r_{Fk} - S_{kc})) \phi_{yn}^k - R_{ksy} \phi_{xn}^k] \bar{i}_{zo} \right\} \end{aligned}$$

\bar{F}_T = total applied force acting on K+1 bodies

M_T = total mass of K+1 bodies

\bar{M}_O = total moment of all applied forces on K+1 bodies about 0th body center of mass

\bar{I} = inertia tensor for the K+1 bodies about 0th body center of mass

FLEXIBLE AIRFRAME EQUATIONS OF MOTION

FOR $s = 1, 2, 3, \dots, N$

$$\begin{aligned}
 m_s \ddot{q}_s + \omega_s^2 m_s q_s + \sum_{n=1}^N \sum_{k=1}^K m_k [\phi_{xs}^k \phi_{xn}^k + \phi_{ys}^k \phi_{yn}^k + \phi_{zs}^k \phi_{zn}^k] \dot{q}_n \\
 + \sum_{k=1}^K m_k [(\ddot{X} - A_{k31} \ddot{S}_k) \phi_{xs}^k + \ddot{Y} \phi_{ys}^k + (\ddot{Z} - A_{k33} \ddot{S}_k) \phi_{zs}^k] \\
 + \dot{\omega}_x \sum_{k=1}^K m_k [R_{ksy} \phi_{zs}^k - (R_{ksz} + A_{k11} (r_{Fk} - S_{kc})) \phi_{ys}^k] \tag{3-26} \\
 + \dot{\omega}_y \sum_{k=1}^K m_k [(R_{ksz} + A_{k11} (r_{Fk} - S_{kc})) \phi_{xs}^k - (R_{ksx} - A_{k13} (r_{Fk} - S_{kc})) \phi_{zs}^k] \\
 + \dot{\omega}_z \sum_{k=1}^K m_k [(R_{ksx} - A_{k13} (r_{Fk} - S_{kc})) \phi_{ys}^k - R_{ksy} \phi_{xs}^k] = Q_s
 \end{aligned}$$

$Q_s = Q_s^T + Q_s^{DC} + Q_s^A$ = Generalized forces associated with s th mode due to engine thrust, drag chute deployment and aerodynamic pressure respectively

Symbols are defined on the following page

FLEXIBLE AIRFRAME EQUATIONS OF MOTION

m_s, q_s, ω_s = Generalized mass, generalized coordinate and natural frequency respectively associated with the s th elastic free-free mode

$$Q_s^T = \phi_{xs}^{T_1} T_{x1} + \phi_{xs}^{T_2} T_{x2} + \phi_{xs}^{T_3} T_{x3} + \phi_{xs}^{T_4} T_{x4}$$

T_{x1} through T_{x4} = Engine thrust forces

$\phi_{xs}^{T_1}$ through $\phi_{xs}^{T_4}$ = Magnitude of s th mode shape at point force application

$$Q_s^{DC} = \phi_{xs}^{DC} F_{cx} + \phi_{ys}^{DC} F_{cy} + \phi_{zs}^{DC} F_{cz}$$

F_{cx}, F_{cy}, F_{cz} = Forces due to deployment of drag chute

$\phi_{xs}^{DC}, \phi_{ys}^{DC}, \phi_{zs}^{DC}$ = Magnitude of s th mode shape at point of force application

$$Q_s^A = -B_s^1 \phi_{xs}^A a + B_s^2 \phi_{ys}^A y - B_s^3 \phi_{zs}^A n_f + B_s^4 \theta_{xs}^A l + B_s^5 \theta_{ys}^A m + B_s^6 \theta_{zs}^A n$$

a, y, n_f = Aerodynamic forces; l, m, n = aerodynamic moments

$\phi_{xs}^A, \phi_{ys}^A, \phi_{zs}^A$ = Magnitude of s th mode shape at point of force application

$\theta_{xs}^A, \theta_{ys}^A, \theta_{zs}^A$ = Slope of s th mode shape at point of moment application

B_s^1 through B_s^6 = Participation factors for s th mode

Certain simplifying assumptions were made in the equations of motion. These assumptions were consistent with those made in the existing TOLA formulation. In the rigid body equations, the Coriolis acceleration terms for the landing gear struts were neglected mainly because the rotational velocities of the aircraft are small at landing relative to strut acceleration terms retained. Also, in the rigid body rotational equations, terms involving the variation of the inertia or inertia derivative tensors resulting from changing position vectors of the strut masses are small. The changes in the gear positions are very small compared to the overall airplane dimensions, therefore the variation of the inertia terms due to gear position changes are small and were neglected. The flexible airframe equations of motion were also simplified by neglecting terms analogous to those neglected in the rigid body equations. Coriolis and centripetal type accelerations of the strut masses were considered small, again mainly because the rotational velocities of the aircraft are small relative to the strut acceleration terms retained. Rigid body "tangential" type acceleration terms that vary with changing position vectors were neglected; however, all others were retained.

The terms in the rigid body equations, (3-24) and (3-25), resulting from the addition of flexibility were programmed and added to the rigid body equations already coded in TOLA. The flexible airframe equations of motion (3-26) in their entirety were programmed and incorporated in TOLA. Modifications in the strut equations of motion required to reflect the elasticity of the airframe are discussed in the following section.

3.1.2.2 Landing Gear Equations - These equations consist of the strut mass, strut secondary piston, and wheel equations of motion. Since the basic landing gear idealizations are identical to those used in the existing TOLA computer program, their equations of motion will not be completely rederived. However, they will be discussed in sufficient detail so as to clarify the changes made.

The equation of the k^{th} strut mass for a rigid airframe from Reference (1), (Equation 37) is

$$\ddot{\mathbf{S}}_k = \{ \ddot{\mathbf{R}} + \dot{\bar{\omega}} \times (\bar{\mathbf{R}}_k)_o + \bar{\omega} \times [\bar{\omega} \times (\bar{\mathbf{R}}_k)_o] \} \cdot \bar{\mathbf{i}}_{zk} - \frac{1}{m_k} \sum F_{kz} \quad (3-27)$$

where F_{kz} = forces applied to k^{th} strut in $\bar{\mathbf{i}}_{zk}$ direction

The strut mass, m_k , is defined as the landing gear mass which may move relative to the airframe (0^{th} body). \mathbf{S}_k is defined in Figure 3-4 and

Equation (3-20). Neglected and not shown in Equation (3-27) are the quantities $2\bar{\omega} \times \dot{\bar{r}}_{kc}$, $\dot{\bar{\omega}} \times \bar{r}_{kc}$ and $\bar{\omega} \times [\bar{\omega} \times \bar{r}_{kc}]$. These quantities were neglected since $\bar{\omega}$ and $\dot{\bar{\omega}}$ are small at landing and $(\bar{R}_k) \gg \bar{r}_{kc}$.

With airframe flexibility, the equation of motion for the k^{th} strut mass becomes

$$\ddot{\bar{S}}_k = \{\ddot{\bar{R}} + \ddot{\bar{R}}_{ke} + \dot{\bar{\omega}} \times \bar{R}_{ks} + \bar{\omega} \times [\bar{\omega} \times \bar{R}_{ks}]\} \cdot \bar{i}_{zk} - \frac{1}{m_k} \sum F_{zk} \quad (3-28)$$

In addition to the terms neglected in Equation (3-27), the quantities $2\bar{\omega} \times \dot{\bar{R}}_{ke}$, $\dot{\bar{\omega}} \times \bar{R}_{ke}$, and $\bar{\omega} \times [\bar{\omega} \times \bar{R}_{ke}]$ were neglected in Equation (3-28) since $\bar{\omega}$ is small at landing and $\bar{R}_{ks} \gg \bar{R}_{ke}$. Thus, the modification in the strut equation of motion to reflect airframe flexibility is

$$\ddot{\bar{R}}_{ke} \cdot \bar{i}_{zk} = A_{k31} \sum_{n=1}^N \phi_{xn}^k \ddot{q}_n + A_{k33} \sum_{n=1}^N \phi_{zn}^k \ddot{q}_n \quad (3-29)$$

Equation (3-29) was programmed and incorporated in the strut equations solved in TOLA's flexible body option.

The forces, F_{zk} , acting on the k^{th} strut in Equation (3-28) are completely defined in Reference (1). Some of these forces are functions of S_{k2} and \dot{S}_{k2} , the displacement and velocity respectively, of the strut secondary piston mass. Figure 2-1 shows the secondary piston mass and Figure 3-4 shows S_{k2} . The equation of motion for the k^{th} strut secondary piston mass for a rigid airframe from Reference (1), (Equation 56) is

$$\ddot{S}_{k2} = \frac{1}{m_{k2}} \sum F_{k2z} - \{\ddot{\bar{R}} + \dot{\bar{\omega}} \times (\bar{R}_k)_o + \bar{\omega} \times [\bar{\omega} \times (\bar{R}_k)_o]\} \cdot \bar{i}_{zk} + \dot{S}_k \quad (3-30)$$

where m_{k2} = mass of k^{th} strut secondary piston mass

F_{k2z} = forces applied to k^{th} strut secondary piston mass

\dot{S}_k = Defined in Equation (3-27)

For the flexible body option, the k^{th} strut secondary piston mass equation is

$$\ddot{S}_{k2} = \frac{1}{m_{k2}} \sum F_{k2z} - \{\ddot{\bar{R}} + \ddot{\bar{R}}_{ke} + \dot{\bar{\omega}} \times \bar{R}_{ks} + \bar{\omega} \times [\bar{\omega} \times \bar{R}_{ks}]\} \cdot \bar{i}_{zk} + \ddot{S}_k \quad (3-31)$$

in which \ddot{S}_k is defined by Equation (3-28). The simplifying assumptions made to obtain Equations (3-30) and (3-31) are identical to those made in arriving

at Equations (3-27) and (3-28) respectively. Equation (3-29) also defines the changes made to the k^{th} strut secondary piston mass equation of motion in TOLA to incorporate the flexible body option.

The final landing gear equation of motion to consider is the strut wheel rotational equation. Since the ground reaction forces are dependent on the tire-ground interface velocities, the rotational velocities of the wheels or tires are required. The rotational equation of motion for the k^{th} strut wheel is

$$\dot{\omega}_{Tk} = \left(M_{Ak} - M_{Bk} \left| \frac{\omega_{Tk}}{\omega_{Tk}} \right| \right) \cdot \left(\frac{1}{n_k I_k} \right) \quad (3-32)$$

ω_{Tk} = rotational rate of k^{th} strut wheel

M_{Ak} = moment of the ground reaction forces about k^{th} strut axle

M_{Bk} = moment of the applied braking forces about k^{th} strut axle

I_k = moment of inertia of k^{th} strut wheel about axle

n_k = number of tires on k^{th} strut

The above Equation (3-32) from Reference (1) (Equation 148) remains unchanged in form for the flexible body option. However, the moment M_{Ak} is dependent on the airframe elastic displacements and velocities.

In addition to M_{Ak} , the ground reaction forces and moments included in \bar{F}_T , \bar{M}_O and F_{zk} of equations (3-24), (3-25), and (3-28) are functions of the airframe elastic displacements or velocities. Also, other quantities, such as the tire deflection, which is directly used in the TOLA program logic to determine whether or not the tire deflection has been exceeded, depend in part on the airframe elastic displacements. The changes in the TOLA equations made to reflect these effects are defined below.

The position vector of the k^{th} strut axle for a rigid airframe, from Equation (98) of Reference (1), is

$$(\bar{r}_k)_O + \bar{r}_k = R_{Axk} \bar{i}_{xg} + R_{Ayk} \bar{i}_{yg} + R_{Azk} \bar{i}_{zg} \quad (3-33)$$

where

$$\begin{Bmatrix} R_{Axk} \\ R_{Ayk} \\ R_{Azk} \end{Bmatrix} = \begin{bmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_3 & n_3 \end{bmatrix} \begin{bmatrix} [R_{kx} + A_{k31} (r_{Fk} - S_k)] \\ [R_{ky}] \\ [R_{kz} + A_{k33} (r_{Fk} - S_k)] \end{bmatrix}$$

This position vector is shown in Figure 3-4. Using the first of Equations (3-9) and (3-10), the position vector of the k^{th} strut axle for the flexible airframe option becomes

$$\begin{Bmatrix} R_{Axk} \\ R_{Ayk} \\ R_{Azk} \end{Bmatrix} = \begin{Bmatrix} R_{Axk} \\ R_{Ayk} \\ R_{Azk} \end{Bmatrix} + \begin{Bmatrix} \Delta R_{Axk} \\ \Delta R_{Ayk} \\ \Delta R_{Azk} \end{Bmatrix} \quad (3-34)$$

where

$$\begin{Bmatrix} \Delta R_{Axk} \\ \Delta R_{Ayk} \\ \Delta R_{Azk} \end{Bmatrix} = \begin{bmatrix} l_1 & m_1 & n_1 \\ l_2 & m_2 & n_2 \\ l_3 & m_3 & n_3 \end{bmatrix} \begin{Bmatrix} \sum_{n=1}^N \phi_{xn}^k q_n \\ \sum_{n=1}^N \phi_{yn}^k q_n \\ \sum_{n=1}^N \phi_{zn}^k q_n \end{Bmatrix}$$

The velocity vector of the k^{th} strut axle was also modified. From Equation (139) of Reference (1), the velocity vector for the axle assuming a rigid airframe is

$$\left(\dot{\vec{R}}_k \right)_o + \dot{\vec{r}}_k = R_{Dxk} \bar{i}_{xo} + R_{Dyk} \bar{i}_{yo} + R_{Dzk} \bar{i}_{zo} \quad (3-35)$$

where

$$\begin{Bmatrix} R_{Dxk} \\ R_{Dyk} \\ R_{Dzk} \end{Bmatrix} = \begin{bmatrix} [-\dot{S}_k A_{k31} + \omega_y A_{k33} (r_{Fk} - S_k) + \omega_y R_{kz} - \omega_z R_{ky}] \\ [(r_{Fk} - S_k) (\omega_z A_{k31} - \omega_x A_{k33}) + \omega_z R_{kx} - \omega_x R_{kz}] \\ [-\dot{S}_k A_{k33} - \omega_y A_{k31} (r_{Fk} - S_k) + \omega_x R_{ky} - \omega_y R_{kx}] \end{bmatrix}$$

Using the time derivatives of the first of Equations (3-9) and (3-10), the velocity vector of the k^{th} strut axle for the flexible airframe option is

$$\begin{Bmatrix} R_{Dxk} \\ R_{Dyk} \\ R_{Dzk} \end{Bmatrix} = \begin{Bmatrix} R_{Dxk} \\ R_{Dyk} \\ R_{Dzk} \end{Bmatrix} + \begin{Bmatrix} \Delta R_{Dxk} \\ \Delta R_{Dyk} \\ \Delta R_{Dzk} \end{Bmatrix} \quad (3-36)$$

where

$$\begin{Bmatrix} \Delta R_{Dxk} \\ \Delta R_{Dyk} \\ \Delta R_{Dzk} \end{Bmatrix} = \begin{Bmatrix} \left[\omega_y \sum_{n=1}^N \phi_{zn}^k q_n - \omega_z \sum_{n=1}^N \phi_{yn}^k q_n + \sum_{n=1}^N \phi_{xn}^k \dot{q}_n \right] \\ \left[\omega_z \sum_{n=1}^N \phi_{xn}^k q_n - \omega_x \sum_{n=1}^N \phi_{zn}^k q_n + \sum_{n=1}^N \phi_{yn}^k \dot{q}_n \right] \\ \left[\omega_x \sum_{n=1}^N \phi_{yn}^k q_n - \omega_y \sum_{n=1}^N \phi_{xn}^k q_n + \sum_{n=1}^N \phi_{zn}^k \dot{q}_n \right] \end{Bmatrix}$$

This completes the discussion of the analytical methods used to modify the TOLA computer program to incorporate the flexible body option.

3.2 Program Description - The changes and additions made to the TOLA computer program are discussed in general in this section. The structure of the flexible body option and how it interfaces with the existing TOLA program are described using a flow diagram. All programming is in CDC FORTRAN 2.3 language for machine computation on CDC 6000 series computers.

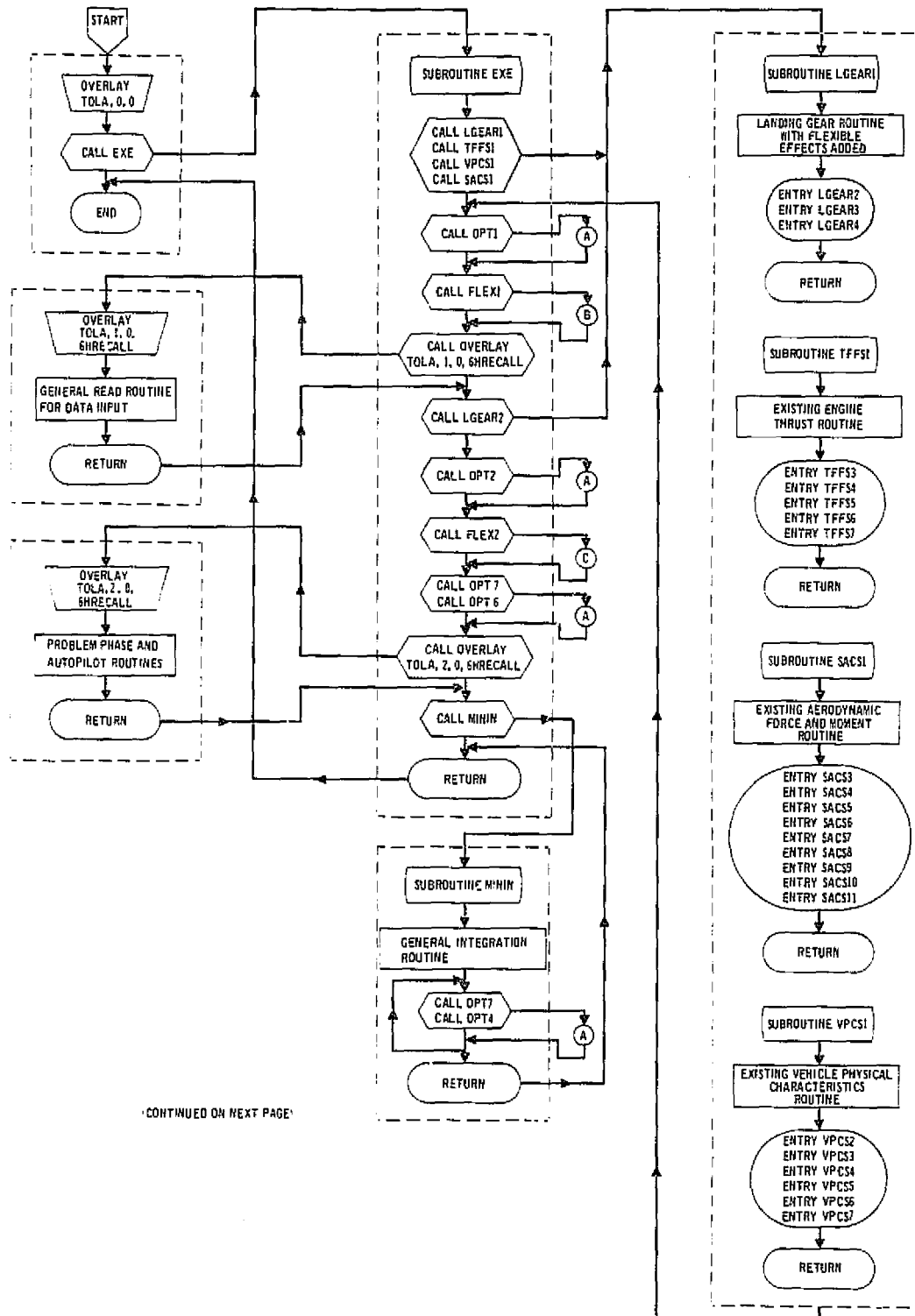
3.2.1 Option Flow Diagram - A flow diagram showing the general operation of the flexible body option is shown in Figure 3-5. The three OVERLAY segments are shown in addition to the various subroutines which directly interface with the flexible body option subroutine, FLEX1. The diagram is not intended to be a comprehensive programming chart, but shows the general flow of the option logic and indicates the order of operations within FLEX1. A complete listing of the TOLA computer program with flexible body option is given in Appendix A.

The basic structure of TOLA has been retained. It is still made up of three OVERLAY segments. OVERLAY (TOLA, 0, 0) consists of the executive subprogram TOLA. Through its call to subroutine EXE, it calls the other two overlays and controls the execution of the complete program. TOLAN1 is the executive subprogram in OVERLAY (TOLA, 1, 0). It reads the input data and checks to determine if the proper amount of input data has been supplied. TOLAN2 is the executive subprogram in OVERLAY (TOLA, 2, 0). It provides the autopilot and problem phase functions.

The flexible body option is contained in subroutine FLEX1. The operations performed in FLEX1 are indicated in Figure 3-5. FLEX1 is structured similar to subroutines OPT1 and LGEAR1. This allows efficient use of the existing read, write, integration and update routines.

3.3 Program Operation - An understanding of program development in itself will not result in smooth program operation. Successful operation of the TOLA computer program with the flexible body option depends on proper input of all required data. Much of these data are associated with the existing rigid body version of TOLA. It is not the purpose of this document to define these data, for this is done in Reference 3. The sections that follow will describe the general input data format, define all possible data associated with the flexible body option and the manner in which it is to be input, and discuss the resulting output.

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FIGURE 3-5 FLOW DIAGRAM FOR TOLA COMPUTER PROGRAM FLEXIBLE BODY OPTION

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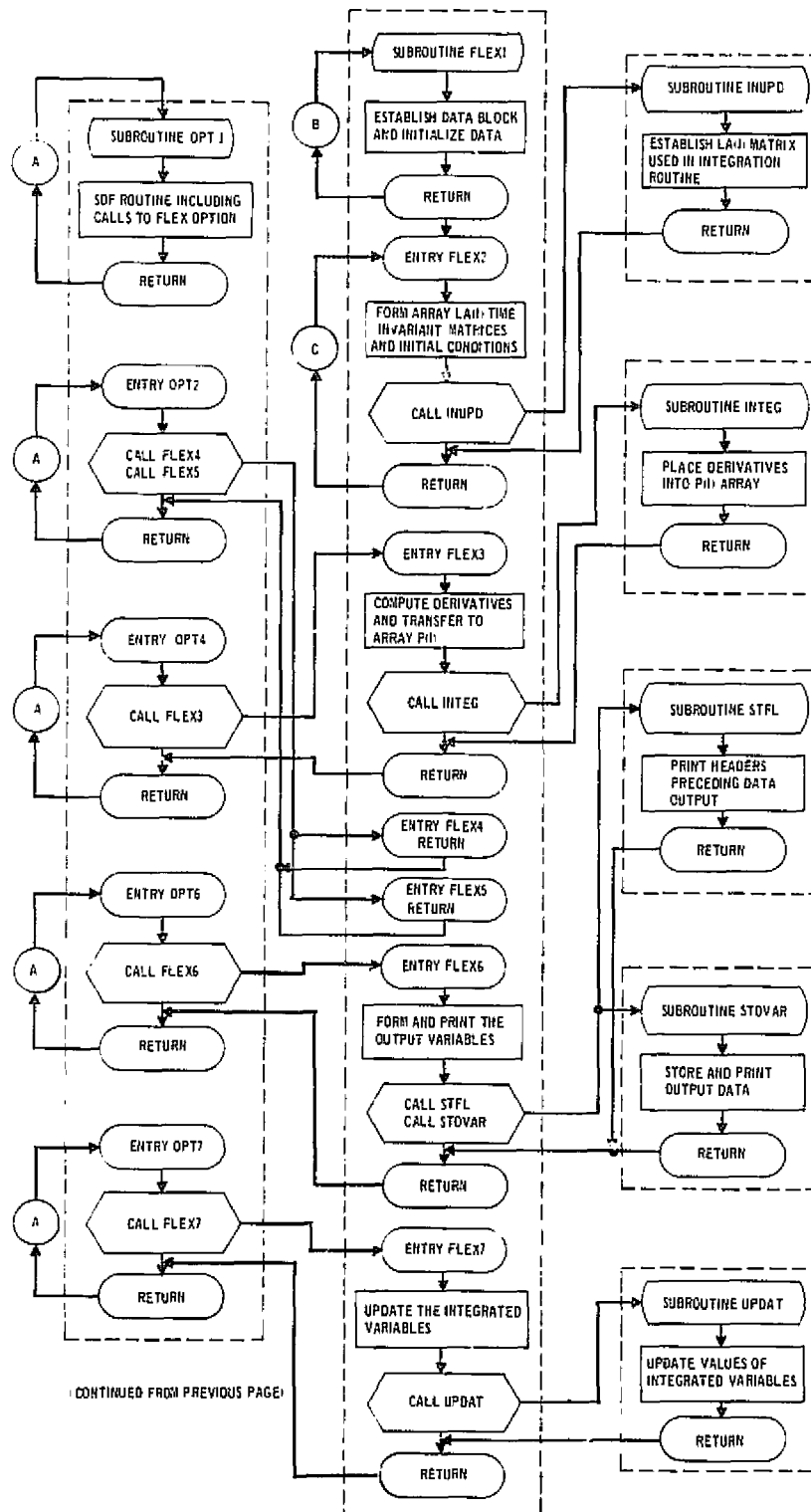


FIGURE 3-5 FLOW DIAGRAM FOR TOLA COMPUTER
PROGRAM FLEXIBLE BODY OPTION (Continued)

3.3.1 General Input Data Format - The input data associated with the flexible body option are read into the program by the existing input routine (READ). As a result, it must follow the same general format as the rigid body data. The input must follow the following format:

Card Columns	1-6	7	8-10	11	12-66	67-72	73-80
Field Number	I	II	III	IV	V	VI	VII

Field number I contains the alphanumeric variable name of the data contained in Field V. Example:

[illegible]

The program will assign a value of "1" to the variable INDFLX.

Field number II is not used.

Field number III is used to define the type of data in Field V by means of the words DEC, BCD, INT, TRA or a blank. DEC and blank are equivalent and denote that data which follow are in decimal form. The word OCT specifies that the data in Field V are to be interpreted as octal numbers. The word BCD specifies that N binary coded, six character words (N punched in column 12) are to be loaded. These decimal words begin in column 13. The largest number of six character words that can be loaded from one card is nine. The user should make sure that BCD data does not get punched into Field VI, or an input error will result. When the word INT is used, it is assumed that all numbers in Field V will be loaded as integers. If only one integer is punched per card, the INT may be omitted. The word TRA denotes to the read routine that all data have been input and to return control to the calling program.

Example:

[illegible]

INPUT INDICATOR/ VARIABLE	COORDINATE SYSTEM(1)	INDICATOR OR VARIABLE DEFINITION
INDFLX		INDICATOR DEFINING OPTION INDFLX = 0 - RIGID AIRFRAME INDFLX = 1 - FLEXIBLE AIRFRAME
NMODE		INDICATES NUMBER OF MODES INPUT (20 MAXIMUM)
GMAS1(I)		GENERALIZED MASS OF I TH ELASTIC MODE
GFREQ(I)		FREQUENCY OF I TH MODE (RADIAN/SEC)
SXMOD(I)	BCS	X MODE SHAPE FOR STRUT ATTACHMENT POINTS IN I TH MODE
SYMOD(I)	BCS	Y MODE SHAPE FOR STRUT ATTACHMENT POINTS IN I TH MODE
SZMOD(I)	BCS	Z MODE SHAPE FOR STRUT ATTACHMENT POINTS IN I TH MODE
TXMOD(I)	BCS	X MODE SHAPE FOR ENGINE THRUST APPLICATION ATTACHMENT POINTS IN I TH MODE
ARMODE(I)	BCS	X,Y,Z, θ_x , θ_y , θ_z COMPONENTS OF MODE SHAPE FOR AERODYNAMIC FORCE AND MOMENT REFER- ENCE LOCATION IN I TH MODE
PF(I)		PARTICIPATION FACTORS OF GENERALIZED AERODYNAMIC FORCES AND MOMENTS IN I TH MODE
SKC(K)	SCS	DISTANCE BETWEEN K TH STRUT AXLE AND STRUT CENTER OF MASS
DCMODE(I)	BCS	X,Y,Z COMPONENTS OF MODE SHAPE FOR DRAG CHUTE ATTACHMENT POINT IN I TH MODE
NPTS		NUMBER OF POINTS ON THE AIRFRAME AT WHICH OUTPUT IS REQUESTED (20 MAXIMUM)
ROIS(J)	BCS	ROISX, ROISY, ROISZ COMPONENTS OF POSITION VECTOR FOR J TH POINT ON FLEXIBLE AIRFRAME AT WHICH OUTPUT IS REQUESTED
OUTMOD(I)	BCS	X,Y,Z COMPONENTS OF I TH MODE SHAPE FOR POINTS ON FLEXIBLE AIRFRAME AT WHICH OUTPUT IS REQUESTED.
IFLX(I)		INDICATES THE POINTS WHOSE DATA WILL BE STORED ON TAPE

(1) NOTE: BCS = BODY COORDINATE SYSTEM SCS = STRUT COORDINATE SYSTEM

FIGURE 3-6 INPUT DATA FOR TOLA FLEXIBLE BODY OPTION

can be used. The natural frequency, GFREQ(I), and generalized mass, GMASS1(I), for each mode must be input. The mode shape magnitudes, SXMOD(I), SYMOD(Y), SZMOD(Z), for each mode at the strut attachment locations should be input. While the program will run without these input data, it will use a value of zero for the mode shape magnitudes. Similarly, the mode shape data at the point of application of the engine thrust, TXMOD(I), and aerodynamic forces and moments, ARMODE(I), should be input for solution of any practical takeoff/landing problem.

The aerodynamic loads are treated as concentrated loads in TOLA in the form of total aerodynamic forces and moments acting at a selected reference point on the airframe. To obtain realistic flexible body response, weighting effects or participation factors, PF(I), of the aerodynamic loads on the response of each normal mode are required. If aerodynamic effects on the flexible airframe response are desired, the user must input the proper values for the PF(I) array. If the PF(I) are not input, the default values for this array are zero and all effects of the aerodynamic loads on modal response are assumed to be small and therefore neglected. A general approach for calculating the aerodynamic weighting effects is suggested in Appendix B.

All of the arrays used in the flexible body option are in vector form (one dimensional), and the subroutine expects the modal data to appear in a particular order on the data input cards. The order required by the subroutine is best shown through an example. If the aircraft simulated in the program has three landing gear struts and two engines, and four vibratory modes are selected to represent airframe flexibility, then the typical strut and engine attachment point modal data would appear as follows:

Strut 1 Attach Point

Mode	X	Y	Z
1	-.41	.68	-.14
2	.38	.03	.79
3	-.40	-.08	.03
4	-.25	.16	.17

Strut 2 Attach Point

Mode	X	Y	Z
1	-.83	.69	-.33
2	.48	.06	.86
3	-.83	-.07	.05
4	-.47	.17	.38

Strut 3 Attach Point

Mode	X	Y	Z
1	-1.00	.69	-.41
2	.52	.07	.89
3	-1.00	-.08	.05
4	-.55	.17	.49

Engine 1 Attach Point

Mode	X
1	-.64
2	.29
3	-.59
4	-.32

Engine 2 Attach Point

Mode	X
1	-.68
2	.36
3	-.65
4	-.37

Write each component of the strut attachment point mode shape as though in an array dimensioned number-of-struts x number-of-modes.

$$\begin{aligned}
 [\text{SXMOD}] &= \begin{bmatrix} -.41 & .38 & -.40 & -.25 \\ -.83 & .48 & -.83 & -.47 \\ -1.0 & .52 & -1.0 & -.55 \end{bmatrix} \\
 [\text{SYMOD}] &= \begin{bmatrix} .68 & .03 & -.08 & .16 \\ .69 & .06 & -.07 & .17 \\ .69 & .07 & -.08 & .17 \end{bmatrix} \\
 [\text{SZMOD}] &= \begin{bmatrix} -.14 & .79 & .03 & .17 \\ -.33 & .86 & .05 & .38 \\ -.41 & .89 & .05 & .49 \end{bmatrix}
 \end{aligned}$$

The engine attachment point modal data should be written in an array dimensioned number-of-engines x number-of-modes:

$$[\text{TXMOD}] = \begin{bmatrix} -.64 & .29 & -.59 & -.32 \\ -.68 & .36 & -.65 & -.37 \end{bmatrix}$$

Transform each array into vector form by reading the matrix elements by columns. Thus the order in which the data is read would be as follows:

SXMOD = -.41	SYMOD = .68	SZMOD = -.14	TXMOD = -.64
-.83	.69	-.33	-.68
-1.0	.69	-.41	.29
.38	.03	.79	.36
.48	.06	.86	-.59
.52	.07	.89	-.65
-.40	-.08	.03	-.32
-.83	-.07	.05	-.37
-1.0	-.08	.05	
-.25	.16	.17	
-.47	.17	.38	
-.55	.17	.49	

This data would then be placed on cards according to the format described in the previous section.

Typical aerodynamic data and participation factors would appear as follows:

Aerodynamic Data

Mode	X	Y	Z	θ_X	θ_Y	θ_Z
1	.16	.20	-.89	.0004	.0045	.0009
2	.20	.15	-.96	.0002	.0053	-.0003
3	.12	.08	-.65	-.0001	.0038	.0010
4	.05	.09	-.59	.0003	.0036	-.0007

Participation Factors

Mode	X	Y	Z	θ_X	θ_Y	θ_Z
1	.30	.36	-1.87	.15	-.93	.20
2	.46	.39	2.15	.12	-1.15	-.09
3	.28	.21	-1.13	.04	-.83	.21
4	.16	.24	.97	.08	-.79	-.17

Again, write the data in an array where each column represents the data for a single mode; then read the matrix columnwise.

$$\text{ARMODE} = \begin{bmatrix} .16 & .20 & .12 & .05 \\ .20 & .15 & .08 & .09 \\ -.89 & -.96 & -.65 & -.59 \\ .0004 & .0002 & -.0001 & .0003 \\ .0045 & .0053 & .0038 & .0036 \\ .0009 & -.0003 & .0010 & -.0007 \end{bmatrix} \quad \text{PF} = \begin{bmatrix} .30 & .46 & .28 & .16 \\ .36 & .39 & .21 & .24 \\ -1.87 & 2.15 & -1.13 & .97 \\ .15 & .12 & .04 & .08 \\ -.93 & -1.15 & -.83 & -.79 \\ .20 & -.09 & .21 & -.17 \end{bmatrix}$$

ARMODE = .16

.20

-.89

.0004

.0045

.0009

.20

.15

.

.

.

PF = .30

.36

1.87

.15

-.93

.20

.46

.39

.

.

.

SKC(K) and DCMODE(I) are optional data. The program sets these quantities to zero if not input. SKC(K) is the distance from the tire axle to the strut center of mass measured along the strut stroke. It is approximately equal to zero for many landing gears. The order in which the struts are numbered in SKC(K) must be consistent with the order implied by the strut attachment point mode shapes. If the third row in the modal data represents the motion of the third strut, the third element in array SKC(K) must be the described distance for that strut.

DCMODE(I) defines the mode shape at the drag chute attach point and is necessary only when the aircraft has a drag chute. These modal data are input in an order similar to that for the aerodynamic data. If written in a two-dimensional array, each column of data represents the X, Y, Z components of the mode shape for a given mode.

The remaining input data indicated in Figure 3-6 are necessary to obtain flexible body response output on the airframe. NPTS indicates the number of points at which output is requested. ROIS(J) are the X, Y, Z components of

the position vector defining the location of the points relative to the air-frame or 0th body coordinate system. OUTMOD(I) are the components of each mode shape at those points for which output is specified. As before, the order of the data is significant and an example will best show this. If output is desired at two points on the aircraft, typical data would appear as below:

Point 1

Location	Mode	1	2	3	4
X = 2.71	X	.09	.11	-.05	.02
Y = 17.63	Y	.02	.01	-.03	.01
Z = 1.52	Z	.95	-.98	.87	-.77

Point 2

Location	Mode	1	2	3	4
X = 2.71	X	.07	.10	-.04	.01
Y = 8.42	Y	.01	-.02	-.03	-.02
Z = 1.25	Z	.43	-.39	.41	-.29

The matrix ROIS(J) should be written as though dimensioned 3(X,Y,Z) x NPTS and then read by columns. For the above example, ROIS(J) would appear as follows:

$$\text{ROIS(J)} = 2.71, 17.63, 1.52, 2.71, 8.42, 1.25$$

Each column of OUTMOD(I) should contain all of the modal data for a given point. The X component of data for all modes should precede the Y component, with the Y component preceding the Z. Written in two dimensional form for the example being considered, OUTMOD(I) would be given as:

$$[\text{OUTMOD}] = \begin{bmatrix} .09 & .07 \\ .11 & .10 \\ -.05 & -.04 \\ .02 & .01 \\ .02 & .01 \\ .01 & -.02 \\ -.03 & -.03 \\ .01 & -.02 \end{bmatrix} \left\{ \begin{array}{l} \text{X Component} \\ \text{Y Component} \end{array} \right.$$

$$\begin{bmatrix} .95 & .43 \\ -.98 & -.39 \\ .87 & .41 \\ -.77 & -.29 \end{bmatrix} \left. \vphantom{\begin{bmatrix} .95 & .43 \\ -.98 & -.39 \\ .87 & .41 \\ -.77 & -.29 \end{bmatrix}} \right\} \text{Z Component}$$

This matrix should be transformed to vector form by reading the elements by column.

The array IFLX(I) dictates which flexible body response data will be saved on tape and used as input for a plot routine. Subroutine FLEX can formulate and print the flexible body response at up to twenty points on the aircraft. IFLX(I) enables the user to select from these points, those whose data will be plotted. Each output point is assigned a number by the order in which their modal data appears in array ØUTMØD(I). An element in IFLX whose value is one will cause the data for that respective point to be placed on tape. For example, if response data is formulated at five points on the aircraft, IFLX = (1, 0, 1, 1, 0) will cause all flexible body data associated with point numbers one, three and four to be saved on tape. Other indicators required to store TOLA output data are discussed in Section 3.3.5. If no flexible body response data is desired, NPTS, RØIS, ØUTMØD and IFLX need not be input.

There is no specific system of units associated with the input information, except for the modal frequencies which must be expressed in radians/unit time. All other parameters may be expressed in any consistent set of units, either English or Metric (inches or centimeters, pounds or dynes). The units selected must, of course, be consistent with the rigid body set used (see Reference 3).

3.3.3 Output Data from the Flexible Body Option - The data that can be output from subroutine FLEX1 consists of the flexible body components of the inertial accelerations, velocity and displacement in each of the three body coordinate directions and the total inertial acceleration and velocity in each coordinate direction. The output variable names used in FLEX1 and their definition are given in Figure 3-7.

3.3.4 Staging the Flexible Body Option into the Program - If aircraft elasticity is desired in an analysis, the program will turn the flexible body option subroutine on at the same time the landing gear subroutine is staged

ALL QUANTITIES ARE IN BODY COORDINATES

POINT - DEFINES THE POINT NUMBER (1-20)

XD2F - X COMPONENT OF THE INERTIAL ACCELERATION DUE TO FLEXIBILITY

XD2T - X COMPONENT OF THE TOTAL INERTIAL ACCELERATION

YD2F - Y COMPONENT OF THE INERTIAL ACCELERATION DUE TO FLEXIBILITY

YD2T - Y COMPONENT OF THE TOTAL INERTIAL ACCELERATION

ZD2F - Z COMPONENT OF THE INERTIAL ACCELERATION DUE TO FLEXIBILITY

ZD2T - Z COMPONENT OF THE TOTAL INERTIAL ACCELERATION

XD1F - X COMPONENT OF THE INERTIAL VELOCITY DUE TO FLEXIBILITY

XD1T - X COMPONENT OF THE TOTAL INERTIAL VELOCITY

YD1F - Y COMPONENT OF THE INERTIAL VELOCITY DUE TO FLEXIBILITY

YD1T - Y COMPONENT OF THE TOTAL INERTIAL VELOCITY

ZD1F - Z COMPONENT OF THE INERTIAL VELOCITY DUE TO FLEXIBILITY

ZD1T - Z COMPONENT OF THE TOTAL INERTIAL VELOCITY

XDOF - X COMPONENT OF DISPLACEMENT DUE TO FLEXIBILITY

YDOF - Y COMPONENT OF DISPLACEMENT DUE TO FLEXIBILITY

ZDOF - Z COMPONENT OF DISPLACEMENT DUE TO FLEXIBILITY

FIGURE 3-7 OUTPUT VARIABLES USED IN FLEX1

into the program. This is done by testing the values of both the flexible body option indicator (INDFLX) and the landing gear indicator (INDLG). Both must be non-zero for flexibility effects to be included.

Initial generalized displacements are calculated based on values of variables at the time the option is staged into the program. These initial displacements are then used in subsequent calculation of the generalized accelerations.

3.3.5 Data Plotting Information - Major revisions were made to the subroutine that stores data for use by a separate plotting program. As now rewritten, subroutine SDFLGP first prints headers that identify the variable names of the data that follow. These headers are printed only once. Each call to the subroutine then writes to tape all data associated with a single time point. This eliminates the need to store the data in intermediate arrays.

The indicators described in Reference 3 and earlier in this report that control the logic in SDFLGP have not been modified. They are as follows:

IPLT = 1	denotes that data will be stored on tape for plotting
ISDF = 1	indicates rigid body data will be saved
ISTPL1 = 1	} denotes that data for landing gears number 1 through 5 will be stored on tape
ISTPL2 = 1	
ISTPL3 = 1	
ISTPL4 = 1	
ISTPL5 = 1	
IFLX(I) = 1	indicates that flexible response data for the i th output point will be saved

A new plotting program was developed to be compatible with the data format of the revised TOLA subroutine SDFLGP. This program, entitled PLTDAT, is submitted as a separate job after a data tape has been generated by the TOLA program. The plot tape generated by PLTDAT can then be used by any off-line plotting device. A listing of the PLTDAT computer program is given in Appendix C.

The plot program was designed to permit the user a high degree of flexibility in the use of the program. Any variable stored for plotting may be chosen as the independent variable. Not only does this allow conventional time history plots to be made, but also such plots as the altitude of the

center of gravity versus downrange position or strut acceleration versus strut stroke. A maximum of five dependent variables can be plotted on a single graph. This enables the users to make direct comparisons of several simultaneously displayed variables.

All graphs are scaled to an 8-1/2 x 11 inch page size; however, the actual plotting area depends on the number of dependent variables. The ordinate (dependent variable) axis is six inches in length. The length of the abscissa (independent variable) axis ranges from 9.4 inches for one dependent variable to 7.0 inches for five dependent variables.

The input data required by the plot program must follow a particular format. The first card contains an integer (format I6) that specifies the number of data points plotted per graph. The remaining cards control the number of plots, define graph titles and dictate the dependent and independent variables. This is accomplished by beginning each data card with a control identifier. These control identifiers are TITLE1, TITLE2, INDVAR, DEPVAR and PLOT. All identifiers must begin in column 1 with their associated data beginning in column 11. TITLE1 and TITLE2 permit a 40 character title and subtitle to be printed on the graph. If no titles are desired, these data are omitted. INDVAR defines the variable name on that card as the independent variable. DEPVAR defines a maximum of five variable names (format 5A10) as dependent variables. The word PLOT causes the graphs to be generated with the current titles, dependent and independent variables.

In order to uniquely identify all variables, a two digit numerical prefix is assigned to each repetitive data name. For example, if TOLA subroutine SDFLGP has saved data for landing gears one, three, and five, PLTDAT will assign a 01 prefix to all data for gear one, a 02 prefix to all data for gear three, and a 03 prefix to all data for gear five. Thus the strut acceleration for gear five would be 03SD2 while the strut stroke for gear three would be 02S.

Figure 3-8 shows a sample of input data for the plotting program. TOLA subroutine SDFLGP has already saved flexible body data for three points on the aircraft and landing gear data for gear numbers one, three, four and five. The first line in the plotting data indicates that two hundred points will be plotted on each graph. The main title for the first plot is "TOLA TIME HISTORY" while the subtitle is "STRUT ACCELERATIONS". The independent variable is time.

and its operating cost. Using the existing OVERLAY structure, the TOLA computer program with the flexible body option has a core requirement of 67K octal words. Most of the space associated with the flexible body option itself is allocated to store the potentially large quantity of input modal data. Every effort was made during program development to streamline the option.

Program operating costs vary from one computer system to the next so it is not possible to develop a single cost formula. Several observations, however, can be made. The major factors that effect the cost of a TOLA run are the total number of integration steps and the number of variables that need to be integrated. The number of integration steps is dictated by the time length of the analysis and the integration step size. Although the user has little control over the step size chosen by the integration routine, he can directly input the time at which the program will terminate. Care should be taken to insure that the program does not continue to run beyond the points of interest.

Figure 3-9 lists the running time in seconds for five examples used to test the flexible body option. All runs terminated at the same point in the landing analysis so that the differences in cost can be attributed to the number of variables that required integration. A flexible body run adds two variables that require integration for each additional mode. An approximation to determine the time of a flexible body run is given by the expression:

$$(\text{TIME})_{\text{FLEX}} \doteq (\text{TIME})_{\text{RIGID}} \cdot \left(\frac{(\text{NO. OF INTEGRATED VARIABLES})_{\text{FLEX}}}{(\text{NO. OF INTEGRATED VARIABLES})_{\text{RIGID}}} \right)^{1.4}$$

Example Number	CPU Running Time (Sec)
2	1562
3	2217
4	2335
5	2943
6	2560

FIGURE 3-9 TOLA EXAMPLE RUN TIMES

4. EXAMPLES

This section describes the various test cases used to exercise the modified TOLA computer program. It is intended to illustrate actual program operation with emphasis on properly interpreting and incorporating the flexible body data associated with each test case.

A total of six examples are described. The first two cases are rigid body runs that do not include the effects of flexibility, while the remaining four cases employ the flexible body option. Associated with each example are listings of the input data and sample output. These data are shown in the appendix section. The input datafiles list all data required for each example. The TOLA computer program does not print the input data in this form since staging data are not printed until the stage is in operation. The output samples shown give the response data for several time points as printed by the program. All of the test cases are summarized in Figure 4-1.

EXAMPLE NUMBER	DATA	OBJECTIVE
1	AIRPLANE A RIGID AIRFRAME	COMPARE RESULTS WITH "AS RECEIVED" TOLA
2	AIRPLANE B RIGID AIRFRAME	REFERENCE RUN
3	AIRPLANE B SIMULATED "RIGID" AIRFRAME	CHECK OPERATION OF FLEXIBLE BODY OPTION
4	AIRPLANE B FLEXIBLE AIRFRAME FOUR MODES	OBTAIN "TYPICAL" FLEXIBLE AIRFRAME RESULTS
5	AIRPLANE B FLEXIBLE AIRFRAME EIGHT MODES	DETERMINE EFFECT OF HIGHER ORDER MODES
6	AIRPLANE B FLEXIBLE AIRFRAME FOUR MODES	EVALUATE EFFECTS OF AERODYNAMICS ON FLEXIBLE BODY RESPONSE

FIGURE 4-1 EXAMPLE RUN SUMMARY

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4.1 Rigid Body Examples - Two test cases were run without exercising the flexible body option using different sets of input data. The first set of data, denoted "Airplane A" in Figure 4-1, was originally supplied with the program. The purpose of this run was to check whether the capabilities of the original program had been altered by the addition of the flexible body option. The output from this run compared exactly with the original program results. As can be seen in the input data listing of Appendix D, setting the indicator INDFLX to zero is the only flexible body data required when running a rigid body case.

The second rigid body test case employed a new set of input data supplied by the NASA Langley Research Center. These data are denoted "Airplane B" in Figure 4-1. The program was first exercised as a rigid body run enabling the output to serve as a reference for comparing the effects of flexibility in later cases. Input data and sample output for this example are listed in Appendix E.

4.2 Flexible Body Examples - Four test cases were run to determine the effect that various parameters have on flexible body response. All flexible body data required by each run were taken from data supplied by NASA and shown in Figure 4-2. These data consist of a modal frequency, generalized mass, and modal deflections for sixteen free-free, normal modes. Several observations can be made that help in interpreting program input and results. Only modal deflections in the vertical (Z) direction are given. Consequently, there is no flexible body response in the X and Y directions. In addition, the mode shapes defined by the modal deflections are all symmetric from wing tip to wing tip. This results in a symmetric landing (simultaneous main gear touchdown) since all the rigid body data are also symmetric.

A brief description is given below for each flexible body example. Time history plots of several variables are also shown to illustrate the particular effect emphasized by the test case.

4.2.1 Simulated Rigid Body Run - To obtain results comparable to the rigid body data of Example 2, the flexible body option was first exercised with modal data simulating a stiff airframe. This was accomplished by using the modal deflections and generalized mass associated with the first four modes shown in Figure 4-2 but increasing the modal frequencies by a factor of 20.

MODE NUMBER	MODAL FREQ HZ	MODAL MASS SLUGS	NORMALIZED MODAL DATA - POSITIVE DOWN						
			PILOT STA.	NOSE GEAR	AERO DEF	AERO SLOPE	MAIN GEARS	ENGINE	TAIL
1	2.099	66.6617	+.1970	+.0800	-.1140	-4.239E-4	-.1000	-.0400	+.2030
2	2.628	79.4557	-.0385	-.0200	-.0414	3.643E-4	-.0042	+.1885	-.2440
3	4.784	70.8341	+.0035	-.1530	+.0405	-6.03E-4	+.1393	+.1380	-.1072
4	6.907	18.1131	+.0035	-.0650	+.0644	-3.034E-5	+.0112	-.0510	-.1250
5	7.671	20.0656	+.0254	+.0400	-.0342	-5.653E-5	-.0087	+.0111	+.1998
6	9.728	99.7316	+.3028	+.1850	-.0054	-1.351E-1	+.1200	+.0559	-.4409
7	11.797	70.4027	-.1673	-.0100	-.1258	3.716E-4	+.1050	+.0588	-.0165
8	13.878	31.6212	-.1157	+.0500	-.0323	-9.602E-4	-.0100	+.0350	-.2167
9	15.552	40.4199	+.0494	-.0300	-.0036	7.309E-4	+.0500	+.1025	+.2985
10	17.638	12.1885	-.0038	+.0050	-.0044	8.596E-7	+.0500	+.0100	+.0982
11	20.019	27.2611	+.0370	-.0500	-.0814	5.78E-4	-.0870	-.0200	-.3728
12	21.099	25.7565	+.0181	-.0350	-.0653	2.801E-4	+.0200	+.0075	-.0837
13	23.396	37.8456	+.0135	-.0500	+.0085	1.617E-4	.0000	+.0400	-.1269
14	23.969	39.6848	-.0180	+.0400	-.0009	-1.503E-4	+.0350	+.0250	-.2163
15	25.637	29.5837	-.0072	+.0150	+.0174	-1.417E-4	-.1300	-.0300	+.2243
16	25.694	8.2589	-.0023	+.0075	+.0044	-4.213E-5	-.0320	+.0050	+.0670

PILOT STATION X = 42.6667
 NOSE GEAR X = 35.08333
 MAIN GEARS X = -2.83867
 Y = \pm 8.3333
 Z = 0.509583

ENGINES X = -5.4722
 Y = \pm 14.1667
 TAIL X = -32.333

FIGURE 4-2 AIRPLANE B FLEXIBLE BODY DATA

Referring to the input data listing in Appendix F, each modal frequency and generalized mass are placed in arrays GFREQ and GMASS1 respectively. The vertical deflections for each landing gear attach point are in SZMOD. Since there are no other landing gear data, SXMOD and SYMOD are not input. Modal data for the aerodynamic reference point are contained in ARMODE. The aerodynamic weighting factors, PF, were not input, thus eliminating the effect of aerodynamic loads on flexible body response. Engine attach point modal data in the X direction is assumed zero; therefore, TXMOD is not input. Flexible body responses are output for four points on the aircraft, the pilot station, nose gear, right main gear, and tail. Modal data for these points are in OUTMOD, and their position vectors are defined in ROIS.

The output data from this run showed good agreement with that of Example 2, indicating that the flexible body option was operating properly. Differences in rigid body data between these two examples were not distinguishable on a graph; therefore, time history plots of these data are not given.

4.2.2 Flexible Body Run - Four Modes - The flexible body option was then run with the data described for Example 3 but using the actual modal frequencies defined in Figure 4-2. Output data from this run are shown graphically in Figures 4-3 through 4-6 and illustrate the effects of flexibility on aircraft response. These graphs demonstrate that for this example, flexibility has a more significant effect on landing gear dynamics than on rigid body response. It should be noted that the accuracy of all graphs in this section is limited by the time increment at which the data is plotted. Input data and sample output for this example are listed in Appendix G.

4.2.3 Flexible Body Run - Eight Modes - This test case was run to determine the effect of higher order modes on flexible body response. Airframe flexibility was represented by the modal data for the first eight modes of Figure 4-2. The input listing for this example in Appendix H shows the effect that increasing the number of modes has on the arrays associated with the flexible body data. Eight generalized masses and frequencies are shown in GMASS1 and GFREQ, and the size of all arrays containing modal deflections has been increased.

Figures 4-7 through 4-9 compare response data obtained by using four modes and then eight modes to represent airframe elasticity.

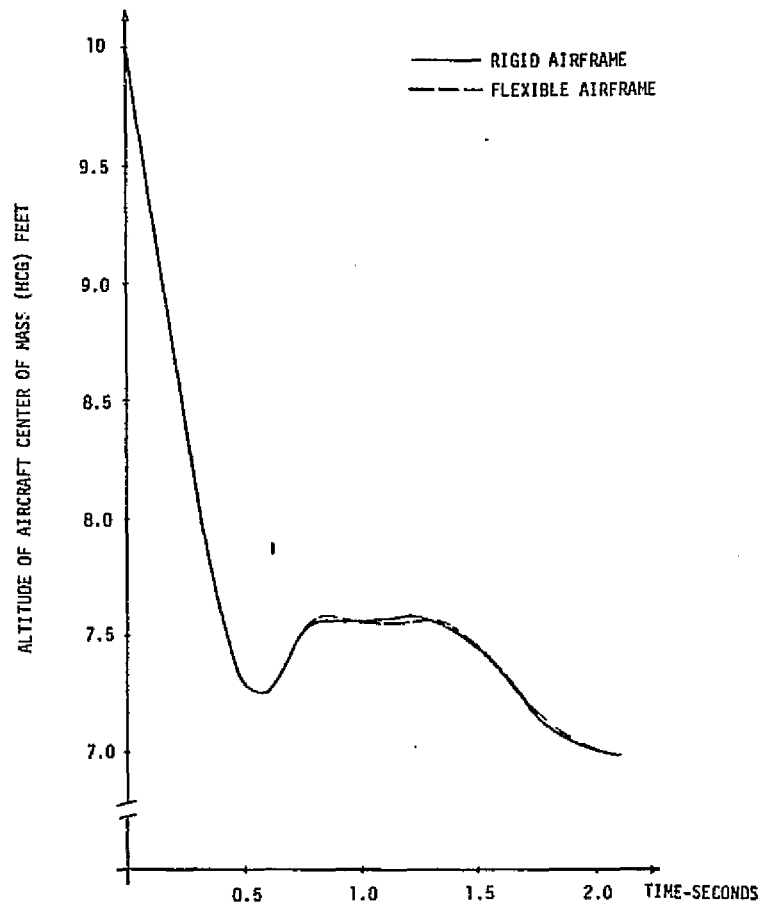


FIGURE 4-3 ALTITUDE OF AIRCRAFT CENTER OF MASS VS TIME

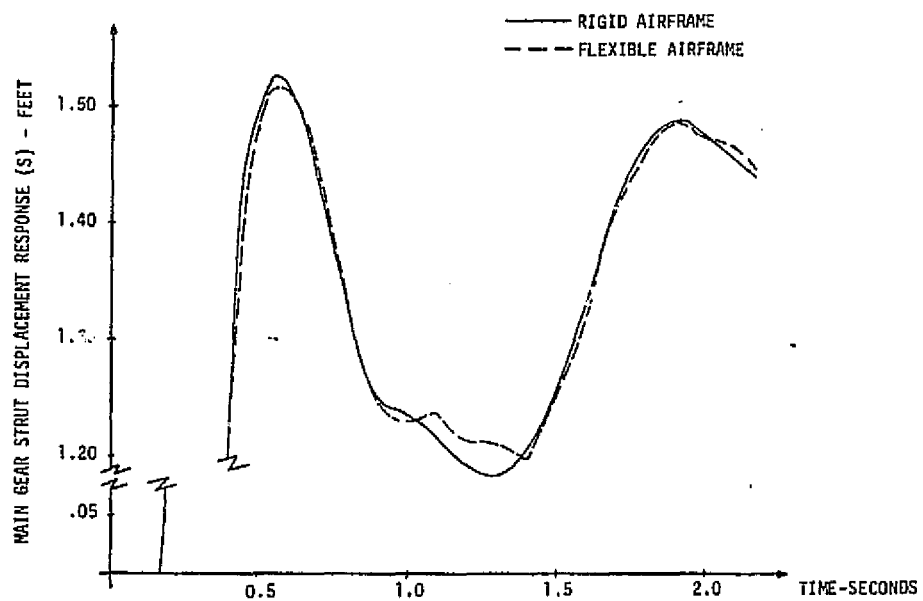


FIGURE 4-4 MAIN GEAR STRUT DISPLACEMENT VS TIME

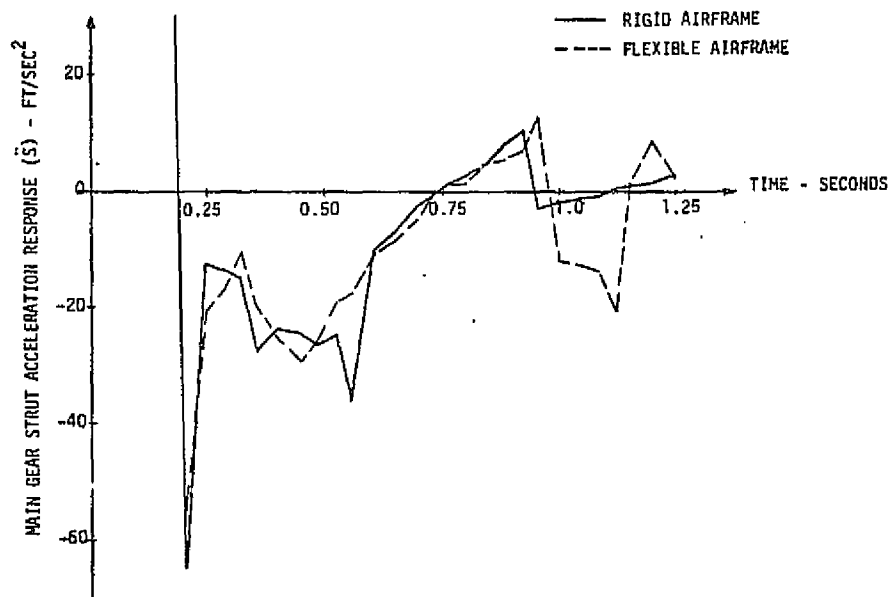


FIGURE 4-5 MAIN GEAR STRUT ACCELERATION VS TIME

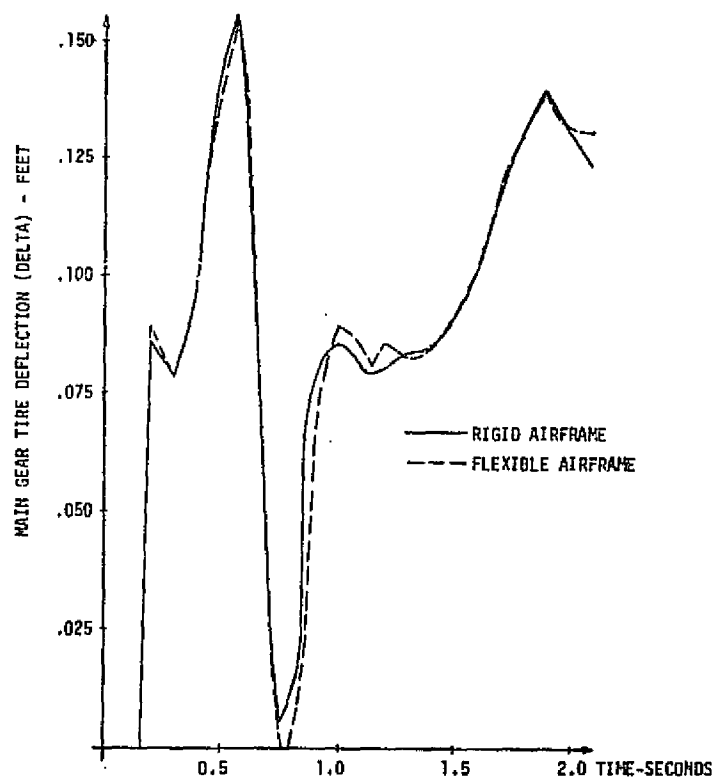


FIGURE 4-6 MAIN GEAR TIRE DEFLECTION VS TIME

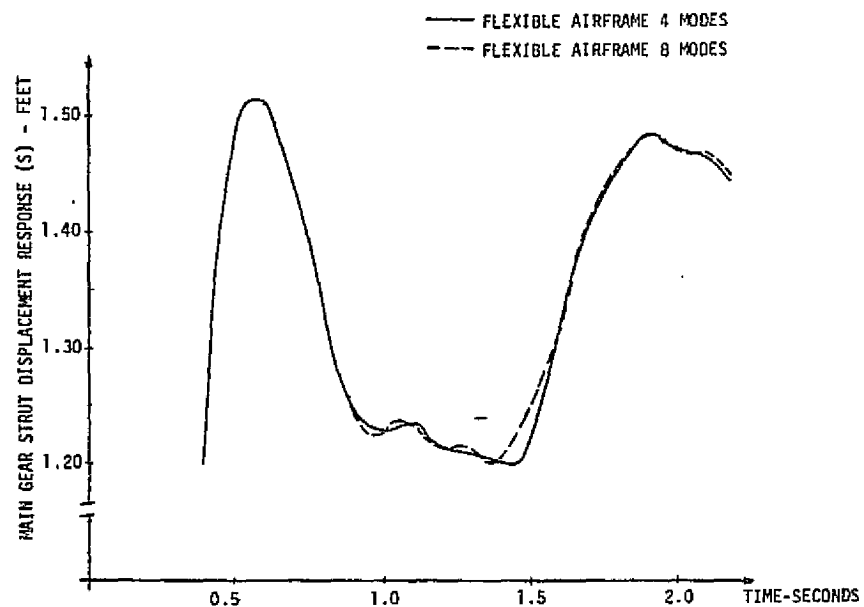


FIGURE 4-7 MAIN GEAR STRUT DISPLACEMENT VS TIME

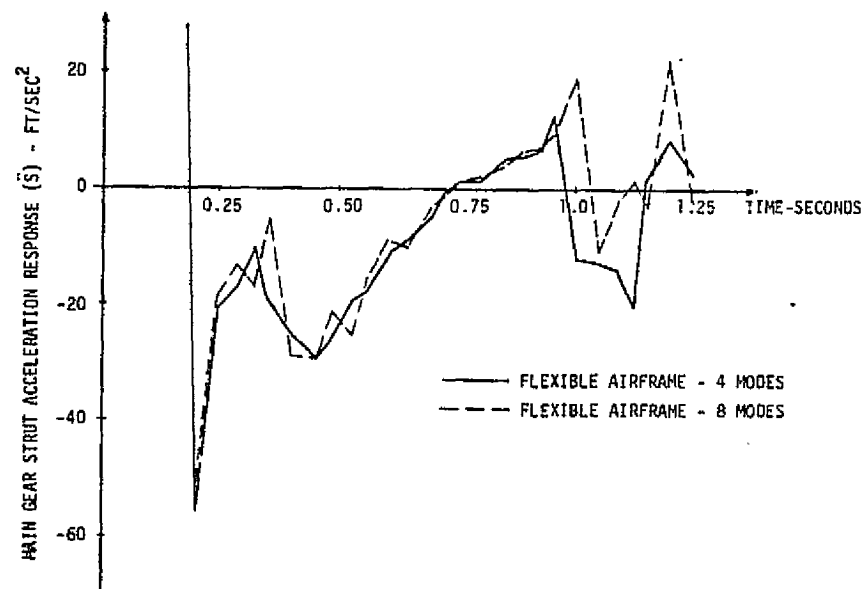


FIGURE 4-8 MAIN GEAR STRUT ACCELERATION VS TIME

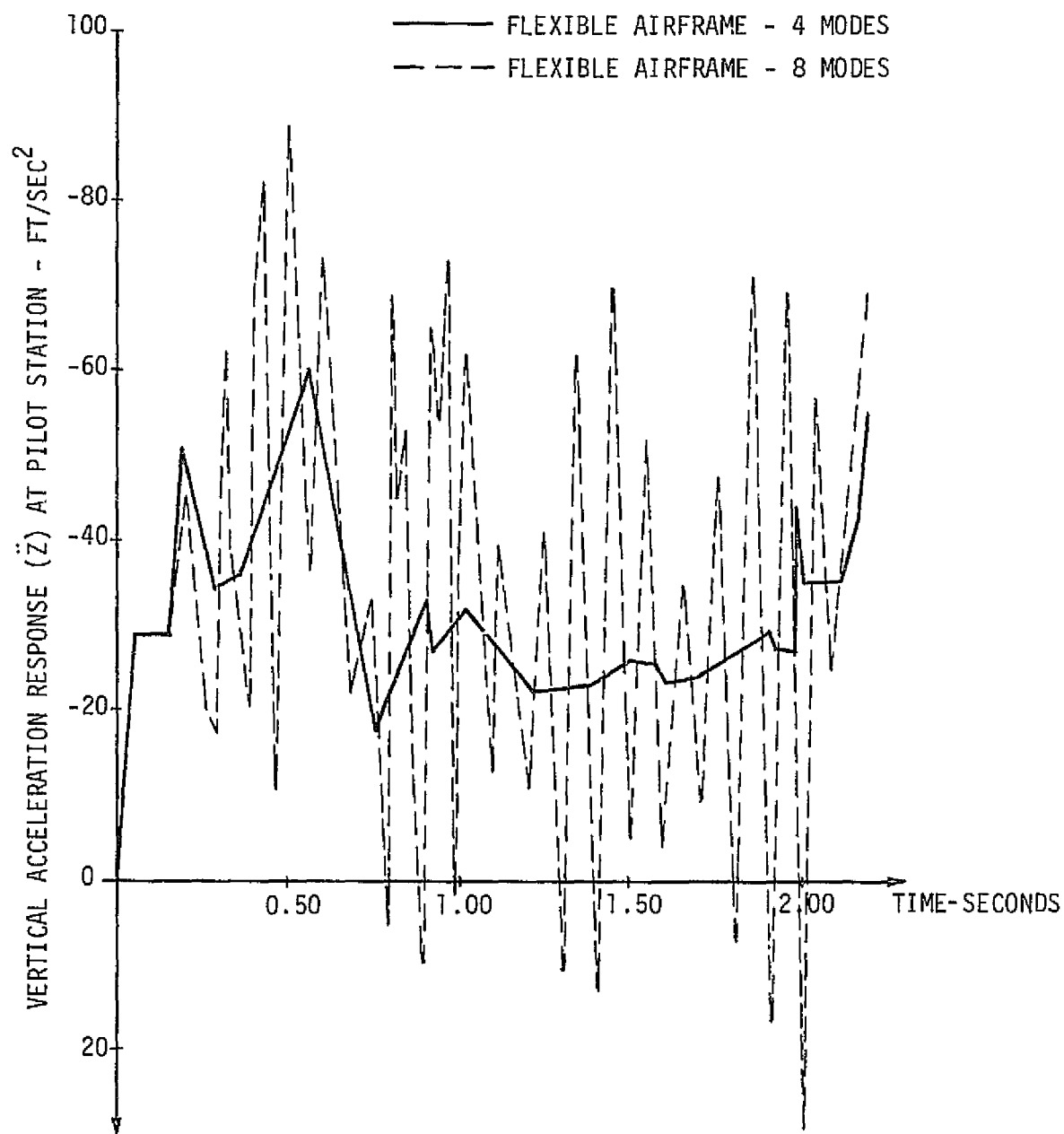


FIGURE 4-9 ACCELERATION RESPONSE AT PILOT STATION VS TIME

4.2.4 Flexible Body Run - Four Modes with Aerodynamic Weighting Factors - Aerodynamic weighting values or participation factors were calculated for each of the first four modes in Figure 4-2 and included in the program to determine the effect of aerodynamic loading on flexible body response. These weighting values were calculated by the method outlined in Appendix B assuming an elliptical spanwise lift distribution over the aircraft's wing. The resulting participation factors with their proper data format are shown with the rest of the flexible body data in the input listing for this example in Appendix I.

Figures 4-10 through 4-12 illustrate the effect that aerodynamic loading has on flexible body response for this airplane.

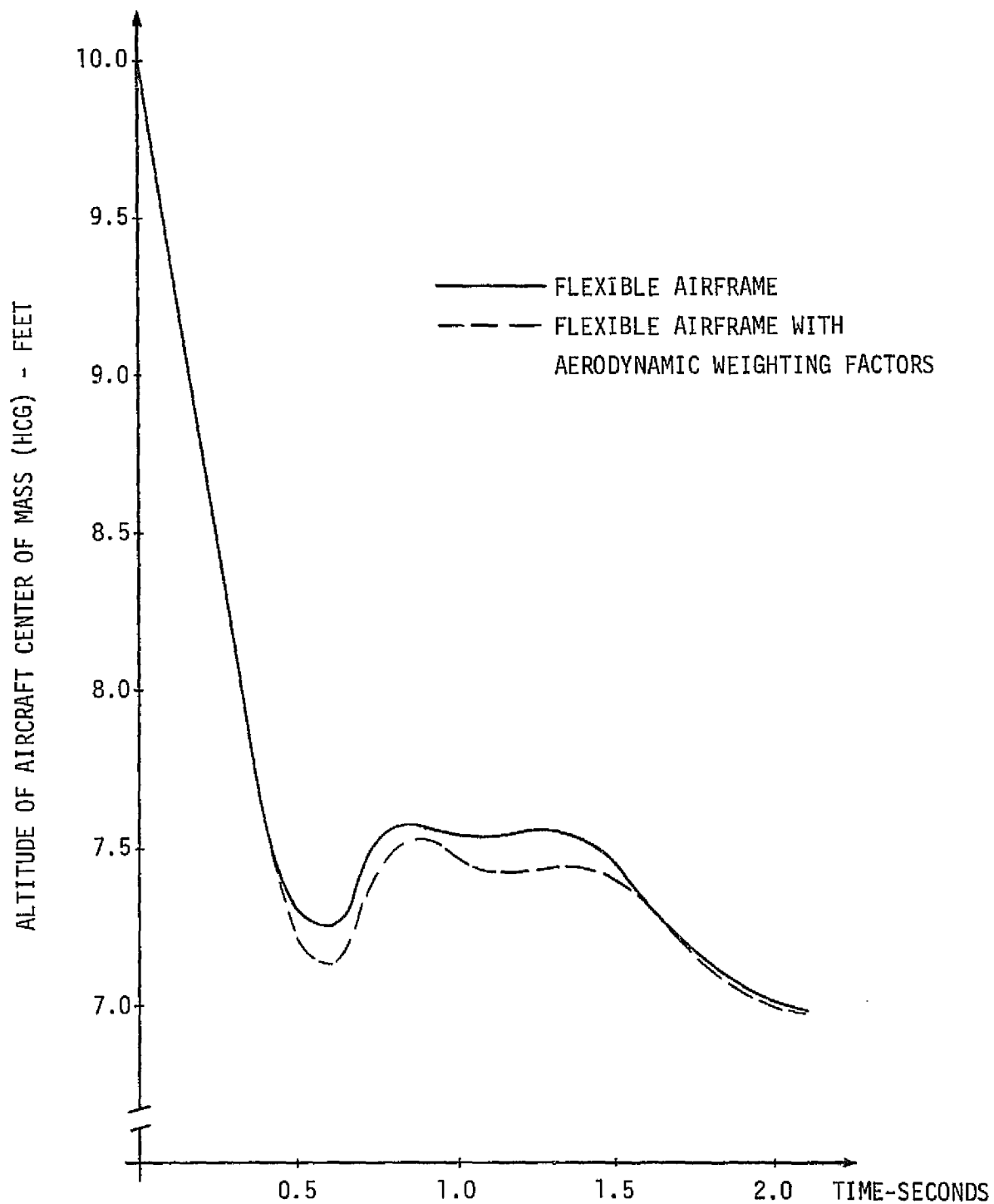


FIGURE 4-10 ALTITUDE OF AIRCRAFT CENTER OF MASS VS TIME

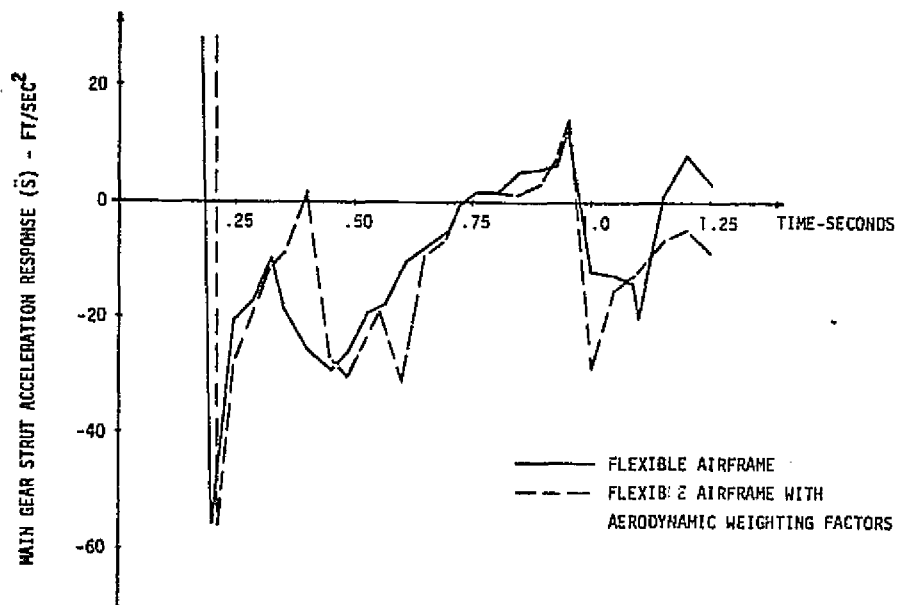


FIGURE 4-11 MAIN GEAR STRUT ACCELERATION VS TIME

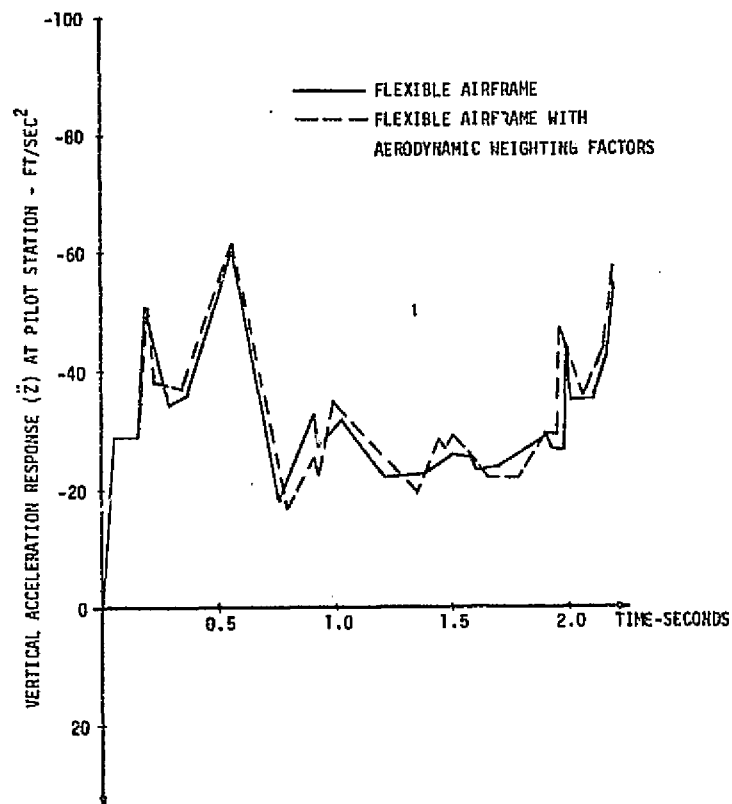


FIGURE 4-12 ACCELERATION RESPONSE AT PILOT STATION VS TIME

5. REFERENCES

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5. Dick, J. W. and Benda, B. J.: "Addition of Flexible Body Option to the TOLA Computer Program, Part II - User and Programmer Documentation", NASA CR-132732, October 1975

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APPENDIX A

PROGRAM LISTING - TOLA COMPUTER PROGRAM
WITH FLEXIBLE BODY OPTION

```

C OVERLAY (TOLA,0,0)
PROGRAM TOLA (INPUT, OUTPUT, TAPES=INPUT, TAPE6=OUTPUT,
1 TAP=13, TAP=16, TAP=31)
COMMON/TAADDIR/TABLE (800)
COMMON/READIR/DM1 (64), JBC, INXQ
CALL FTN3IN (1,0, DUMMY)
REWIND 13
C READ SUBROUTINE INITIALIZATION
JBC=-1
INXQ=0
1 CALL EXE
GO TO 1
END
SUBROUTINE EXE
C EXECUTIVE PROGRAM
DIMENSION IMTHD (1)
LOGICAL INDAHC, END, SKIPUP
LOGICAL STSMCH, TABSTP
COMMON /STOPIT/ STSMCH, TABSTP
COMMON /DI-COM/
* SKIPUP, HJ, T, TIMINT, DM1 (4),
* AMI, ICR, AMAXER,
* RELER1, DM7 (15), RELER2, DM2 (7), AINGRS (4), DM4 (46), TIMER, DM3 (64),
* AMAXH, DM11 (180), DECRES (4),
* DM13 (8), DELTS, DM14 (6), DLH1, DM15 (4),
* OLTH1, OLTH2, OLTH3, DM16 (18), EPS1, DM8,
* EPS11, LM21, EPS13, DM22 (12), EPS25,
* DM23, EPS3, DM24, EPS5, DM25,
* EPS7, DM26, EPS9, DM27 (25), GREFF,
* DM28 (17), HGC7F, DM29 (44),
* INDAHC, DM31 (2), INDAHC, DM32,
* INDAHC, INDAUT, DM33 (123), INDAHC, DM38 (34)
COMMON /DIR-COM/
* INDAHC, DM4, INDAHC, INDAHC, INDAHC, INDAHC,
* DM41 (2), INDAHC, INDAHC, DM42, INDAHC,
* DM43, INDAHC, DM44 (9),
* INDAHC, DM46 (3), DM47 (63), REP (30),
* RE77F, DM48 (28), RP77F, DM50 (14),
* DM51 (6), SIGN, DM52 (66), TIME, DM53 (2),
* TIMES, DM55 (3), TIMES, DM56, TL1,
* TL11, TL12, TL13, DM57 (127),
* PRIIT, DM58 (6), STGVAR (2), DM59 (13),
* DM60 (277), NSTRT, DM61 (49), IL, DM62 (215), ALPDES, DM61 (111),
* INDAHC, DM11 (151), DM11 (151),
COMMON/TA-RC/DM1 (11)
COMMON/EXLAUT/AUT1, SWT1, TIME1, ALPOD1, DUMM1 (5)
COMMON/LG/DM1 (7)
COMMON/AUTSAC/DM4 (4)
COMMON/AUTSAC/DM5 (5)
COMMON/LG/AUTS/DM6 (14)
COMMON/FLAUP/DM1 (6)
COMMON/AUTSAC/ALPJK1, DMESR, DUMM3 (4)
COMMON/HTCOM/HT1, HT2
COMMON/CONTR/CONTR1, CONTR2, CONTR3
LOGICAL SWT1, SWT2, SWT3
EQUIVALENCE (IMTHD, SKIPUP)
DATA STCOM2, STCOM3, BLANK/4HTMAX, 5HSTAGE, 6H
FORMAT (1H, 15X, 1.06/ (1H, 15X, 1.06))
FORMAT (1H, 15X, 4HSTOP)
FORMAT (1H, 15X, 16HSTAGE DATA ERROR)
FORMAT (1H, 15X, 11HSTAGE ON--2Ab)
FORMAT (1H, 15X, 5HSTOP- A6)
*****
INITIALIZATION BEFORE DATA READ FOR ALL SUBPROGRAMS.
*****

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35  DO 35 I=1,3959
36  INTHJ(I)=J
DO 36 I=1,3959
36  REM(I)=BLANK
DO 100 I=1,4
AINCRS(I)=BLANK
100  JECRES(I)=BLANK
DO 20 I=1,10
20  IOM4(I)=J
DO 21 I=1,63
21  IOM5(I)=J
DO 23 I=1,14
23  IOM6(I)=J
DO 24 I=1,648
24  IOM7(I)=J
CALL LGEAR1
CALL TFFS1
CALL VPCS1
CALL SACS1
CALL OPT1
CALL FLEX1
SWT2=.FALSE.
SWT3=.TRUE.
NSTAGE=1
INSTE=1
INDATH=1
SIGN=1.
AMAXH=1.E0
DELTS=.1
PRINT=.1
OLTM1=.0001
OLTM2=.0001
TIMER=0.
OLH1=1.
EPS1=1.
EPS2=1.
EPS3=1.
EPS4=1.
EPS5=1.
EPS6=1.
EPS7=1.
EPS8=1.
EPS9=1.
EPS10=1.
EPS11=1.
EPS12=1.
EPS13=1.
EPS14=1.
EPS15=1.
OMGR=7.23-115)8E-5
RE77F=2.320428.
RP77F=2.335965.
RELER1 = .00007
RELER2 = .000005
AMINER = .001
AMAXER=1.0000.
TIMINT = AMINER
OLTM3=.001
GRFF=32.174
C  AUTS SUBROUTINE INITIALIZATION
  SWT1=.TRUE.
  ALPG01=J.
C  AUTS - SACS SUBROUTINES INITIALIZATION
  ALPG1=J.
  QDCSR=J.
C  *****
C  POST DATA INITIALIZATION AND PRINT
C  *****
264  ICONTR=1
266  CALL OVERLAY(4LTOLA,1,.,6HRECALL)
266  CALL STGTSI
266  CALL DEF

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C INOSKP=J
H.=DELTS
IF (TIMINT .LT. AMINER) TIMINT = AMINER
CALL INPUZ
IF (SWT2) GO TO 302
C AUTS SUBROUTINE INITIALIZATION
ADDM1=ALPDES
TIME1=TIME
C
HT=DELTS
HT1=HT
HT2=HT
SWT2=.TRUE.
302 T=TIME
TL1=TIME
TL11=TIME
TL12=TIME
TL13=TIME
TIMX=TIME-TIMX
INJARC = HGC7F .GT. AMAXH
CALL LINES (12)
WRITE (6,1) (REM(I),I=1,30)
IF (INDVPG.EQ.0) GO TO 303
ICONT=4
CALL OVERLAY(4LTOLA,1,4,6HRECALL)
303 IF (INOTFF.EQ.0) GO TO 304
ICONT=2
CALL OVERLAY(4LTOLA,1,2,6HRECALL)
304 IF (INDALV.LN.0) GO TO 305
ICONT=3
CALL OVERLAY(4LTOLA,1,3,6HRECALL)
305 ICONT=5
CALL OVERLAY(4LTOLA,1,5,6HRECALL)
IF (INDLG.EQ.0) GO TO 306
ICONT=6
CALL OVERLAY(4LTOLA,1,6,6HRECALL)
306 SKIPUP=.TRUE.
CALL VPCC2
C POST DATA INITIALIZATION FOR SUBPROGRAMS
CALL LG=ARC
CALL OPT2
CALL FLX2
413 CALL OPT7
CALL SUFLGP
CALL OPT3
IF (INDAUT.EQ.0) GO TO 307
ICONT=2
CALL OVERLAY(4LTOLA,2,2,6HRECALL)
307 SKIPUP=.FALSE.
END = .FALSE.
TIMEA=DELTS+T-1.E-6
TIMEP=PRINT+T-1.E-6
*****
EXECUTIVE PROGRAM
*****
412 TPD = T+DELTS
IF (TPD .LT. TMAX) GO TO 413
DELTS = TMAX-T
H. = DELTS
END = .TRUE.
413 CALL HMIN(MIM)
IF (MIM.NE.0) GO TO 415
CALL SUFLGP
IF (INDSTL.EQ.0) GO TO 417
IF (END) GO TO 417

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C IF (INDSTG.NE..J) GO TO 417
  TIMEA=T+DELTS-1.E-6
  IF (T.LT.TIMEP) GO TO 414
  TIMEP=T+PRINT-1.E-6
  CALL OPT6
  IF (INDAUT.EQ..J) GO TO 416
  ICONTR=2
  CALL OVERLAY(4LTOLA,2,J,6HRECALL)
  GO TO 415
414 IF (INDAUT.EQ..J) GO TO 416
  ICONTR=1
  CALL OVERLAY(4LTOLA,2,J,6HRECALL)
  GO TO 415
415 CALL SDFLGP
  IF (T.LT.TMAX) END=.FALSE.
  IF (INDSTG.EQ..J) GO TO 417
  IF (END) GO TO 417
  IF (INDSTG.NE..J) GO TO 417
  CALL OPT3
  TIMEP=T+PRINT-1.E-6
  IF (T.LT.TIMEA) GO TO 416
  TIMEA=T+DELTS-1.E-6
  IF (INDAUT.EQ..J) GO TO 416
  ICONTR=2
  CALL OVERLAY(4LTOLA,2,J,6HRECALL)
  GO TO 415
417 CALL OPT6
  IF (INDAUT.EQ..J) GO TO 416
  ICONTR=2
  CALL OVERLAY(4LTOLA,2,J,6HRECALL)
416 IF (INDSTG.EQ..J) GO TO 744
  IF (END) GO TO 743
  IF (INDSTG.EQ..J) GO TO 412
  *****
  STAGING IS REQUIRED
  *****
511 INDSTG = J
  CALL LINES (2)
  WRITE (6,3) (STGVAR(I),I=1,2)
524 DO 225 JJ=1,4
  AINOPS(JJ)=BLANK
525 DECRS(JJ)=BLANK
  IF (INDSTF.EQ..J) GO TO 537
  INDSTF=L
  CALL LINES (2)
  WRITE (6,1.) STCOM3
  GO TO 744
537 INDUSKP=1
  CALL DEF
  ICONTR=1
  CALL OVERLAY(4LTOLA,1,L,6HRECALL)
  STAGE DATA IS READ - TEST MAJOR OR MINOR
C 543 INDUSKP=J
572 IF (INDSTY.NE..J) GO TO 631
  CALL STGT3I
  T=TIME
  MD=DELTS
  SKIPUP=.TRUE.
  IF (SWT3) GO TO 22
  IF (INDLG.NE..2) GO TO 22
  NDEFS=5*NSTRUT
  IF (IL.NE..J) NDEFS=3*NSTRUT
  CALL LNUPO(NDEFS)
  SWT3=.TRUE.
  IF (ISIGN(1,INDLG).GT.L) GO TO 416

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C SWI3=FALSE
  INDLG=-INJLG
  ICONTR=6
  CALL OVERLAY(4LTOLA,1,J,6HRECALL)
  CALL LGEAR2
  CALL LGEAR3
  CALL FLEX2
  GO TO 41.
601 INDSTY=2
  CALL DEF
  IF (INDSTR.EQ.3) GO TO 604
  INDSTR=J
  TIMSX=1
  NSTAGE=NSTAGE+1
604 IF (ISIGN(1,INDVPC).GT.0) GO TO 605
  CALL VPCS1
  INDVPC=-INDVPC
  ICONTR=4
  CALL OVERLAY(4LTOLA,1,J,6HRECALL)
605 IF (ISIGN(1,INDTFF).GT.0) GO TO 608
  CALL TFF3
  INDTFF=-INDTFF
  ICONTR=2
  CALL OVERLAY(4LTOLA,1,J,6HRECALL)
608 IF (ISIGN(1,INDAER).GT.0) GO TO 264
  CALL SAC31
  INDAER=-INDAER
  ICONTR=3
  CALL OVERLAY(4LTOLA,1,J,6HRECALL)
  GO TO 65+
743 CALL LINES (2)
  WRITE (6,1) STCOM2
C744 GENERAL STOP
744 CALL LINES (2)
  WRITE (6,3)
  STSNCH=TRUE.
  CALL LGEARP
  RETURN
END
SUBROUTINE INUPD (N,L)
  INTEGER L(1)
  COMMON/DIRCOM/SKIPUP(646),INDSTE(1245),OH(2068)
  COMMON/UPDCAL/ NUM , P( 90),Y( 90)
  IF (NUM+N .LE. 90) GO TO 5
  CALL DEF
  WRITE (6,700)
700 FORMAT(55H,NUMBER OF INTEGRATION VARIABLES EXCEEDS MAX LIMIT 90)
  STOP
  DO 2 I= 1,N
  NUM= NUM +1
20 L(I)= NUM
  RETURN
END
SUBROUTINE LNUPO(HN)
  COMMON/UPDCAL/ NUM,P(90),Y(90)
  NUM=NUM-HN
  RETURN
END
SUBROUTINE INPUZ
  COMMON/UPDCAL/ NUM,P(90),Y(90)
  NUM
  DO 10 I=1,90
  P(I) = 0.
  Y(I) = 0.
  RETURN

```

```

END
SUBROUTINE INTEG(K,XU)
COMMON/UPICAL/NUM,P(90),Y(90)
P(K) = XU
RETURN
END
SUBROUTINE UPDAT (JX1,JX2,XJ1,XJ2,XJ3,XJ4,XJ5)
COMMON/DIRCOM/SKIPUP,DM(645),INDSTE(1245),DM1(2068)
COMMON/UPICAL/NUM,P(90),Y(90)
LOGICAL SKIPUP
IF (SKIPUP) GO TO (200,201,202,203,204) ; JX1
GO TO (100,101,102,103,104) ; JX1
104 XJ5 = Y(JX2+4)
103 XJ4 = Y(JX2+3)
102 XJ3 = Y(JX2+2)
101 XJ2 = Y(JX2+1)
100 XJ1 = Y(JX2)
RETURN
204 Y(JX2+4) = XJ5
203 Y(JX2+3) = XJ4
202 Y(JX2+2) = XJ3
201 Y(JX2+1) = XJ2
200 Y(JX2) = XJ1
RETURN
END
SUBROUTINE MINIM(MIM)
LOGICAL SH
COMMON/DIRCOM/F,UX,X,STOPIT,IVAR84,SW,DM1(2),DXMIN,
*UXMAX,RELER1,DM2(5),RELER2,DM3(629),INDSTE,DM4(950),
*RTMIN,DM5(161),INDLG,DM6(151),DM7(2068)
COMMON/UPICAL/N,P(90),Y(90)
COMMON/HTCOM/HT,HT1,HT2
DIMENSION YMAX(90),YJ(90),PO(90),S(90),YP(90),Y1(90),Z(90),
GXK(90,3)
MIM=L
ACH=L
XF=X+DX
IF (IVAR84.NE. J) GO TO 360
XJ=X
DO 2 I=1,N
26 YMAX(I)=ABS(Y(I))
30 H=AMIN1(HT,HT1,HT2)
40 X=XJ
H=AMIN1(AJS(H),ABS(DXMAX))
DO 50 I=1,N
50 YJ(I)=Y(I)
CALL OPT7
CALL OPT4
IF (SW.OR.(INDSTE.EQ.)) GO TO 360
DO 60 I=1,N
60 PJ(I)=P(I)
Y(I)=YJ(I)+.5*H*PJ(I)
X=XJ+.5*H
CALL OPT7
CALL OPT4
IF (INDSTE.EQ.) GO TO 360
IF (SW.AND.(H.GT.STOPT)) GO TO 270
DO 80 I=1,N
80 S(I)=2.*PJ(I)+PJ(I)
Y(I)=YJ(I)+.5*H*P(I)
CALL OPT7
CALL OPT4
IF (INDSTE.EQ.) GO TO 360
IF (SW.AND.(H.GT.STOPT)) GO TO 270
DO 90 I=1,N

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90 S(I)=2.*P(I)+S(I)
   Y(I)=Y(I)+H*P(I)
   X=XJ+H
   CALL OPT7
   CALL OPT4
   IF(INSTE.EQ.3)GO TO 360
   IF(SW.AND.(H.GT.STOPT)) GO TO 270
   DO 100 I=1,N
100 Y(I)=Y(I)+H*(P(I)+S(I))/6.
110 X=XJ+0.25*H
   DO 120 I=1,N
120 Y(I)=Y(I)+J.25*H*P(I)
   CALL OPT7
   CALL OPT4
   IF(INSTE.EQ.0)GO TO 360
   IF(SW.AND.(H.GT.STOPT)) GO TO 270
   DO 130 I=1,N
130 S(I)=2.*P(I)+P(I)
   Y(I)=Y(I)+0.25*H*P(I)
   CALL OPT7
   CALL OPT4
   IF(INSTE.EQ.1)GO TO 360
   IF(SW.AND.(H.GT.STOPT)) GO TO 270
   DO 140 I=1,N
140 S(I)=2.*P(I)+S(I)
   Y(I)=Y(I)+0.5*H*P(I)
   X=XJ+0.5*H
   CALL OPT7
   CALL OPT4
   IF(INSTE.EQ.2)GO TO 360
   IF(SW.AND.(H.GT.STOPT)) GO TO 270
   DO 150 I=1,N
150 Y1(I)=Y(I)+0.5*H*(P(I)+S(I))/6.
   Y(I)=Y1(I)
   CALL OPT7
   CALL OPT4
   IF(SW.UR.(INSTE.EQ.0))GO TO 360
   DO 160 I=1,N
160 S(I)=P(I)
   Y(I)=Y1(I)+0.25*H*P(I)
   X=XJ+0.75*H
   CALL OPT7
   CALL OPT4
   IF(INSTE.EQ.3)GO TO 360
   IF(SW.AND.(H.GT.STOPT)) GO TO 270
   DO 170 I=1,N
170 S(I)=2.*P(I)+S(I)
   Y(I)=Y1(I)+0.25*H*P(I)
   CALL OPT7
   CALL OPT4
   IF(INSTE.EQ.0)GO TO 360
   IF(SW.AND.(H.GT.STOPT)) GO TO 270
   DO 180 I=1,N
180 S(I)=2.*P(I)+S(I)
   Y(I)=Y1(I)+0.5*H*P(I)
   X=XJ+H
   CALL OPT7
   CALL OPT4
   IF(INSTE.EQ.1)GO TO 360
   IF(SW.AND.(H.GT.STOPT)) GO TO 270
   R=C
   DO 190 I=1,N
   Y(I)=Y1(I)+0.5*H*(P(I)+S(I))/6.
   ERR=(Y(I)-YP(I))/15.
   Z(I)=AMAX1(YMAX(I),ABS(Y(I)))

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      R = 4MAX1( R,ABS(ERR) / 4MAX1( Z(I) ,1.0) )
      IF (RELER1 - R) 185,190,190
185  IF (ABS(H).GT.ABS(OXMIN)) GO TO 270
190  YMAX(I)=Z(I)
      IF (INDLG.NE.) CALL LGDET
      IF (SW) GO TO 360
205  XJ=XJ+H
      IF (ABS(XF-XJ).GT.1.E-10) GO TO 211
210  CALL OPT7
      CALL OPT4
      GO TO 360
211  IF (H.GT.PRIMIN) GO TO 212
      ACH=ACH+H
      IF (ACH.GE.PRIMIN) GO TO 213
      GO TO 220
213  CALL OPT7
      CALL OPT4
      HT=H
      CALL LINES(1)
      WRITE(6,700) HT
700  FORMAT(22H INTEG RTN.      HT = ,E15.8)
      HIM=1
      RETURN
212  ACH=0.
220  IF (R-RELER2) 230,230,240
230  H=H*H
240  IF (ABS(H).LE.ABS(XF-XJ)) GO TO 40
250  HT=H
      H=XF-XJ
      GO TO 40
270  H=.5*H
      DO 280 I=1,N
280  YP(I)=Y1(I)
      GO TO 10
300  KF=FIX(OX/OXMIN)
      H=OX/ABS(FLOAT(KF))
      K=
305  K=K+1
      DO 310 I=1,N
310  Y(I)=Y1(I)
      CALL OPT7
      CALL OPT4
      IF (SW.OR.(INCSTE.EQ.)) GO TO 360
      X=X+.5*H
      DO 320 J=1,2
      DO 320 I=1,N
      XK(I,J)=H*P(I)
320  Y(I)=Y(I)+.5*XK(I,J)
      CALL OPT7
330  CALL OPT4
      IF (INCSTE.EQ.) GO TO 360
      X=X+.5*H
      DO 340 I=1,N
      XK(I,3)=H*P(I)
340  Y(I)=Y(I)+XK(I,3)
      CALL OPT7
      CALL OPT4
      IF (INCSTE.EQ.) GO TO 360
      DO 350 I=1,N
350  Y(I)=Y(I)+(XK(I,1)+2.*(XK(I,2)+XK(I,3))+H*P(I))/5.
      IF (K.LT.KF) GO TO 305
      X=XF
      IF (INDLG.NE.) CALL LGDET
      CALL OPT7
      CALL OPT4

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00 CALL LIN=5(1)
   WRITE(6,75)HT
   RETURN
   END
   SUBROUTINE LGUET
   COMMON/UPD/CAL/NUN,P(9),Y(9)
   COMMON/LGUE/LA(25),FG2(5),P2(5),PRES(5),C(5),IPPT,LTPT
   COMMON/DI/LON/CH(646),INDSTE(675),NSTRUT,DM2(84),
   CA2(5),IL,S2T(5),LS2(5),
   COM(5),MASS2(5),DM5(34),ES(5),SB(5),DM4(131),IB(5),DM6(127),
   CINLG,DM7(151),DM8(268)
   COMMON/HTCON/HT,HT1,HT2
   REAL MASS2
   IF(INULG.EQ.2)RETURN
   DO 1, I=1,NSTRUT
   K=I+NSTRUT
   J=LA(K)
   KK=K-1
   JJ=LA(KK)
   LL=KK+2*NSTRUT
   LL=LA(LL)
   MM=K+2*NSTRUT
   MM=LA(MM)
   NN=LA(1)
   HT1=HT
76 IF(P(J))79,77,78
79 TTIME=Y(J)/ABS(P(J))
   IF(TTIME.GE.HT)GO TO 77
   HT1=TTIME
   GO TO 77
78 TTIME=(S2T(I)-Y(J))/P(J)
   GO TO 79
77 CONTINUE
   IF(Y(J).GT.(-ES(I)))GO TO 50
   WRITE(6,49)I,1,Y(J)
49 FORMAT(58X,4H-ES(,I1,10H) EXCEEDED/
   C58X,2H5(,I1,4H) = E15.7)
50 IF(Y(J).LE.ES(I))GO TO 51
   IF(Y(J).LE.(S2T(I)-ES(I)))GO TO 55
   IF(Y(J).LE.(SB(I)+LS(I)))GO TO 52
   WRITE(6,53)I,1,Y(J)
53 FORMAT(58X,4H-ES(,I1,10H) EXCEEDED/
   C58X,2H5(,I1,4H) = E15.7)
52 IF(Y(JJ).LE.L.)GO TO 20
   Y(JJ)=0.
   P(J)=0.
20 IF(P(JJ).LT.L.)GO TO 55
   P(JJ)=0.
   GO TO 55
51 IF(Y(JJ).GE.L.)GO TO 21
   Y(JJ)=0.
   P(JJ)=0.
21 IF(P(JJ).LT.C.)P(JJ)=1.
55 CONTINUE
   IF(IL.NE.J)GO TO 61
   HT2=HT
   IF(P(MM))86,87,88
86 TTIME=Y(MM)/ABS(P(MM))
89 IF(TTIME.GE.HT)GO TO 87
   HT2=TTIME
   GO TO 87
88 TTIME=(S2T(I)-Y(MM))/P(MM)
   GO TO 89
87 CONTINUE
   IF(Y(MM).GT.(-ES2(I)))GO TO 58

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57 WRITE(6,57)I,I,Y(MM)
   FORMAT(31X,5A-E52(,11,10H) EXCEEDED/
C58X,3HS2(,11,4H) = E15,7)
58 IF(Y(MM).LE.E52(I))GO TO 61
   IF(Y(MM).LE.(S2(I)-E52(I)))GO TO 61
   IF(Y(MM).LE.(S2(I)+E52(I)))GO TO 62
   WRITE(6,53)I,I,Y(MM)
63 FORMAT(58X,5H-E52(,11,10H) EXCEEDED/
C38X,3HS2(,11,4H) = E15,7)
62 IF(Y(LL).LE.0.)GO TO 22
   Y(LL)=0.
   P(MM)=0.
22 IF(P(LL).LT.0.)GO TO 61
   GO TO 14.
61 IF(Y(LL).GE.0.)GO TO 23
   Y(LL)=0.
   P(MM)=0.
23 IF(P(LL).GE.0.)GO TO 61
140 P(LL)=0.
60 CONTINUE
   IF(I0(I).NE.(-1))GO TO 10
   P(MM)=0.
   Y(MM)=0.
10 CONTINUE
   RETURN
END
SUBROUTINE STGTS1
LOGICAL SH
COMMON /DIRCCM/
*COMVAL(5) , SH(19) , AINCPS(4) , DM2(292) , DECRES(4) , DM3(510),
*STEST ( 4) , STESTD(4) , DM4(187) , STGVAR(4) , DM5(543),
*ISTAGE,DM1(314),DM7(2168)
COMMON/STGT/ICOUNT,KCOUNT,LOCAIN(4),LOCADE(4)
COMMON/CONTR/ICONT1,CONTR1,ICONT2,ICONT3
DATA BLANK/1H /
ICOUNT = 0
KCOUNT = 0
DO 1 I=1,4
IF (AINCR5(I) .EQ. BLANK) GO TO 15
ICONT1=8
CONTR1=AINCR5(I)
CALL OVERLAY(4LTOLA,1,3,6HRECALL)
LOCAIN(I)=ICONT2
IF (ICONT3.EQ.0.)GO TO 12
WRITE (6,11) AINCPS(I)
11 FORMAT (26H ERROR,THE STAGE VARIABLE **A6,
* 26H** IS NOT IN THE DIRECTORY/24HU...LOOKING FOR NEW CASE)
CALL EXERR(1)
RETURN
ICOUNT = ICOUNT+1
12 CONTINUE
DO 2 I=1,4
IF (DECRES(I) .EQ. BLANK) GO TO 21
ICONT2=8
CONTR1=DECRES(I)
CALL OVERLAY(4LTOLA,1,0,6HRECALL)
LOCADE(I)=ICONT2
IF (ICONT3.EQ.0.)GO TO 24
WRITE (6,11) DECRES(I)
CALL EXERR(1)
RETURN
24 KCOUNT = KCOUNT+1
23 CONTINUE
21 RETURN
END

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DATA MAXT/115/
DO 1000 I=1,MAXT
IF (SYH2.NE. STABLE(I) ) GO TO 1000
JM=1
DO 500 J=1,N2
LOC2(J) = LOCS(JM)
500 JM=JM+1
IER = -1
RETURN
1000 CONTINUE
IER = 1
RETURN
END
SUBROUTINE ASPCH(LOC1,SYH1)
COMMON/TABCOM/LOCS(115),STABLE(115)
DATA BLANK,MAXT/1H ,115/
DO 2000 I=1,MAXT
IF (LOC1.NE. LOCS(I)) GO TO 2000
SYH1 = STABLE(I)
RETURN
2000 CONTINUE
SYH1 = BLANK
RETURN
END
SUBROUTINE DEF
C TITLE PRINT ROUTINE
COMMON /GITCOM/ D1(24), INDSOF , D2(19) , LONG , NCASE , NPAGE ,
NSTAGE,D3(12,4),D4(2,8)
930 FORMAT(1H,3X,7H SIX DEGREES OF FREEDOM FLIGHT PATH STUDY/
*1H ,42X,28H GENERALIZED COMPUTER PROGRAM/
*1H,28X,7H INDSOF I2,5X,5H CASE A6,7X,
36H NSTAGE I2,5X,5H NPAGE I6,1H )
NPAGE=NPAGE+1
LONG=J
WRITE(6,900) INDSOF,NCASE,NSTAGE,NPAGE
RETURN
END
SUBROUTINE STFL(JOPT,N,ARG1)
C GENERAL PRINT ROUTINE
LOGICAL CLEAN,INTEG
COMMON/CLEAUP/I2,CLEAN,INTEG
COMMON/STOFA/ARG(48),ALIST(8),GETARG(8),NENT,LENT,K
DIMENSION ARG1(1)
IF(JOPT.EQ.1)GO TO 5
IF(JOPT.EQ.3)GO TO 6
DO 4 I=1,N
4 ARG(I)=ARG1(I)
5 IF(JOPT-1)1,2,3
NENT=1
IF(I2.EQ.1)RETURN
CLEAN=.TRUE.
CALL ARRAY(N,1)
RETURN
C
2 NENT=2
K=1
CALL ARRAY(N,6)
RETURN
C
3 NENT=4
K=1
CALL ARRAY(N,J)
RETURN
6 GETARG(1)=ARG1(1)
NENT=5

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K=2
CALL ARRAY(N,C)
RETURN
END
BLOCK DATA STFLD
COMMON/CL=AUP/I2,CLEAN,INTEG
LOGICAL CLEAN,INTEG
DATA I2,CLEAN,INTEG/.,.TRUE.,.FALSE./
END
SUBROUTINE STOVAR(N,A,B,C,D,E,F,G,H)
COMMON/STORA/ARG(48),ALIST(8),GETARG(8),NENT,LENT,K
IF (IABJ(N).LE.2)GO TO 2
IF (IABC(N).LE.4)GO TO 1
GETARG(3)=H
GETARG(7)=G
GETARG(6)=F
GETARG(5)=E
1 GETARG(4)=D
2 GETARG(3)=C
GETARG(2)=B
GETARG(1)=A
NENT=2
K=2
CALL APRAY(N,C)
RETURN
END
SUBROUTINE ARRAY(N,IOPT)
LOGICAL CLEAN,INTEG
COMMON/CL=AUP/I2,CLEAN,INTEG
COMMON/STORA/ARG(48),ALIST(8),GETARG(8),NENT,LENT,K
705 FORMAT(5X,18,7I15)
710 FORMAT(7X,A6,7(9X,A6))
715 FORMAT(1X,8(1PE15.7))
720 FORMAT(1X)
IF (IOPT.NE.0)GO TO 2005
IF (NENT.EQ.LENT)GO TO 1010
IF (I2.LQ.0)GO TO 1005
CLEAN=.TRUE.
GO TO 2005
1005 CALL LINES (1)
WRITE (6,720)
IF (NENT.EQ.1) RETURN
1010 INTEG = (N.LT.0)
NMAX=IABJ(N)
LENT=NENT
J=1
GO TO 500
C
C CLEAN OUT ARRAY
2005 CALL LINES (1)
IF (LENT.GE.4) GO TO 2015
IF (INTEG) GO TO 2035
WRITE (6,715) (ALIST(I),I=1,I2)
GO TO 2025
2025 WRITE (6,705) (ALIST(I),I=1,I2)
GO TO 2025
2015 WRITE (6,710) (ALIST(I),I=1,I2)
2020 I2=0
IF (.NOT.CLEAN)GO TO 500
CLEAN=.FALSE.
GO TO 1005
C
C DEVELOP ARRAY
C
701 ALIST (I2) = GETARG (J)

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C  GO TO 520
510 ALIST (I2) = ARG (J)
520 J=J+1
    IF (I2.EQ. 4) GO TO 2000
530 IF (J.GT.NMAX) RETURN
    I2=I2+1
    GO TO (510,500),K
END
SUBROUTINE LTNLS(LCOUNT)
C  LINLS ACCOUNTING ROUTINE
COMMON /UIRCOM/01(663),LONG,02(1227),03(2068)
LONG=LONG+LCOUNT
IF (LONG.LE.51) RETURN
CALL OLF
LONG=LCOUNT
RETURN
END
FUNCTION ASIN(X)
EXTERNAL ACOS
ASIN=1.5707963-ACOS(X)
RETURN
END
FUNCTION ACOS(X)
IF (ABS(X).GT. 1.) GO TO 130
IF (ABS(X).GT. 7.4505806E-09) GO TO 50
ACOS=1.5707963
RETURN
50 IF (X.NE. 1.) GO TO 40
ACOS=0.
RETURN
40 IF (X.NE. (-1.)) GO TO 30
ACOS=3.1415926
RETURN
30 A=X
X1=X
DO 20 I=1,27
IF (X1.GT. 0.) GO TO 10
SA=1.
X2=1.-(2.*X1**2)
GO TO 5
10 SA=X1
X2=(2.*X1**2)-1.
A=A+SA*2.**(-(I-1)-1)
X1=X2
20 ACOS=3.1415926*A
RETURN
100 WRITE (6,200)X
210 FORMAT(26H,ARGUMENT OUT OF RANGE X =E2J.0)
ACOS=99999999.
RETURN
END
FUNCTION ATANL (Y,X)
C  *****
C  SINGLE PRECISION FORTRAN ARCTANGENT FUNCTION SUBROUTINE
C  NOTE. ----- ZERO ARGUMENTS WILL EXIT WITH ZERO ANSWER
C  *****
LOGICAL INVIC
REAL L
DIMENSION AA(6),A(4),B(4),PN(4)
DATA (AA(I), I=1,6) /
C  MIN IS AA(1), MAX IS AA(6)
* .18020451E-8, .176326981E+0, .577350269E+0, .119175359E+1,
2 .274747742E+1, .134217728E+9 /
DATA (A(I), I=1,4) /
* .449587214E+J, .195014224E+0, .944754986E-1, .288535059E-1 /

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DATA (U(I), I = 1,4) /
.1398857E+1, .39645266E+0, .218181818E+0, .168724015E+0 /
DATA (PN(I), I = 1,4) /
.3496585E+0, .698131701E+0, .104719755E+1, .139626340E+1 /
DATA C1, C2, C3, L /
.51113459E-1, .270998425E-2, .216649136E+0, .163636364E+0 /
DATA P10V2, ONEPI /
.15717363E+1, .314159265E+1 /
IF (Y.EQ. 0.0) GO TO 16
IF (X.EQ. 0.0) GO TO 15
INDIC = (X.LT. 0.0)
C INDIC = .TRUE., ANGLE IS IN QUADRANT 1 OR 4
R = Y/X
9 Z = ABS(R)
DO 10 I = 1,6
IF (Z-AA(I).LT. 0.0) GO TO (18,12,11,11,11,11),I
10 CONTINUE
GO TO 17
11 I = I - 2
J = 6 - I
P = PN(I)
Z = A(I) - B(I)/(Z + AA(J))
GO TO 13
12 Z = Z*L
J = 5 - I
P = P*2 + C2 - C2/((Z**2) + C1)
ATAN2 = Z/I + P
14 ATAN2 = SIGN(ATAN2,R)
19 IF (.NOT. INDIC) RETURN
IF (ATAN2.GT. 0.0) GO TO 23
ATAN2 = ATAN2 + ONEPI
RETURN
15 ATAN2 = SIGN(P10V2,Y)
RETURN
16 IF (X.GE. 0.0) GO TO 22
ATAN2 = ONEPI
RETURN
17 ATAN2 = P10V2
GO TO 14
18 ATAN2 = R
GO TO 19
22 ATAN2 = 0.0
RETURN
23 ATAN2 = ATAN2 - ONEPI
RETURN
END
C SUBROUTINE ERRPR(LOC)
GENERAL TABLE ERROR ROUTINE
COMMON /DIRCOM/ DM(5), SW(641), INDSTE, DM1(1244),DM2(2068)
DATA IUL / 1H /
INDSTE=J
CALL LINES (2)
CALL ASRCH(LOC,NAME)
IF (NAME.EQ. IUL) GO TO 5
WRITE (6,1) NAME
RETURN
5 WRITE (6,2)
1 FORMAT (14HSTABLE ERROR ,A6)
2 FORMAT (12HSTABLE ERROR/1H ,47H...LOCATION OF TABLE NOT LISTED IN
10IRECTORY...)
RETURN
END
C SUBROUTINE EXERR(NUM)
COMMON /DIRCOM/ DM(5), SW(641), INDSTE, DM1(1244),DM2(2068)

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0 INOSTE = 4
IF (NDM.EQ.0) RETURN
CALL STFL(1,1,DU)
CALL LINES(3)
WRITE(6,3) NUM
3 FORMAT(1HA,15X,12HSTOF NUMBER I3)
RETURN
END
SUBROUTINE NOTLU (ND,NA,X,Z,XA,ZR,IE)
      N-DIMENSION TABLE LOOK-UP ROUTINE
      ND      DIM. OF LOOK-UP
      NA      NUMBERS OF VALUES OF EACH TABLE
      X      TABLES OF EACH X IN ORDER
      Z      FUNCTION VALUES
      XA      ARRAY OF ARGUMENTS
      ZR      RESULT
      IE      ERROR RETURN
      0      NO ERROR
      -1     X ARRAY TO SMALL
      1      X ARRAY TO LARGE
      2      ARRAY NOT ASCENDING ORDER
      WJ(2**MAX(N))
      DIMENSION X(1),Z(1),NA(1),XA(1),NS(8),WJ( 32)
      IE=0
      L1=2
      LF=NO-1
      DO 3 I=1,LF
      L2=L1+NA(I)-2
      FIND=0
      DO 4 J=L1,L2
      IF(X(J).GT.X(J-1)) GO TO 5
      IE=2
      RETURN
6 IF(FIND.NE.0) GO TO 4
IF (XA(I)-X(J-1)) 8,4,4
8 IF (J.GT.L1) GO TO 13
IE=-1
RETURN
10 FIND=1
NS(I)=J-2
4 CONTINUE
IF (FIND) 11,12,11
12 IF (XA(I)-X(L2)) 13,13,14
14 IE=1
RETURN
13 NS(I)=L2-1
11 L1=L2+2
3 CONTINUE
KF=2**LF
MW=-2
DO 18 I=1,KF,2
L1=J
IZ=J
MW=MW+2
NPT=1
DO 19 J=1,LF
MW=2**(J-1)
IF (AND(MW,MW).EQ.0) GO TO 22
N=NS(J)+1
GO TO 23
22 N=NS(J)
23 N=N-L1
L1=L1+NA(J)
IZ=NPT*(N-1)+IZ
NPT=NPT*NA(J)

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18  WJ(I)=Z(I2+1)
    WJ(I+1)=Z(I2+2)
    LI=1
    DO 32 I=1,LF
    M=NS(I)
    PER=(XA(I)-X(M))/(X(M+1)-X(M))
    JF=KF/L
32  WJ(J)=WJ(2*J-1)+(WJ(2*J)-WJ(2*J-1))*PER
    Z3=WJ(1)
    RETURN
END
SUBROUTINE ATMS (HGC7F)
C     ATMOSPHERE CALCULATION ROUTINE
    LOGICAL HGT9, EVLN
    DIMENSION H3(11), RHONH(11), PB(11), TB(11), AK1(11), AK2(11), AK3(11),
1A(2), B(2), C(2), D(2)
    COMMON /CIRGMA/
    DIMENSION AMJA7F, DM1(324), INDATA, DM2(132), PA77P,
2DM3(95), DM4(89), TA77R, DM5(8), VS77F,
3DM6(946), DM7(2J68)
C
C     ALTITUDE, DENSITY, PRESSURE, TEMPERATURE, /
    DATA (H3(I), I=1, 11)/, 1.1E4, 2.5E4, 4.7E4, 5.3E4, 7.9E4,
    G3.E4, 1.0E5, 1.6E5, 1.7E5, 2.0E5,
    DATA (RHONH(I), I=1, 11)/2.3769E-4, 7.762E-4, 7.765E-5,
    C2.88E-5, 1.3946E-7, 4.1189E-8, 4.261E-9, 2.232E-10,
    C1.845E-12, 1.338E-12, 6.113E-13,
    DATA (PB(I), I=1, 11)/2.116, 2.1695, 472.73, 51.979, 2.5155,
    C1.2161, 2.1.8E-2, 1.8.9E-4, 15.562E-5, 75.578E-7,
    C58.954E-7, 6.9.7E-7,
    DATA (TB(I), I=1, 11)/518.688, 389.988, 389.988, 508.788,
    C50.188, 238.188, 298.188, 416.188, 2386.188,
    C2566.188, 2836.188,
    DATA (AK1(I), I=1, 11)/-.225569E-4, 0., .138466E-4, 0.,
    C-.159E-4, ., .241458E-4, .886289E-4, .754341E-5,
    C-.3271E-5, .222129E-5,
    DATA (AK2(I), I=1, 11)/-.25612, 0., 11.3883, 0., -.7.59218,
    C., 8.5412, .7.224, 3.41648, 6.83296, 9.76137,
    DATA (AK3(I), I=1, 11)/., .157689E-3, 0., .126869E-3,
    C., .206234E-3, .5E-4,
    DATA A(1), A(2), B(1), B(2), C(1), C(2), D(1), D(2)/.759511, .935787,
    C.174164, .273966, 22., 18., 25., 140./
C
    IF ((INDATA.EQ.0).OR.(HGC7F.GE.2.5E6)) GO TO 470
    IF (HGC7F.LE.0.) GO TO 460
    TMP=.3.48*HGC7F
    HGP=TMP/(1.+TMP/6356766.)
    HGT9=.TRUL.
    M=2
    IF (HGP.GT.180000.) GO TO 49
    M=1
    IF (HGP.GT.30000.) GO TO 49
    HGT9=.FALSE.
C SEARCH FOR LAYER
49  IF (HGP.LT.HB(11)) GO TO 50
    LAY=11
    GO TO 50
50  DO 55 I=2, 11
    IF (HGP.GT.HB(I)) GO TO 55
    LAY=I-1
    GO TO 50
55  CONTINUE
60  TMP=HGP-H3(LAY)
    TMP2=1.+AK1(LAY)*TMP

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69 IF (LAY.GT.6) GO TO 69
70 IF (2*(LAY/2).NE.LAY) GO TO 69
EVEN=.TRUE.
GO TO 71
EVEN=.FALSE.
TA77R=TB(LAY)*TMP2
IF (EVEN) GO TO 72
PA77P=PB(LAY)*TMP2*(-AK2(LAY))
RHOAS=RHO(LAY)*TMP2*(-1.-AK2(LAY))
GO TO 80
72 TMP3=EXP(-AK3(LAY)*TMP)
PA77P=PB(LAY)*TMP3
RHOAS=RHO(LAY)*TMP3
80 IF (HGT.9L) GO TO 85
STA77R=SQRT(TA77R)
VS77F=49.2576*STA77R
ANUA7F=.226988E-6*(TA77R*STA77R/((TA77R+198.72)*RHOAS))
RETURN
85 VS77F=.
ANUA7F=.
TA77R=TA77R*(A(M)-B(M)*ATAN(HGP-C(M)/D(M)))
RETURN
460 VS77F=1115.43372
TA77R=TB(1)
PA77P=PB(1)
ANUA7F=1.5723288E-4
RHOAS=RHO(1)
RETURN
471 VS77F=.
TA77R=.
PA77P=.
ANUA7F=.
RHOAS=.
RETURN
END
C SUBROUTINE INVR3(A,B,INDER)
A 3 X 3 MATRIX INVERSION ROUTINE
DIMENSION A(3,3),B(3,3)
Q(1,1)=A(2,2)*A(3,3)-A(2,3)*A(3,2)
Q(1,2)=A(3,2)*A(1,3)-A(1,2)*A(3,3)
Q(1,3)=A(1,2)*A(2,3)-A(2,2)*A(1,3)
Q(2,1)=A(1,3)*A(2,3)-A(2,3)*A(1,3)
Q(2,2)=A(1,1)*A(2,3)-A(2,3)*A(1,1)
Q(2,3)=A(1,1)*A(3,3)-A(3,3)*A(1,1)
Q(3,1)=A(2,1)*A(3,3)-A(3,3)*A(2,1)
Q(3,2)=A(2,1)*A(1,3)-A(1,1)*A(2,2)
Q(3,3)=A(1,2)*A(2,2)-A(1,2)*A(2,1)
IF (ABS(Q).LE.1.E-18) GO TO 14
B(2,1)=A(3,1)*A(2,3)-A(3,3)*A(2,1)
B(2,2)=A(1,1)*A(3,3)-A(3,1)*A(1,3)
B(2,3)=A(2,1)*A(1,3)-A(1,1)*A(2,3)
B(3,1)=A(2,1)*A(3,3)-A(3,1)*A(2,2)
B(3,2)=A(3,1)*A(1,2)-A(1,1)*A(3,2)
B(3,3)=A(1,2)*A(2,2)-A(1,2)*A(2,1)
DO 17 J=1,3
DO 17 I=1,3
B(I,J)=B(I,J)/Q
INDER=1
RETURN
19 INDER=2
RETURN
END
C SUBROUTINE MULT31(A,B,C)
A MATRIX MULTIPLICATION ROUTINE
DIMENSION A(3,3),B(3,3),C(3)
DO 1 I=1,3
C(I)=.
DO 1 J=1,3

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      C(I)=C(I)+A(I,J)*B(J)
      RETURN
    END
C
SUBROUTINE MULT33(A,B,C)
  A 3 X 3 MATRIX MULTIPLICATION ROUTINE
  DIMENSION A(3,3),B(3,3),C(3,3)
  DO 1 I=1,3
  DO 1 J=1,3
  C(I,J)=0
  DO 1 K=1,3
  C(I,J)=C(I,J)+A(I,K)*B(K,J)
  1 RETURN
  END
C
SUBROUTINE TRNPOS(A,B)
  A 3 X 3 MATRIX TRANSPOSE ROUTINE
  DIMENSION A(3,3),B(3,3)
  DO 1 I=1,3
  DO 1 J=1,3
  B(I,J)=A(J,I)
  1 RETURN
  END
C
SUBROUTINE HIHC(N,LOCT,NX1,NX2,NX3,NX4,X1ARG,X2ARG,
  *X3ARG,X4ARG,A)
  TABLE SET-UP ROUTINE
  COMMON/TA3UIP/TA(1)
  DIMENSION XA(4),NA(4)
  11 FORMAT (1H,15X,4HAN ARGUMENT EXCEEDS LOWER LIMIT OF TABLE)
  12 FORMAT (1H,15X,4HAN ARGUMENT EXCEEDS UPPER LIMIT OF TABLE)
  16 FORMAT (1H,15X,4HAN INDEPENDENT VARIABLES NOT IN ASCENDING ORDER)
  XA(1)=X1ARG
  XA(2)=X2ARG
  XA(3)=X3ARG
  XA(4)=X4ARG
  NA(1)=NX1
  NA(2)=NX2
  NA(3)=NX3
  NA(4)=NX4
  NAT=NX1
  IF (N-4) 3,6,5
  3 NAT=NAT+NA(2)
  GO TO 6
  4 NAT=NAT+NA(2)+NA(3)
  GO TO 6
  5 NAT=NAT+NA(2)+NA(3)+NA(4)
  6 II=NAT+LOCT
  CALL NOTLJ(N,NA,TA(LOCT),TA(II),XA,A,IERROR)
  IF (IERROR.EQ.0) RETURN
  CALL STFL(,1,0UM)
  CALL ERROR(LOCT)
  CALL LINES(2)
  IF (IERROR-1) 7,14,15
  7 WRITE(6,11)
  RETURN
  13 WRITE(6,16)
  RETURN
  15 WRITE(6,16)
  RETURN
  END
C
SUBROUTINE TLU(X,LOCT,Y)
  TWO DIMENSIONAL TABLE LOOK-UP ROUTINE
  COMMON/TA3UIP/C(1)
  EQUIVALENCE (N,Z)
  LOCTM1=LOCT-1
  N=
  Z=C(LOCT)

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C 00.1 I=1,N
  J=2*I+LOCTH1
  IF(C(J)-X) 1,6,2
1  CONTINUE
  GO TO 5
2  IF(J.GT.(LOCTH1+2))GO TO 4
  J=3+LOCTH1
5  CALL ERROR(LOCT)
4  Y=C(J-1)+(C(J+1)-C(J-1))*(X-C(J-2))/(C(J)-C(J-2))
  RETURN
6  Y=C(J+1)
  RETURN
END
SUBROUTINE TFFS1

      ENGINE THRUST

      INPUT REQUIRED (FROM DIRCON)
      ALT77F, AMACH, AMASS, AMASS1, AMASZS, AMT77F,
      AMT77F, IND77F, TXB7P, TYB7P, TZB7P, IN, N(5),
      IT1W, IT1X, ZN(5), YN(5)

      COMMON/DIRCON/DM1(26),ALT77F,DM2(6),AMACH,DM3(2),
      *AMASS,AMASS1,AMASZS,DM4(5),AMT77F,DM5(13),AMT77F,
      *DM6(49),IND77F,DM7(26),TXB7P,DM8(2),TYB7P,DM9(2),
      *TZB7P,DM10(2),IT1W,IT1X,DM11(2),IT1W,IT1X,DM12(22),
      *AMASFS(2),AMASF1(2),DM13(44),IN,ZN(5),YN(5),N(5),DM14(29),
      *DM15(2,68)

      IN      - NUMBER OF ENGINES
      N(1)    - THROTTLE POSITION FOR I ENGINE
      YN(1)   - ENGINE POSITION FOR I ENGINE
      ZN(1)   - ENGINE POSITION FOR I ENGINE
      MT(1)   - ENGINE PITCH MOMENT FOR I ENGINE
      NT(1)   - ENGINE YAW MOMENT FOR I ENGINE
      T(1)    - ACTUAL ENGINE THROUST FOR I ENGINE

      DIMENSION S(2)
      COMMON/FLXUP/DT1(3,6),T(5),BH2(303)
      COMMON/TABSPC/LOC(2),DUMM1(168)
      REAL N,MT(5),NT(5)
      DATA FMT1/6H, TFFS/,
      CS(1),S(2)/2HNT,2HNT/

      INITIALIZATION BEFORE DATA READ IN

      TXB7P=.
      TYB7P=.
      TZB7P=.
      ALT77F=.
      AMT77F=.
      AMT77F=.
      RETURN

      THRUST COMPUTATION SECTION

      ENTRY TFFS3
      TXB7P=.
      TYB7P=.
      TZB7P=.
      ALT77F=.
      AMT77F=.
      AMT77F=.
      IF(IND77F.EQ.0)RETURN

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DO 10 I=1,IN
CALL HIRU13,LCC(1),IT10W,IT10X,DU,DU,N(I),AMACH,
CDD, T(I)
MT(I)=T(I)*ZN(I)
NT(I)=-T(I)*YN(I)
TXB7P=TXB7P+T(I)
AMT77F=AMT77F+MT(I)
ANT77F=ANT77F+NT(I)
10 CONTINUE
RETURN

GGG INITIAL PRINT
ENTRY TFFS4
RETURN

GGG COMPUTE AND PRINT CODES
ENTRY TFFS5
IF(INOTFF,DU,.)RETURN
CALL STFL(3,1,FMT1)
CALL STFL(2,2,S)
RETURN

GGG TIME HISTORY PRINT
ENTRY TFFS6
IF(INOTFF,DU,.)RETURN
CALL STFL(3,1,FMT1)
CALL STOVAK(2,AMT77F,ANT77F,DU,DU,DU,DU,DU,DU)
CALL STFL(4,1,DU)
CALL LINES(2)
60 WRITE(6,6) (T(I),I=1,IN)
FORMAT(1H,63X,4HT(I)/(14X,5E20.8))
RETURN

GGG UPDATE INTEGRATION
ENTRY TFFS7
RETURN
END
SUBROUTINE TFFS8(TC,TN)

GGGGGG SEARCH THROUGH RANGES OF N TO FIND THE N
THAT CORRESPONDS WITH THRUST TC AND CURRENT
MACH NUMBER

GGGGGG INPUT - TC (THRUST) AND MACH (CURRENT AMACH NO.)
OUTPUT - TN (THRUSTLE SETTING)

COMMON/DIRCON/DM1(26),ALT77F,DM2(6),AMACH,DM3(2),
*AMAS5,AMAS11,AMAS25,DM4(5),AMT77F,DM5(13),ANT77F,
*DM6(45),INOTFF,DM7(146),TXB7P,DM8(2),TYB7P,DM9(2),
*TXB7P,DM10(2),IT10W,IT10X,DM11(2),IT11W,IT11X,DM12(221),
*AMASFS(2),AMASF1(2),DM13(444),IN,ZN(5),YN(5),N(5),DM14(290),
*DM15(2,66)

COMMON/TANDIR/C(1)
COMMON/TASRC/LOC(2),DUMH1(100)

C IF(INOTFF,NE,.)GO TO 26
TN=.
RETURN
26 LOC=LOC(1)-1
DO 20 I=1,IT11W

```



```

10DRFF      ,DM11(15) ,EPS21 ,EPS22 ,
2EPS18      ,EPS19 ,DM12 ,EPS20 ,EPS21 ,EPS22 ,
3EPS23      ,EPS24 ,DM13(215) ,
4INDJDP      ,DM14(3) ,
5DM15(53) ,
6INDTSO      ,INDVPC ,DM16(2) , INDXYS ,INDXZS ,
7DM17(223) ,
8TIMEC      ,DM18(74) ,DM19( 930) ,DM20(2058)
9XCGBF      ,XCGGF ,
COMMON/TAB,PC/DUMM1(H.),LOC(18),DUMM2(11)
2EQUIVALENCE (BS1IXX,AIXXS1),(BS1IYY,AIYYS1),(BS1IZZ,AIZZS1),
*(BS1IXY,AIXYS1),(BS1IXZ,AIXZS1),(BS1IYZ,AIYZS1)
DATA
1(A(1),I=1,4)/5HXCGPF,5HAREFF,5HDIRFF,5HDIRFF/,
20,HUC1/5HAMASS,6H VPCS/
2 FORMAT (1H,15X,26HINITIAL PRINT OUT FOR VPCS)
C RETURN
C *****
C INITIALIZATION AFTER DATA READ IN
C ENTRY VPCS2
C IF (INDVPC.EQ.0) RETURN
C *****
173 BS1IXX=.
BS1IYY=.
BS1IZZ=.
BS1IXY=.
BS1IXZ=.
BS1IYZ=.
ALLJOF=.
ALHJOF=.
ALNJOF=.
ALYJOF=.
ALZJOF=.
IF (INDXZS.EQ.0) GO TO 212
AIXYBS=.
AIYZBS=.
212 IF (INDXYS.NE. ) AIXZBS=.
RETURN
C *****
C VEHICLE PHYSICAL CHARACTERISTICS SUBPROGRAM SECTION
C *****
C ENTRY VPCS3
C IF (INDVPC.EQ.0) RETURN
C *****
216 IF (INDTSO.EQ.0) GO TO 451
223 CALL TLU(AMACS,LOC(1),XCGBF)
CALL TLU(AMASS,LOC(2),AIXXBS)
CALL TLU(AMASS,LOC(3),AIYYBS)
CALL TLU(AMASS,LOC(4),AIYZBS)
XCGGF=XCGBF+EPS18
AIXXBS=AIXXBS+EPS19
AIYYBS=AIYYBS+EPS20
AIZZBS=AIZZBS+EPS21
IF (INDXZS.NE. ) GO TO 335
CALL TLU(AMACS,LOC(5),AIXYBS)
CALL TLU(AMASS,LOC(7),AIYZBS)
AIXYBS=AIXYBS+EPS22
AIYZBS=AIYZBS+EPS24
335 IF (INDXYS.NE. ) GO TO 353
CALL TLU(AMACS,LOC(6),AIXZBS)
AIXZBS=AIXZBS+EPS23
353 IF (INDJDP.EQ.0) GO TO 451
CALL TLU(XCGGF,LOC(8),ALYJOF)
CALL TLU(XCGGF,LOC(9),ALZJOF)
CALL TLU(XCGGF,LOC(10),ALLJOF)

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C CALL TLU(XCGDF,LOC(11),ALNJOE)
451 IF (INDIOT.EQ.) GO TO 567
CALL TLU(TIMES,LOC(13),BS11XX)
CALL TLU(TIMES,LOC(14),BS11YY)
CALL TLU(TIMES,LOC(15),BS11ZZ)
503 IF (INDXZ3.NE.U) GO TO 551
CALL TLU(TIMES,LOC(16),BS11XZ)
CALL TLU(TIMES,LOC(18),BS11YZ)
551 IF (INDXYS.NE.C) GO TO 567
CALL TLU(TIMES,LOC(17),BS11XZ)
567 DXCGF=XCGDF-XCGRF
RETURN
*****
C INITIAL PRINT
C ENTRY VPC34
IF (INDVPC.EQ.) RETURN
*****
C 27 CALL STFL(0,1,DU)
WRITE (6,2)
CALL STFL(2,4,A)
CALL STOV42(4,XCGRF,AREFF,D1RFF,D2RFF,DU,DU,DU,DU)
RETURN
*****
C COMPUTE AND PRINT CODES
C ENTRY VPC35
IF (INDVPC.EQ.) RETURN
*****
C 64 CALL STFL(3,1,HBCI)
CALL STFL(4,1,H)
RETURN
*****
C TIME HISTORY PRINT
C ENTRY VPC36
IF (INDVPC.EQ.) RETURN
*****
C 103 CALL STFL(3,1,HBCI)
CALL STFL(1,1,AMASS)
RETURN
*****
C ENTRY VPC37
*****
C RETURN
END
SUBROUTINE SACS1
EXTERNAL ASIN
C LOGICAL AERO DYNAMIC FORCES AND MOMENTS
LOGICAL INDAPC
DIMENSION B(3),D(3),TMP(20),INC(79),TC(79)
COMMON /DIRGCM/
10M(22)
2AA77P ,DM1(91) ,
3ALA77F ,DM2(3) ,
4ALPHU,DM4(3),ALPHR1,DM5(3),
5ALPTD ,DM6(8) ,
6AMACH(3),DM7(4) ,
7DM8(3),AMT77F,DM56(5),
8ANAZ7F ,ANA77P ,DM9(6) ,ANT77F,
9ANUA7F ,DM10(2) ,AREFF ,DM11(11) ,
1BETAD,DM12(3),ETAK1,DM13(22),
2CA ,DM14(2) ,CAMNU ,DM15(6) ,
3CD ,DM16(2) ,CDMNU ,DM17(6) ,CL
4DM18(3) ,CLMNU ,CM ,CMMNU ,
5CM2MNU,CM14NU,DM19,CPHIA,DM20(9),
6CRM ,DM21(7) ,

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7CY ,DM22 ,CYM ,CYMNU ,DM23(49) ,DCW2 ,
 8DCU1 ,DCV1 ,DCW1 ,DCU2 ,DCV2 ,
 9DCU3 ,DCV3 ,DCW3 ,DM24(15) ,
 COMMON /DIR COM7
 17ELPD ,DM22 ,DELOD ,DM26 ,DELPD ,DM27(17) ,
 2ORAGP ,DM28 ,DXCGF ,DM24(13) ,
 3OYNPP ,DM31 ,DIRFF ,DM31 ,DIRFF ,DM32(6) ,
 4EPS1 ,EPS1 ,EPS11 ,EPS12 ,DM33(7) ,
 5EPS2 ,DM34(7) ,
 6EPS3 ,EPS4 ,EPS5 ,EPS6 ,EPS7 ,EPS8 ,
 7EPS9 ,DM35(43) ,HGC7F ,DM61(44) ,
 8INDAER ,DM37(12) ,INDARC ,DM48(3) ,
 COMMON /DIR COM7
 1INDA1 ,INDA11 ,INDA13 ,INDA14 ,INDA15 ,INDA16 ,INDA17 ,INDA18 ,INDA19 ,INDA20 ,INDA21 ,INDA22 ,INDA23 ,INDA24 ,INDA25 ,INDA26 ,INDA27 ,INDA28 ,INDA29 ,INDA30 ,INDA31 ,INDA32 ,INDA33 ,INDA34 ,INDA35 ,INDA36 ,INDA37 ,INDA38 ,INDA39 ,INDA40 ,INDA41 ,INDA42 ,INDA43 ,INDA44 ,INDA45 ,INDA46 ,INDA47 ,INDA48 ,INDA49 ,INDA50 ,INDA51 ,INDA52 ,INDA53 ,INDA54 ,INDA55 ,INDA56 ,INDA57 ,INDA58 ,INDA59 ,INDA60 ,INDA61 ,INDA62 ,INDA63 ,INDA64 ,INDA65 ,INDA66 ,INDA67 ,INDA68 ,INDA69 ,INDA70 ,INDA71 ,INDA72 ,INDA73 ,INDA74 ,INDA75 ,INDA76 ,INDA77 ,INDA78 ,
 4INDA8J ,DM52(13) ,INDBAU ,DM39(7) ,
 COMMON /DIR COM7
 7INDFLT ,DM41(55) ,
 8INDSDF ,DM41(23) ,
 8NSYMB ,DM41(14) ,
 9SIOEP ,DM41(11) ,
 9SP4IA ,DM41(11) ,
 1VA77F ,DM41(11) ,
 2VA77F ,DM41(11) ,
 4YA77P ,DM47(8) ,YGM7F1 ,DM59(173) ,
 5P177R ,DM43(7) ,
 6P177R ,DM43(7) ,
 7P177R ,DM43(13) ,TS77P ,DM51(428) ,IAP ,DM57(3) ,
 *ALPHDS ,ALPHDL ,FCG ,DM53(94) ,DELOD ,DM54(7) ,
 *JLQL ,DELJU ,DM55(7) ,DELRL ,DELRU ,DM56(78) ,HP ,DM58(64) ,DDM77(2068) ,
 COMMON /TA35FC/DUMM2(2) ,LDC(73) ,DUMM2(29) ,
 COMMON /AUTSAC/ALPH1 ,QDESP ,CLRR ,ALPOES ,COP ,DELRN
 COMMON /LG/FXH ,FYH ,FZH ,LM ,HM ,NH ,EPSLOL
 REAL LM ,HM ,NH
 EQUIVALENCE (INDA1 ,INC(1)) ,
 * (TC(1) ,CAALPH) , (TC(2) ,CAALSO) , (TC(3) ,CAHETA) , (TC(4) ,CAHTS) ,
 * (TC(5) ,CAHTL) , (TC(6) ,CAULSO) , (TC(7) ,CAALDT) , (TC(8) ,CAALDL) ,
 * (TC(9) ,CAHTL) , (TC(10) ,CAULSO) , (TC(11) ,CAALDT) , (TC(12) ,CAALDL) ,
 * (TC(13) ,CAHTL) , (TC(14) ,CAULSO) , (TC(15) ,CAALDT) , (TC(16) ,CAALDL) ,
 * (TC(17) ,CAHTL) , (TC(18) ,CAULSO) , (TC(19) ,CAALDT) , (TC(20) ,CAALDL) ,
 * (TC(21) ,CAHTL) , (TC(22) ,CAULSO) , (TC(23) ,CAALDT) , (TC(24) ,CAALDL) ,
 * (TC(25) ,CAHTL) , (TC(26) ,CAULSO) , (TC(27) ,CAALDT) , (TC(28) ,CAALDL) ,
 * (TC(29) ,CAHTL) , (TC(30) ,CAULSO) , (TC(31) ,CAALDT) , (TC(32) ,CAALDL) ,
 * (TC(33) ,CAHTL) , (TC(34) ,CAULSO) , (TC(35) ,CAALDT) , (TC(36) ,CAALDL) ,
 * (TC(37) ,CAHTL) , (TC(38) ,CAULSO) , (TC(39) ,CAALDT) , (TC(40) ,CAALDL) ,
 * (TC(41) ,CAHTL) , (TC(42) ,CAULSO) , (TC(43) ,CAALDT) , (TC(44) ,CAALDL) ,
 * (TC(45) ,CAHTL) , (TC(46) ,CAULSO) , (TC(47) ,CAALDT) , (TC(48) ,CAALDL) ,
 * (TC(49) ,CAHTL) , (TC(50) ,CAULSO) , (TC(51) ,CAALDT) , (TC(52) ,CAALDL) ,
 * (TC(53) ,CAHTL) , (TC(54) ,CAULSO) , (TC(55) ,CAALDT) , (TC(56) ,CAALDL) ,
 * (TC(57) ,CAHTL) , (TC(58) ,CAULSO) , (TC(59) ,CAALDT) , (TC(60) ,CAALDL) ,
 * (TC(61) ,CAHTL) , (TC(62) ,CAULSO) , (TC(63) ,CAALDT) , (TC(64) ,CAALDL) ,

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      * (TC(85),CN2ALD); (TC(96),CN2BUL); (TC(97),CN2BTD); (TC(98),CN2BEX);
      * (TC(85),CN2BUL); (TC(96),CN2BUL); (TC(97),CN2BTD); (TC(98),CN2BEX);
      * (TC(73),CN2ALD); (TC(74),CN2BUL); (TC(75),CN2BTD); (TC(76),CN2BEX);
      * (TC(77),CN2R ); (TC(78),CN2RX ); (TC(79),CAVAH)
      EQUIVALENCE (CY,CYA), (DYNPL,DYNPP)
      DATA DEGRAD/.J1745329/
      DATA
      *H3C1,C/oh SAC1,6HCAVAH /,
      1 (J(I),I=1,3)/2HCA,2HCM,2HCY/,
      2 (J(I),I=1,3)/2HCL,2HCM,3HCNN/
      1 1267 FORMAT (1H,15X,26HINITIAL PRINT OUT FOR SAC1)
      ANA77P=.
      ALA77F=.
      AMA77F=.
      ANA77F=.
      AA77P=.
      YA77P=.
      RETURN
      C *****
      C ENTRY SAC33
      C *****
      IF (INDAER.EQ. ) RETURN
      IF (INDAER) GO TO 1267
      IF (VS77F.NE.. ) GO TO 1470
      CA =CAHNU
      CN =CN1MNJ
      CY =CYHNU
      CRM=CLMNU
      CA =CMHNU
      CY=CNEHNU
      1401 TMP(1)=EPS9*CY+EPS6
      TMP(2)=DYNPP*AREFF
      YA77P=TMP(1)*TMP(2)
      ALA77F=(EPS7*CRM+EPS8)*TMP(2)*D2RFF
      ANA77F=(EPS11*CYM+EPS12)*TMP(2)*D2RFF
      TMP(1)=EPS3*CA+EPS4
      TMP(2)=DYNPP*AREFF
      AA77P=TMP(1)*TMP(2)
      ANA77P=(EPS1*CN+EPS2)*TMP(2)
      AMA77F=(EPS9*CM+EPS1L)*TMP(2)*D1RFF
      RETURN
      1470 IGO1=1
      IGO2=1
      IGO3=1
      DO 71 I=1,79
      71 TC(I)=.
      50 HG=HGC7F
      IF (IAP.GE.3) HG=HR
      C EPSLO2 IS COMPUTED IN SUBROUTINE LGEA3C
      TMP(1)=EXP(-4.E*(HG-EPGLO2-HCG)/(D2RFF-HCG))
      DO 79 I=1,79
      IF (INC(I).NE.. ) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
      79 CONTINUE
      DO 80 I=15,16
      IF (INC(I).NE.. ) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
      80 CONTINUE
      DO 81 I=1,12
      IF (INC(I).NE.. ) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
      81 CONTINUE
      DO 85 I=20,22,2
      IF (INC(I).NE.. ) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
      85 CONTINUE
      IF (INDAER.NE.. ) CAVAH =(AERO1(LOC(79),AERO2)-AERO2)*TMP(1)+AERO2
      GO TO (1,20,33),IGO1

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1  DO 82 I=71,83
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
82  CONTINUE
   DO 83 I=73,83
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
83  CONTINUE
   GO TO (11,40),IG02
11  DO 84 I=27,28
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
84  CONTINUE
   DO 70 I=54,71
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
70  CONTINUE
   GO TO (12,65),IG03
12  DO 72 I=3,4
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
72  CONTINUE
   DO 73 I=13,14
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
73  CONTINUE
   DO 74 I=17,28
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
74  CONTINUE
   DO 75 I=33,51
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
75  CONTINUE
   DO 76 I=54,55
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
76  CONTINUE
   DO 77 I=64,67
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
77  CONTINUE
   DO 78 I=72,78
   IF (INC(I).NE.0) TC(I)=(AERO1(LOC(I),AERO2)-AERO2)*TMP(1)+AERO2
78  CONTINUE
   TMP(2)=A35(ALPH0)
   TMP(4)=A35(BETAD)
   TMP(3)=B1AD**2
   TMP(5)=A35(DELQ0)
   TMP(6)=ALPH0*ALPH0
   TMP(7)=A35(DELQ0)
   TMP(8)=.5*DELQ0**2/VA77F
   CJ=CAYAH+TMP(2)*CAALPH+ALPH0**2*CAALSQ+TMP(4)*CABETA+TMP(3)*
   *CABTSJ+TMP(5)*CADLQ+DELQ0**2*CADLSQ+ANS(ALPH0*DELQ0)*CAALDL+
   *ANS(ALPH0*BETAD)*CAALHT+ANS(BETAD*DELQ0)*CABTDL
   CL=CN1ZL**2*ALPH0*CN1ALP+ALPH0*TMP(2)*CN1ASQ+TMP(4)*CN1BET+
   *TMP(3)*CN1BSQ+DELQ0*CN1DLQ+TMP(5)*DELQ0*CN1DSQ+TMP(2)*DELQ0*
   *CN1ALQ+TMP(4)*ALPH0*CN1ALB+TMP(4)*DELQ0*CN1BL+
   *01*FF/VA77F*ALPH0**2/2*(CN1A)*DXCGF+CN1ADL+
   *01*FF/VA77F*GT77**2*(CN1QX*DXCGF+CN1Q)
   TMP(9)=ALPH0**2/17453.4
   CA=CU*COS(TMP(3))-CL*SIN(TMP(9))
   CN=CL*COS(TMP(3))+CU*SIN(TMP(9))
   CY=CYZL**2+TMP(2)*CYALP+TMP(6)*CYALSQ+BETAD*CYBETA+BETAD*TMP(4)*
   *CYBTSD+DELQ0*CYDLR+TMP(7)*DELRO*CYDRSQ+TMP(2)*DELRO*CYALDL+
   *TMP(2)*DELQ0*CYALHT+TMP(4)*DELRO*CYBTOL+
   *BETAD*TMP(4)*CYBTDX*DXCGF+CYBTOT+
   *177K*TMP(8)*(CYRX*DXCGF+CYR)
   TMP(8)=A35(ALPH0)
   TMP(1)=ALPH0**2
   TMP(9)=A35(BETAD)
   TMP(10)=A35(DELQ0)
   TMP(2)=DELQ0**2/VA77F*2.1
   TMP(3)=BETAD*BETAD
   TMP(4)=A35(DELQ0)

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C  * CRH=CLZERO+TMP(8)*CLALPH+TMP(11)*CLALSO+TMP(9)*CLBETA+BETAD**2*
C  * CLD1SQ+DELPD*CLDLTP+ABS(DELPOY)*DELPD*CLDLSQ+TMP(8)*DELPD**2*
C  * CLALDL+ABS(ALPHD*BETAD)*CLALUT+TMP(9)*DELPD*CLBTOL+
C  * TMP(2)*PI77R*CLP+PI77R*TMP(2)*(CLR*DXCGF+CLR)
C  * CM=CHZERO+ALPHD*CHALPT+TMP(8)*ALPHD*CHALSO+TMP(9)*CMBETA+TMP(3)*
C  * CHUTS+DELGD*CHDLTQ+TMP(4)*DELGD*CHDLSQ+TMP(8)*CHALDL*DELGD+
C  * TMP(3)*ALPHD*CHALBT+TMP(9)*DELGD*CHBTOL+
C  * D1KFF/VA77F*ALPHR1/2*(CMADTX*DXCGF+CHALDT)+
C  * D1KFF/VA77F*QI77R/2*(CMQX*DXCGF+CMQ)-
C  * DXCGF/D1RFF*CN
C  * CYM=CHZERO+TMP(8)*CN2ALP+TMP(11)*CN2ASQ+BETAD*CN2BET+TMP(9)*BETAD*
C  * CN2BS+DELRO*CN2DLT+TMP(10)*CN2DSQ*DELRO+TMP(8)*DELRO*CN2ALD+
C  * TMP(8)*BETAD*CN2ALB+TMP(9)*CN2BDL*DELRO+
C  * TMP(2)*BETAR1*(CN2BDX*DXCGF+CN2BDT)+
C  * TMP(2)*RI77R*(CN2RX*DXCGF+CN2R)-CY*DXCGF/D2RFF
C  GO TO 1451
C  *****
C  ENTRY SAC34
C  *****
C  IF (INDAER.EQ.0) RETURN
C  RETURN
C  *****
C  ENTRY SAC35
C  *****
C  IF (INDAER.EQ.0) RETURN
63  CALL STFL(3,1,HBCI)
C  IF (INDA80.NE.0) CALL STFL(2,1,C)
C  CALL STFL(2,3,B)
123  CALL STFL(2,3,D)
C  RETURN
C  *****
C  ENTRY SAC36
C  *****
C  IF (INDAER.EQ.0) RETURN
326  CALL STFL(3,1,HBCI)
C  IF (INDA80.NE.0) CALL STFL(1,1,CAVAH)
C  CALL STOVAR(3,CA,CN,CY,DU,DU,DU,DU,DU)
37J  CALL STOVAR(3,CRH,CM,CYM,DU,DU,DU,DU,DU)
C  RETURN
C  *****
C  ENTRY SAC37
C  *****
C  RETURN
C  DETERMINE THE ALPHA THAT MAKES CL=CLRR AND THE
C  ASSOCIATED CUR
C  ENTRY SAC38
C  INPUT FROM CALLING PROGRAM
C  CLRR
C  OUTPUT
C  ALPOES, CUR
C  INPUT FROM DIRCOM
C  DELQN, ALPHDS, ALPHDL, HCGD2RFF, INDA01, INDA02, HR,
C  INDA15, INDA16, INDA38, INDA39, INDA40, INDA80
C  INDA20, INDA22, D1KFF, VA77F, PI77F, ALPHR1
C  IF ((IAP.LT.3).OR.(ABS(HG-HR).LE.1.E-6)) GO TO 20
C  IG01=2
C  GO TO 50
20  TMP(2)=CN1ZER+CN1DLO*DELQN+CN1DSQ*ABS(DELQN)*DELQN-CLPR
C  * .5*CN1Q*QUESR*D1RFF/VA77F
C  ALPOES=AQUAD(CN1ASQ,CN1ALP,TMP(2),ALPHDS,ALPHDL)

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GOB=CAVAH+CAALPH*ABS(ALPDES)+CAALSQ*ALPDES*ALPDES
RETURN

DETERMINE THE CL1 AND CD1 FOR ALPHA=A1
ENTRY SAC39

      INPUT FROM CALLING PROGRAM
ALPDES
OUTPUT
CLRR,COR
      INPUT FROM DIRCOM
DELQN, HCG, D1RFF, INDA11, INDA02, INDA15, INDA16, HR,
INDA38, INDA39, INDA41, INDA83, INDA2L, INDA22,
D1RFF, VA77F, Q177R, ALPHR1

IF ((IAP.LT.3).OR.(ABS(HG-HR).LE.1.E-6))GO TO 3J
IG01=3
GO TO 5J
30 CLRR=CN1ZER+CN1ALP*ALPDES+CN1ASQ*ABS(ALPDES)*ALPDES+CN1DLQ
C*DELQN+CN1USC*ABS(DELQN)*DELQN
C+.5*CN1QC*DESR*D1RFF/VA77F
COR=CAVAH+CAALPH*ABS(ALPDES)+CAALSQ*ALPDES*ALPDES
RETURN

EVALUATE NOMINAL DELQN
ENTRY SAC310

      INPUT FROM CALLING PROGRAM - ALPDES
OUTPUT - DELQN
      INPUT FROM DIRCOM
DELQL, DELQU, HCG, D1RFF, D2RFF, DYNPP, AREFF, DXCGF, HR,
ANT77F, INDA11, INDA12, INDA15, INDA16, INDA38, INDA39, INDA40,
INDA83, INDA51, INDA52, INDA53, INDA56, INDA57,
INDA61, INDAF3, VA77F, ALPHR1, Q177R

IF ((IAP.LT.3).OR.(ABS(HG-HR).LE.1.E-6))GO TO 4J
IG01=1
IG02=2
GO TO 5J
40 TMP(2)=CN1ZER+ALPDES*(CN1ALP+CN1ASQ*ABS(ALPDES))
C+CN1DLQ*DELQN+CN1USC*ABS(DELQN)*DELQN
C+.5*CN1QC*DESR*D1RFF/VA77F
TMP(3)=CAVAH+CAALPH*ABS(ALPDES)+CAALSQ*ALPDES*ALPDES
TMP(4)=TMP(2)*COS(ALPDES*DEGRAD)+TMP(3)*SIN(ALPDES*DEGRAD)
TMP(5)=DYNPP*AREFF*D1RFF
TMP(2)=-TMP(4)*DXCGF*TMP(5)/D1RFF
TMP(3)=CN1LTC*TMP(5)
TMP(4)=(CN1ZFC+ALPDES*(CAALPH+CAALSQ*ABS(ALPDES)))
C*TMP(5)+ANT77F*TMP(2)+HM
C+.5*CN1QC*DESR*D1RFF*TMP(5)/VA77F
TMP(2)=TMP(5)*CN1LSC
DELQN=ADDAD(TMP(2),TMP(3),TMP(4),DELQL,DELQU)
RETURN

EVALUATE NOMINAL DELRN
ENTRY SAC311

      INPUT FROM DIRCOM
IAP, D2RFF, LYNPP, AREFF, ANT77F, YGW7F1, VA77F
DELR1, DELR0

IF ((IAP.LT.3).OR.(ABS(HG-HR).LE.1.E-6))GO TO 6J

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60  IG04=2
    GO TO 11
    BETADE=C.
    IF (IAP.GE.3) BETADE=ASIN(-YGH7F1/VA77F)*57.2957795
    TMP(5)=DY4PP*AK2FF*02RFF
    TMP(6)=DXC6F/D2RFF
    TMP(3)=CN2ULT*TMP(5)
    TMP(2)=CN2USQ*TMP(5)
    TMP(4)=ANT77F+BETADE*(CN2BET-CYBETA*TMP(6)
C+ABS(BETA1E)*(CN2BSQ-CYBTSQ*TMP(6)))*TMP(5)
    DELRN=AQUAD(TMP(2),TMP(3),TMP(4),DELRL,DELRU)
    RETURN
    END
    FUNCTION AE7C1(LOCT,AER02)
    COMMON/TABD,P/C(1)
    AER01=C(LOCT)
    AER02=C(LOCT+1)
    RETURN
    END
    FUNCTION AQUAD(A,B,C,XLLIM,XULIM)
    IF (ABS(A).GT.1.E-10) GO TO 4
    X=.
    IF (ABS(B).LE.1.E-10) GO TO 11
    X=-C/B
    GO TO 11
4    TMP=U*U-.4*A*C
    IF (TMP.LI...) GO TO 30
    TMP1=SQRT(TMP)
    X=(-B+TMP1)*.5/A
    IF (X.LT...) GO TO 5
    IF ((X.LT.XULIM).AND.(X.GT.XLLIM)) GO TO 20
5    X=(-B-TMP1)*.5/A
    IF (X.LT...) GO TO 30
    IF ((X.LT.XULIM).AND.(X.GT.XLLIM)) GO TO 20
30    TMP=R*B+.4*A*C
    IF (TMP.LI...) GO TO 10
    TMP1=SQRT(TMP)
    X=(-B+TMP1)*.5/(-A)
    IF (X.GT...) GO TO 15
    IF ((X.LT.XULIM).AND.(X.GT.XLLIM)) GO TO 20
15    X=(-B-TMP1)*.5/(-A)
    IF (X.GT...) GO TO 10
    IF ((X.LT.XULIM).AND.(X.GT.XLLIM)) GO TO 20
10    FX1=XLLIM*(A*AUS(XLLIM)+B)+C
    FX2=XULIM*(A*AUS(XULIM)+B)+C
    X=XLLIM
    IF (ABS(FX1).GT.AUS(FX2)) X=XULIM
20    AQUAD=X
    RETURN
    END
    SUBROUTINE OPT1
    EXTERNAL ASIN,ATAN2
C    SIX-DEGREE-OF-FREEDOM OVER FLAT PLANET
    DIMENSION
    * TMP(27),D(17),D(2),E(2),DRAGG(4),
    * F(1),H(2),J(3),K(3),
    * L(3),G(2),LA(18)
    LOGICAL ITRARC,SH
    COMMON /DIRCOM/
    * DM(22),AA77P,AE77F,DP2(4),AIXR7S,AIXXBS,
    * AIXXS1,AIXYBS,AIXYS1,AIXZBS,AIXZS1,DM3,
    * AIYBS,AIYYS1,AIYZBS,AIYZS1,DM4,AIZZBS,
    * AIZZS1,DM5(7),AKLT,AKL1,AKL2,AKL3,
    * AKL4,AKL5,AKL6,AKM1,AKM2,AKM3,AKM4,AKM5,AKM6,

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A-32


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SGAMD = SIN(GAMDR)
CGAMD = COS(GAMDR)
SSIGD = SIN(SIGDR)
CSIGD = COS(SIGDR)
THTBR = THBR*.J1745329
PSIBR = PSIB*.J1745329
PHIBR = PHIB*.J1745329
SPHIB = SIN(PHIBR)
CPHIB = COS(PHIBR)
STHBR = SIN(THTBR)
CTHBR = COS(THTBR)
SPSIB = SIN(PSIBR)
CPSIB = COS(PSIBR)
DCL1=CPHIB*CTHBR
DCL2=SPSIB
DCL3=-CPSIB*STHBR
UCH1=SPHIB*STHBR-CPHIB*SPSIB*CTHBR
UCH2=CPHIB*CPSIB
UCH3=SPHIB*CTHBR+CPHIB*STHBR*SPSIB
UCN1=CPHIB*STHBR+CTHBR*SPSIB*SPHIB
UCN2=-SPHIB*CPSIB
UCN3=CPHIB*CTHBR-SPHIB*STHBR*SPSIB
AL1 = DCL1
AL2 = DCL2
AL3 = DCL3
AM1 = UCH1
AM2 = UCH2
AM3 = UCH3
AN1 = UCN1
AN2 = UCN2
AN3 = UCN3
XG77F1= SSIGD*CGAMD*VG77F
YG77F1= CSIGD*CGAMD*VG77F
ZG77F1=-SGAMD*VG77F
TMP(1)= XG77F1
TMP(2)= YG77F1
TMP(3)= ZG77F1
CALL INTEG (LA(16) , XG77F1 )
CALL INTEG (LA(17) , YG77F1 )
CALL INTEG (LA(18) , ZG77F1 )
CALL MULT31 (DCL1,TMP(1),TMP(4))
U777F = TMP(4)
V777F = TMP(5)
W777F = TMP(6)
INOSKP=1
GO TO 702
*****
ENTRY GPI4
*****
C
C621
621
SJF
DCL1 = AL1
DCL2 = AL2
DCL3 = AL3
UCH1 = AM1
UCH2 = AM2
UCH3 = AM3
UCN1 = AN1
UCN2 = AN2
UCN3 = AN3
TMP(1)= U777F
TMP(2)= V777F
TMP(3)= W777F
CALL TRNPS (DCL1,TMP(4))
CALL MULT31 (TMP(4),TMP(1),TMP(13))
XG77F1= TMP(13)

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      YG77F1= TMP(14)
      ZG77F1= TMP(15)
      CALL INTG (LA(16) , XG77F1 )
      CALL INTG (LA(17) , YG77F1 )
      CALL INTG (LA(18) , ZG77F1 )
C7.2  SDF2
702  GX07F = DCL3*GREFF
      GY07F = DCH3*GREFF
      GZ07F = DCH3*GREFF
      HG07F = -ZG77F
      CALL ATMS (HG07F+RWHGR)
      IF (INDGCR.NE..J) RG77N =
      *      SORT((XG77F-XGZ7F)**2+(YG77F-YGZ7F)**2)*1.6457925E-4
      IF (INDWIN.NE..J) GO TO 754
      UH77F = J.
      VH77F = J.
      WH77F = J.
      GO TO 1133
754  GO TO (755,757,761),INDWIN
755  TMP(1)=TIME
      GO TO 757
757  TMP(1)=HG07F
      GO TO 761
761  TMP(1)=RG77N
762  CALL TLU(TMP(1),LOC(2),XGW7F1)
      CALL TLU(TMP(1),LOC(3),YGW7F1)
      CALL TLU(TMP(1),LOC(4),ZGW7F1)
      TMP(1)= XGW7F1
      TMP(2)= YGW7F1
      TMP(3)= ZGW7F1
      CALL MULT11 (DCL1,TMP(1),TMP(4))
      UH77F = TMP(4)
      VH77F = TMP(5)
      WH77F = TMP(6)
1035  VA77F = SORT((U777F-UH77F)**2+(V777F-VH77F)**2+(W777F-WH77F)**2)
      DYNFP = .5*RHOAS*VA77F**2
      AMACH = J.
      IF (VS77F.NE..J) AMACH=VA77F/VS77F
      TMP(1)= U777F-UH77F
      ALPHR = ATAN2(W777F-WH77F,TMP(1))
      BETAR = ATAN2(V777F-VH77F,TMP(1))
      ALPHD = ALPHR*57.2957795
      BETAD = BETAR*57.2957795
      IF (INDSKP.EQ..J) GO TO 1134
      ALPL1 = ALPHR
      BETL1 = BETAR
1134  IF (INDADD.EQ..J) GO TO 1163
      DELT1 = TIME-TL11
      IF (ABS(DELT1).LT.1.) GO TO 1163
      ALPHR1= (ALPHR-ALPL1)/DELT1
      BETAR1= (BETAR-BETL1)/DELT1
      ALPL1 = ALPHR
      BETL1 = BETAR
      TL11 = TIME
C1163  2SDF9
1163  VG77F = SORT(XG77F1**2+YG77F1**2+ZG77F1**2)
      IF (VG77F.EQ..J) GO TO 1314
C1231  2SD10
1231  TMP(1)=-ZG77F1/VG77F
      IF (ABS(TMP(1)).LT.1.) GO TO 1211
      GAM7R=1.5/.79632*TMP(1)/ABS(TMP(1))
      GO TO 1212
1211  GAM7R=ASIN(TMP(1))
1212  GAM7D = GAM7R*57.2957795
      GAMDR = GAM7R

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GAMDD = GAM7D
SIG7R = ATAN2(YG77F1,XG77F1)
SIGDR = SIG7P
SIG7D = SIG7F*57.2957795
SIGDD = SIG7D
C1236 2S011
1236 SGARD = SIN(GAMDD)
CGARD = COS(GAMDD)
SSIGD = SIN(SIGDR)
CSIGD = COS(SIGDR)
IF (INDR2.EQ.1) GO TO 1314
DELT2 = TIME-TL2
IF (ABS(DELT2)-LT.DLTH2) GO TO 1314
GAM7P1 = (GAMDD-GAML1)/DELT2
SIG7P1 = (SIGDR-SIGL1)/DELT2
      TL2 = TIME
      GAML1 = GAMDR
      SIGL1 = SIGDR
1314 IF (INDR1.NE.1) GO TO 1315
SGAMA = SGAMU
GO TO 1315
1315 IF (VA77F.EQ.1) GO TO 1316
SGAMA = (ZG77F1-ZG77F11)/VA77F
1316 IF (INGPLA.EQ.1) GO TO 1754
C1517 2S015
1517 IF (INDR3.EQ.1) GO TO 1751
1524 IF (DCL1.EQ.1) GO TO 1536
THTPM = ATAN2(-DCL1,DCL1)
THTPU = THTPM*57.2957795
1536 IF (ABS(DCL2)-GT.1.1) GO TO 1546
PSIPR = ASIN(DCL2)
GO TO 1554
1546 PSIPR = 1.5779632+DCL2/ABS(DCL2)
1554 PSIPD = PSIPR*57.2957795
IF (DCH2.EQ.1) GO TO 17J1
PHIFM = ATAN2(-DCH2,DCH2)
PHIPD = PHIFM*57.2957795
1701 IF (INDACH.EQ.1) GO TO 1754
IF (ANAST.EQ.1) CALL EXERR (14)
AX77F = EXD7F/AMASS-GXJ7F
AY77F = FYJ7P/AMASS-GYJ7F
AZ77F = FZL7P/AMASS-GZJ7F
IF (INDACH.NE.1) GO TO 1754
THP(1) = AX77F
THP(2) = AY77F
THP(3) = AZ77F
CALL TRNPOS (DCL1,THP(1))
CALL MULT31 (THP(1),THP(1),THP(4))
AXP7F = THP(4)
AYP7F = THP(5)
AZP7F = THP(6)
1754 CALL VPCS3
CALL TFFS3
WTR7P = AMASS*GREFF
C
C
C
C
C
C
CHUTE DRAG COMPUTATION
ICS=1 (FROM LANDING ROLL COMPUTATION,AUTS)
ICS=0 (INPUT)
GDCR DRAG COEFFICIENT
SSH REFERENCE AREA
XCH, YCH, ZCH = CHUTE ATTACH POINTS
2061 IF (ICS.EQ.1) GO TO 2250
FCX=C
FCY=C

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FCY=G.
FCZ=L.
HDX=L.
HDY=L.
HDZ=L.
GO TO 2052
2050 FUC=DDCH*SSH*QYNPP
FCX=-FUC*(U777F-UH777F)/VA77F
FCY=-FUC*(V777F-VH777F)/VA77F
FCZ=-FUC*(W777F-WH777F)/VA77F
HDX=YCH*FCZ-ZCH*FCY
HDY=ZCH*FCX-XCH*FCZ
HDZ=XCH*FCY-YCH*FCX
2062 CALL SACS3
2125 CALL LGEAR3
CALL FLEX3
FXB7P = TXB7P-AA77P +AHASS*GX07F+DLFXP+FXM+FCX
FYB7P = TYB7P-YA77P +AHASS*GYB7F+DLFXP+FXM+FCY
FZB7P = TZB7P-ANA77P +AHASS*GZB7F+DLFXP+FXM+FCZ
ALB77F= ALI77F+DLITF+ALA77F+LM+HDX
AHB77F= AHI77F+DLHTF+AMA77F+HM+HDY
AND77F= ANT77F+DLHTF+ANA77F+NM+HDZ
IF (AHASS.EQ.0.) CALL EXERR (14)
TMP(1)= 2.*AHASS1/AHASS
U777F1= FXB7P/AHASS-QI77R*W777F+RI77R*V777F
V777F1= FYB7P/AHASS-PI77R*U777F+PI77R*W777F+TMP(1)*RI77R*ALYJDF
W777F1= FZB7P/AHASS-PI77R*V777F+QI77R*U777F-TMP(1)*QI77R*ALZJDF
AKL1 = ALB77F+(AIYBS-AIZZBS)*QI77R*RI77R
AKH1 = AHB77F+(AIXBS-AIXXBS)*PI77R*RI77R
AKN1 = AHB77F+(AIXBS-AIYBS)*PI77R*QI77R
IF (INDXBS.EQ.0) GO TO 2317
AKL3 = J.
AKH3 = J.
AKN3 = J.
AKL4 = J.
AKH4 = J.
AKN4 = J.
GO TO 237J
23021
2317 TMP(1)= QI77R**2
TMP(2)= RI77R*PI77R
AKL3 =-AIXYBS *TMP(2)
AKH3 =-AIXYBS *RI77R*QI77R
AKN3 =-AIXYBS *(TMP(1)-PI77R**2)
AKL4 =-AIYZBS *(TMP(1)-RI77R**2)
AKH4 =-AIYZBS *PI77R*QI77R
AKN4 =-AIYZBS *RI77R*PI77R
23022
2370 IF (INDXBS.EQ.J) GO TO 2376
AKL2 = J.
AKH2 = J.
AKN2 = J.
GO TO 2422
23023
2376 AKL2 = AIXZBS*PI77R*QI77R
AKH2 = AIXZBS*(RI77R**2-PI77R**2)
AKN2 =-AIXZBS*QI77R*RI77R
23024
2422 AKL5 =-AIXXS1*PI77R+AIXYS1*QI77R+AIXZS1*RI77R+AHASS1*ALLJDF**2*
PI77R
AKH5 =-AIYYS1*QI77R+AIXYS1*PI77R+AIZS1*RI77R+AHASS1*ALHJDF**2*
QI77R
AKN5 =-AIZS1*RI77R+AIZYS1*QI77R+AIXZS1*PI77R+AHASS1*ALNJDF**2*
RI77R
C716 25026

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Y16 IF (INDRMC.NE..) GO TO 2524
AKL6 = 0.
AKM6 = 0.
AKN6 = 0.
GO TO 2615
C2524 25027
2524 THTRR = THTRL*.51745329
STHTR = 311.(THTRR)
CTHTR = COS(THTRR)
CALL TLU (TIME3,LOC(1),THTRR1)
CALL INTEG (LTHTRR, THTRR1)
THTR0 = THTRR*.57.2457795
OMGRR = OMGR*.1.4719754
AKL6 = AIXR75*OMGRR*(QI77R+THTRR1)*STHTR
AKM6 = -AIXR75*OMGRR*(PI77R*STHTR+RI77R*CTHTR)
AKN6 = AIXR75*OMGRR*(QI77R+THTRR1)*CTHTR
C2615 25028
2615 AKLT = AKL1+AKL2+AKL3+AKL4+AKL5+AKL6
AKMT = AKM1+AKM2+AKM3+AKM4+AKM5+AKM6
AKNT = AKN1+AKN2+AKN3+AKN4+AKN5+AKN6
TMP(1) = AIXXBS
TMP(2) = -AIXYBS
TMP(3) = -AIXZBS
TMP(4) = -AIXYBS
TMP(5) = -AIXYBS
TMP(6) = -AIXZBS
TMP(7) = -AIXZBS
TMP(8) = -AIXZBS
TMP(9) = AIZZBS
CALL INVP1 (TMP(1),TMP(10),INDEP)
IF (INDEP.NE.1) CALL EXEPR (16)
TMP(1) = AKLT
TMP(2) = AKMT
TMP(3) = AKNT
CALL MULT31 (TMP(11),TMP(1),TMP(4))
PI77R1 = TMP(4)
QI77P1 = TMP(5)
RI77P1 = TMP(6)
CALL INTEG (LA(11), U777F1)
CALL INTEG (LA(11), V777F1)
CALL INTEG (LA(12), W777F1)
CALL INTEG (LA(13), PI77R1)
CALL INTEG (LA(14), QI77R1)
CALL INTEG (LA(15), RI77P1)
PI77D = PI77R*.57.2457795
QI77D = QI77P*.57.2457795
RI77D = RI77P*.57.2457795
AL17S1 = PI77P*DCN1-QI77R*DCN2
AL27S1 = RI77P*DCN2-QI77R*DCN3
AL37S1 = RI77P*DCN3-QI77R*DCN1
AM17S1 = PI77P*DCN1-RI77R*DCL1
A427S1 = PI77P*DCN2-PI77R*DCL2
A437S1 = PI77P*DCN3-PI77R*DCL3
AN177S = PI77R*DCN1-PI77R*DCN1
AN277S = QI77P*DCL2-PI77R*DCN2
AN377S = QI77R*DCL3-PI77R*DCN3
CALL INTEG (LA(1), AL17S1)
CALL INTEG (LA(2), AL27S1)
CALL INTEG (LA(3), AL37S1)
CALL INTEG (LA(4), AM17S1)
CALL INTEG (LA(5), AN177S)
CALL INTEG (LA(6), AN277S)
CALL INTEG (LA(7), AN377S)
CALL INTEG (LA(8), AN277S)
CALL INTEG (LA(9), AN377S)

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DC11 = AL1
DC12 = AL2
DC13 = AL3
DCM1 = AM1
DCM2 = AM2
DCM3 = AM3
DCN1 = AN1
DCN2 = AN2
DCN3 = AN3
CALL INVR3 (DC11,TMP(1),INDER)
IF (INDER.NE.1) CALL EXERR (17)
CALL TRNPP3 (TMP(1),TMP(10))
AL1 = .5*(AL1+TMP(10))
AL2 = .5*(AL2+TMP(10))
AL3 = .5*(AL3+TMP(10))
AM1 = .5*(AM1+TMP(11))
AM2 = .5*(AM2+TMP(14))
AM3 = .5*(AM3+TMP(17))
AN1 = .5*(AN1+TMP(12))
AN2 = .5*(AN2+TMP(15))
AN3 = .5*(AN3+TMP(18))
INDSKP=
INDARC = HGC7F .GT. AMAXH
CALL STGTST (INDSTG)
IF (SW .OR. HGC7F.GT. J.) RETURN
INDSTE =
WRITE (6,1)
10 FORMAT (1H0,15X,1GHSTOP-HGC7F)
RETURN
C *****
C ENTRY OPT5
C *****
3340 CALL STFL(3,1,H9C1)
CALL STVAR (8,TIME,TIMES,XG77F,YG77F,HGC7F,U777F,V777F,W777F)
CALL STVAR (8,PI77R,QI77R,RI77R,AMACH,VA77F,DYNPP,XG77F1,YG77F1)
CALL STFL(1,1,ZG77F1)
IF (INDAPG.NE.1) CALL STVAR(2,ALPH0,BETAD,DU,DU,DU,DU,DU,DU)
IF (INDADD.EQ.1) GO TO 3341
ALPHD1=ALPHR1*57.2957795
BETAD1=BETAR1*57.2957795
3341 CALL STVAR(2,ALPHD1,BETAD1,DU,DU,DU,DU,DU,DU)
IF (INDGSP.NE.0) CALL STFL(1,1,VG77F)
IF (INDFPA.NE.0) CALL STVAR(2,GAH7D,SIG7D,DU,DU,DU,DU,DU,DU)
IF (INDFPA.NE.0) CALL STVAR(2,GAH7R1,SIG7R1,DU,DU,DU,DU,DU,DU)
IF (INDGRT.NE.0) CALL STVAR(3,THTPD,PSIPD,PHIPD,DU,DU,DU,DU,DU)
IF (INDACH.EQ.1) CALL STVAR(3,AXP7F,AYP7F,AZP7F,DU,DU,DU,DU,DU)
IF (INDACH.EQ.2) CALL STVAR(3,AX77F,AY77F,AZ77F,DU,DU,DU,DU,DU)
IF (INDHGT.NE.0) CALL STFL(1,1,WTR7P)
IF (INDRMC.NE.0) CALL STFL(1,1,THTRD)
CALL STVAR(4,FC0,FCX,FCY,FCZ,DU,DU,DU,DU)
CALL LGEAR6
CALL VPG30
CALL TFF30
CALL SACS6
CALL FLEX5
CALL STFL(,1,DU)
RETURN
C *****
C ENTRY OPT7
C *****
TIME = DM(3)
TIMES= DM(3) - TIMSX
CALL UPDAT (5,LA(1),AL1,AL2,AL3,AM1,AM2)
CALL UPDAT (5,LA(6),AM3,AN1,AN2,AN3,U777F)
CALL UPDAT (5,LA(11),V777F,W777F,PI77R,QI77R,RI77R)

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CALL UPDAT (3, LA (16), XG77F, YG77F, ZG77F, DU, DU)
IF (INDHMC.NE.0) CALL UPDAT (1, LTHTR, THTR, DU, DU, DU, DU)
CALL LGEAR37
CALL VPCS7
CALL TFFS7
CALL SACS7
CALL FLEX7
RETURN
END
SUBROUTINE LGEAR1
COMMON/DIRCOM/DM1 (136), AMASS, DM2 (147), DCL1, DCM1,
DCM1, DCL2, DCM2, DCL3, DCM3, DCM3 (99), FXB7P2,
DDMM4 (13), FYB7P (4), FZB7P, DM5 (17), GXB7F, DM6 (8), GZB7F,
DM7 (218), INDSFL (235),
CTIME, DM8 (207), PI77R (2), PI77P1 (2), DM9 (4),
CMT77P (2), PI77R1 (2), DM11 (4), PI77R1 (2), DM11 (48),
CXG77F (2), XG77F1 (12), YG77F (2), YG77F1 (12),
CZG77F (2), ZG77F1 (2), DM13 (52),
CNSTRUT, MASS (5), RX (5), PY (5), RZ (5), THETAU (5), ERDEG, RGR,
CNTIRES (5), ZLR0 (5), H (5), DELTAM1 (5), MOMENT (5),
CRF (5), VZ, ITD, PZERO (5), VZLP0 (5), A (5), P20 (5), V2L (5),
CAC (5), IL, S2T (5), E3L (5), C2L (5), MASS2 (5), MUS (5),
CGC (5), DE (5), C2C (5), C2L (5), NVGPT, NPP, MB (5), RLT, NDELTA,
CES (5), SB (5), S021 (2), S022 (2), S023 (2), S024 (2), S025 (2)
COMMON/DIRLOH/
CSD1 (2), S012 (2), S013 (2), S014 (2), S015 (2),
CS1 (2), SS2 (2), S3 (2), S4 (2), S5 (2),
CS2021 (2), S2022 (2), S2023 (2), S2024 (2), S2025 (2),
CS2011 (2), S2012 (2), S2013 (2), S2014 (2), S2015 (2),
CS21 (2), S22 (2), S23 (2), S24 (2), S25 (2),
CMTD11 (2), CMTD12 (2), CMTD13 (2), CMTD14 (2), CMTD15 (2),
CMT2 (2), CMT3 (2), CMT4 (2), CMT5 (2),
CAI (5), U1 (5), ULLTA1, ULLTA2, ULLTA3, DELTA4, DELTA5,
DOELT1, DOELT2, DOELT3, DOELT4, DOELT5, ISTAGE,
CPRTH1, IPLT, ISDF, ISTPL1, ISTPL2, ISTPL3, ISTPL4, ISTPL5,
CMT14 (22), ID (5), DM15 (127), INULG, LM16 (117), CASK (44),
*DM17, NMODL, DM18 (4), SXMOD (101), SYMOD (100), SZMOD (101), DM19 (1686),
*G202 (2), DM22 (2)
REAL MASS, MOMENT, MASS2, MUS, NTIRES, MO
DIMENSION ULGAUT (14), ULGDE (47), ILL (7), DLGE (299)
COMMON/LGAUTS/ARG1, ARG13, ARG31, ARG33, AMA (5), VAXLE (5)
COMMON/LGJL/LA (25), FC2 (5), P2 (5), PRES (5), C (5), IPPT, LTPT
COMMON/LG/FXP, FYH, FZM, LH, MH, NM, EPSLO2
COMMON/LG/A11 (5), A13 (5), A31 (5), A33 (5), RRCGX (5),
CRL (5), RI (5), RY (5), RZ (5), RAY (5), RAZ (5), THP (3), ZZERO (5),
CX2 (5), YR (5), EPSLON (5), P4 (5), FDELTA (5),
CFTRZ (5), RJX (5), RUY (5), R0Z (5), RDXG (5), RUYG (5), RUZG (5),
CVTX (5), VTY (5), VTZ (5), L2 (5), VGPT (5), FTRX (5), FTRY (5),
CUX (5), UY (5), UZ (5), FI (5), FDX (5), F0Y (5), FF (5), AA (5), C2 (5),
CG2 (5), SF (5), PSKD (5), MUVP (5), MTRX (5), MTRY (5),
CMTB7 (5), HA (5), RG11, RG13, RG31, RG33, IPRT,
CHTX, HTY, HTZ, SFTRX, SFTRY, SFTRZ, FTRA,
CFTRA, FTRC, SMTRX, SMTRY, SMTRZ
COMMON/FLXUP/GFORC2 (14), GFORC3 (148), GFORC4 (148), BH1 (308)
EQUIVALENCE (ULGAUT (1), ARG11), (DLG0E (1), LA (1)),
* (DLG (1), FXM), (DLGE (1), A11 (1))
COMMON/TA85PC/DDMM1 (1, 3), LOC (7)
COMMON/HTCDH/HT, HT1, HT2
REAL MUVP, MTRX, MTRY, MTRZ, HA,
CHTX, HTY, HTZ, LH, MH, NM
DIMENSION DELTA (5), DDELTA (5), P (5),
C S02 (2, 5), S01 (2, 5), S (2, 5), S202 (2, 5), S201 (2, 5), S2 (2, 5),
COMETD1 (2, 5), OHET (2, 5)
EQUIVALENCE (P (1), PRES (1))
EQUIVALENCE (DELTA (1), DELTA1), (DDELTA (1), DDELTA1)

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C
C EQUIVALENCE
C(SD21(1),S2(1,1)),(SD11(1),SD1(1,1)),(S1(1),S(1,1)),
C(S2D21(1),S2D2(1,1)),(S2D11(1),S2D1(1,1)),(S21(1),S2(1,1)),
C(OMTD1(1),OMETD(1,1)),(OMT1(1),OMET(1,1))
C PRE DATA INITIALIZATION
DO 1 I=1,14
1  DLGAUT(I)=0.
DO 2 I=1,47
2  DLGDE(I)=J.
DO 3 I=1,7
3  DLG(I)=0.
DO 4 I=1,299
4  DLGE(I)=0.
ISTAGE=0
IPLT=0
IPPT=0
LTPT=1
ISDF=0
ISTPL1=0
ISTPL2=J
ISTPL3=J
ISTPL4=0
ISTPL5=J
EPSLO2=J.
RETURN
*****
C ENTRY LGEAR2
C *****
FXH=0.
FYH=L.
FZH=0.
LM=J.
HM=0.
NM=J.
ERR=.01745329*ERDEG
RG11=COS(ERR)
RG13=-SIN(ERR)
RG31=-RG13
RG33=RG11
ARG11=RG11
ARG13=RG13
ARG31=-RG31
ARG33=RG33
IF(INDLG.EQ.C)RETURN
INITIALIZATION AFTER DATA READ IN
VARIABLES TO BE INTEGRATED
      (OMTD1,OMT1 )
      (OMTD2,OMT2 )
      (OMTD3,OMT3 )
      (OMTD4,OMT4 )
      (OMTD5,OMT5 )
      (SD21 ,SD11 )
      (SD22 ,SD12 )
      (SD23 ,SD13 )
      (SD24 ,SD14 )
      (SD25 ,SD15 )
      (S2D21,S2D11 )
      (S2D22,S2D12 )
      (S2D23,S2D13 )
      (S2D24,S2D14 )
      (S2D25,S2D15 )
      (SD11 ,S1 )
      (SD12 ,S2 )
      (SD13 ,S3 )
      (SD14 ,S4 )
      (SD15 ,S5 )
      (S2D11,S21 )
      (S2D12,S22 )
      (S2D13,S23 )
      (S2D14,S24 )
      (S2D15,S25 )
      IF(INDLG.EQ.2)GO TO 5
NDEQ=5*NSTRUT
IF(IL.NE.J)NDEQ=3*NSTRUT
CALL INPU(NDEQ,LA)

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DO 10 I=1,NSTRUT
THETAR=.1745329*THETAD(I)
A11(I)=COS(THETAR)
A13(I)=-SIN(THETAR)
A31(I)=-A13(I)
A33(I)=A11(I)
10 RRCGX(I)=A11(I)*RX(I)+A13(I)*RZ(I)
IPRT=
RETURN
*****
C
C INITIAL PRINT
C ENTRY LG=4
C *****
C
C RETURN
C *****
C
C ENTRY LGEAR3
C *****
C
C MAIN COMPUTATIONAL AREA
C RL MATRIX ELEMENTS
C IF (INDLG.EQ.1) RETURN
C RL(1,1)=JCL1*RG11+JCL3*RG13
C RL(1,2)=JCL2
C RL(1,3)=JCL1*RG31+JCL3*RG33
C RL(2,1)=DCH1*RG11+DCH3*RG13
C RL(2,2)=UCH2
C RL(2,3)=DCH1*RG31+DCH3*RG33
C RL(3,1)=DCH1*RG11+DCH3*RG13
C RL(3,2)=UCH2
C RL(3,3)=JCH1*RG11+JCH3*RG33
C CALL LGEAR3
C
C CALCULATION OF S2D2, S2D1, AND S2
DO 100 I=1,NSTRUT
IF (INDLG.EQ.2) GO TO 2.
IF (IL.HC.) GO TO 59
THP(1)=S2D1(1,I)-A2(I)*S2D1(1,I)/A(I)
S2D2(1,I)=(P(I)-P2(I))*A2(I)/C(I)*THP(1)*ABS(THP(1))
C=S2D1(1,I)*C2(I)*ABS(S2D1(1,I))+C2L(I))
C/MAS32(1)+G2(I)-S2(I)+S2D2(1,I)
HT2=HT
IF (S2D1(1,I)) 46, 87, 88
86 TTIME=S2(1,I)/ABS(S2D1(1,I))
89 IF (TTIME.GE.HT) GO TO 87
HT2=TTIME
GO TO 87
88 TTIME=(S2(I)-S2(1,I))/S2D1(1,I)
GO TO 89
87 CONTINUE
IF (S2(1,I).GT.(-ES2(I))) GO TO 58
WRITE(6,57) I, I, S2(1,I)
57 FORMAT(58X, 5H -S2(1,I), 14H) EXCEEDED/
C58X, 3HS2(1,1,4H) = E15.7)
58 IF (S2(1,I).LE.ES2(I)) GO TO 61
IF (S2(1,I).LE.(S2(I)-ES2(I))) GO TO 141
IF (S2(1,I).LE.(S2(I)+ES2(I))) GO TO 62
WRITE(6,53) I, I, S2(1,I)
63 FORMAT(54X, 5H ES2(1,I), 14H) EXCEEDED/
C58X, 3HS2(1,1,4H) = E15.7)
62 IF (S2D1(1,I).GT.0.) S2D1(1,I)=0.
IF (S2D2(1,I).LT.0.) GO TO 141
GO TO 143
61 IF (S2D1(1,I).LT.0.) S2D1(1,I)=0.
IF (S2D2(1,I).LT.0.) GO TO 143
141 FC2(I)=0.
GO TO 60
140 FC2(I)=-MAS32(I)*S2D2(1,I)

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○ S2D2(1,I)=..
GO TO 83
59 S2D2(1,I)=..
S2D1(1,I)=..
S2(1,I)=..
FC2(1)=-P(I)-P2(I)*A2(I)-C(I)*SD1(1,I)*ABS(SD1(1,I))
GO TO 94
68 CONTINUE
I1=2*I+3*NSTPUT-1
I2=I1+1
CALL INTEG(LA(I1),S2D2(1,I))
CALL INTEG(LA(I2),S2D1(1,I))
94 CONTINUE
C COMPUTATION OF AA(I)
TMP(2)=0.
IF(SD1(1,I).NE.J)TMP(2)=SD1(1,I)/ABS(SD1(1,I))
SF(I)=-P(I)*(A(I)-A2(I))-P2(I)*A2(I)+FC2(1)-S2D1(1,I)*
C(C2(I)*ABS(S2D1(1,I))+C2L(I))-FF(I)*TMP(2)
AA(I)=(FT(I)+SF(I))/MASS(I)
C CALCULATION OF SD2, SD1, AND S
C CALCULATION OF OMETD1(I) AND OMET(I)
SD2(1,I)=SR(I)+AA(I)-GZ(I)
HT1=HT
IF(SD1(1,I))76,77,78
76 TTIME=S(1,I)/ABS(SD1(1,I))
79 IF(TTIME.GE.HT)GO TO 77
HT1=TTIME
GO TO 77
78 TTIME=(SD1(I)-S(1,I))/SD1(1,I)
GO TO 73
77 CONTINUE
IF(S(1,I).GT.(-ES(I)))GO TO 50
WRITE(6,44)I,I,S(1,I)
49 FORMAT(58X,4H-ES(,11,14H) EXCEEDED/
C58X,2HS(,11,4H) = E15.7)
50 IF(S(1,I).LE.-S(I))GO TO 51
IF(S(1,I).LE.(SD1(I)-IS(I)))GO TO 55
IF(S(1,I).LE.(SD1(I)+ES(I)))GO TO 52
WRITE(6,53)I,I,S(1,I)
53 FORMAT(58X,4H ES(,11,14H) EXCEEDED/
C58X,2HS(,11,4H) = E15.7)
52 IF(SD1(1,I).GT.J)SD1(1,I)=0.
IF(SD2(1,I).LT.J)GO TO 55
SD2(1,I)=J.
GO TO 55
51 IF(SD1(1,I).LT.C.)SD1(1,I)=0.
IF(SD2(1,I).LT.C.)SD2(1,I)=0.
55 CONTINUE
I2=2*I+NSTPUT-1
I1=I2+1
CALL INTEG(LA(I2),SD2(1,I))
CALL INTEG(LA(I1),SD1(1,I))
20 TMP(1)=RZ-PO(I)-DELTA(I)
IF(CASK(I).GT.1.E-15)GO TO 200
HA(I)=-FTRY(I)*TMP(1)*RI(2,1,I)+FTRX(I)*TMP(1)
C*RI(2,2,I)
GO TO 201
200 HA(I)=TMP(1)*SQRT(FTRY(I)*FTRY(I)+FTRX(I)*FTRX(I))
HA(I)=SIGN(HA(I),-VAXLE(I)-OMET(1,I)*TMP(1))
201 ANA(I)=HA(I)
IF(INDLG.EQ.2)GO TO 100
IF(IB(I).NE.(-1))GO TO 48
OMETD1(1,I)=..
OMET(1,I)=..
○ GO TO 21

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) TMP(1)=J.
IF (OMET(1,1).NE.L.) TMP(1)=OMET(1,1)/ABS(OMET(1,1))
21 OMETD1(1,1)=(HA(I)-HB(I)*TMP(1))/(NTIRES(I)*MOMENT(I))
100 CALL INTEG(LA(I),OMETD1(1,1))
C CONTINUE
CALCULATION OF FTRA, FTRB, AND FTRC
SFTRX=.
SFTRY=.
SFTRZ=.
DO 70 I=1,NSTRUT
SFTRX=SFTRX+FTRX(I)
SFTRY=SFTRY+FTRY(I)
70 SFTRZ=SFTRZ+FTRZ(I)
FTRA=RL(1,1)*SFTRX+RL(1,2)*SFTRY+RL(1,3)*SFTRZ
FTRB=RL(2,1)*SFTRX+RL(2,2)*SFTRY+RL(2,3)*SFTRZ
FTRC=RL(3,1)*SFTRX+RL(3,2)*SFTRY+RL(3,3)*SFTRZ
C CALCULATION OF MTX, MTY, AND MTZ
SMTRX=.
SMTRY=.
SMTRZ=.
DO 75 I=1,NSTRUT
SMTRX=SMTRX+MTRX(I)
SMTRY=SMTRY+MTRY(I)
75 SMTRZ=SMTRZ+MTRZ(I)
MTX=RL(1,1)*SMTRX+RL(1,2)*SMTRY+RL(1,3)*SMTRZ
MTY=RL(2,1)*SMTRX+RL(2,2)*SMTRY+RL(2,3)*SMTRZ
MTZ=RL(3,1)*SMTRX+RL(3,2)*SMTRY+RL(3,3)*SMTRZ
C CALCULATION OF FXH, FYH, FZH, LH, MH, AND NH
FXH=.
FYH=.
FZH=.
LH=.
MH=.
NH=.
DO 82 I=1,NSTRUT
FXH=FXH+FTXH(I)
FYH=FYH+FTYH(I)
FZH=FZH+FTZH(I)
LH=LH+LH(I)
MH=MH+MH(I)
NH=NH+NH(I)
DO 14 IL4=1,NMODE
NBB=(IL4-1)*NSTRUT+1
OFXH=OFXH-MASS(I)*SXMOD(NBB)*GGD2(IL4)
OFYH=OFYH-MASS(I)*SYMOD(NBB)*GGD2(IL4)
OFZH=OFZH-MASS(I)*SZMOD(NBB)*GGD2(IL4)
N3H=(I-1)*NMODE+IL4
OLH=OLH-MASS(I)*GFORD2(NBH)*GGD2(IL4)
OMH=OMH-MASS(I)*GFORD3(NBH)*GGD2(IL4)
14 ONM=ONM-MASS(I)*GFORD4(NBH)*GGD2(IL4)
BFX=BFX+OFXH
BFY=BFY+OFYH
BFZ=BFZ+OFZH
OLH=OLH+OLH
OMH=OMH+OMH
ONM=ONM+ONM
TMP(1)=MASS(I)*GD2(1,I)
FXH=FXH+TMP(1)*A31(I)
FYH=FYH+

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FZH=FZH+TMP(1)*A13(I)
LN=LN+TMP(1)*A11(I)*RY(I)
MM=MM+TMP(1)*RRCGX(I)
NM=NM+TMP(1)*A13(I)*RY(I)
FXM=FXM+BFX+FTRA
FYM=FYM+BFY+FTRB
FZM=FZM+BFZ+FTRC
L=L+LM+BLM+MTX
MM=MM+BMM+MTY
NM=NM+BNM+MTZ
RETURN
END
SUBROUTINE LGRA3C
COMMON/DIRCOM/CM1(136),AMASS,DM2(147),DCL1,DCM1,
CCCN1,DCL2,DCM2,DCN2,DCL3,DCN3,CCN3,DM3(99),FX07F,
CDUM4(3),FYH7P(4),FZ07F,DM5(17),GX07F,DM6(8),GZ07F,
COM7(186),INDC1,INDC2,INDC3,INDC4,DM15(28),INDSTE,DM18(234),
CTIME,LM8(237),PI77K,DM19,PI77L,DM9(5),
C0177R,DM24,Q177R1,DM15(5),R177L,DM17,R177R1,DM11(49),
CXG77F,DM13,XG77F,DM21(11),YG77F,DM21,YG77F1,DM22(11),
CZG77F,DM23,ZG77F,DM13(46),NSHAIN,HS2NDY(6),
CNSTRUT,MASS(5),RX(5),RY(5),RZ(5),THETA(5),ERDEC,RGR,
CNTIRES(5),NZERO(5),W(5),DELTA(5),MOMENT(5),
CRF(5),VZ,IFD,PZERO(5),VZERO(5),A(5),P2J(5),V2G(5),
GAZ(5),IL,S2T(5),LS2(5),C2L(5),MASS2(5),MUS(5),
CCG(5),CE(5),C2C(5),C2E(5),NVGPT,NPP,HB(5),RLT,NDELTA,
CES(5),SU(5),SU21(2),SU22(2),SD23(2),SD24(2),SD25(2)
COMMON/DIRCOM/
CS011(2),S012(2),S013(2),SD14(2),SD15(2),
CS1(2),SS2(2),S3(2),S4(2),S5(2),
CS2D21(2),S2D22(2),S2D23(2),S2D4(2),S2D25(2),
CS2D11(2),S2D12(2),S2D13(2),S2D14(2),S2D15(2),
CS2(2),S22(2),S23(2),S24(2),S25(2),
COMT011(2),OMT012(2),OMT013(2),OMT014(2),OMT015(2),
COMT1(2),OMT2(2),OMT3(2),OMT4(2),OMT5(2),
CAI(5),BI(5),DELTA1,DELTA2,DELTA3,DELTA4,DELTA5,
CDELTA1,DELTA2,DELTA3,DELTA4,DELTA5,ISTAGE,
CPRTMIN,IPLT,ISOF,ISTPL1,ISTPL2,ISTPL3,ISTPL4,ISTPL5,
COM14(262),CASK(5),DM25(39),DM26,NHOOE,DM27(40),SXMOU(100),
*SYM00(100),SZMOD(1,1),DM28(1646),GQ(20),GQD1(2),GQD2(20),
*DDM29(2)
REAL MASS,MOHENT,MASS2,MUS,MTIRES,MH
COMMON/LGAUTS/ARG11,ARG13,ARG31,ARG33,AMA(5),VAXLE(5)
COMMON/LG0E/LA(29),FC2(5),P2(5),PRES(5),C(5),IPPT,LTPT
COMMON/LG/FXY,FYM,FZM,LN,MM,NM,EPSLO2
COMMON/LGE/A11(5),A13(5),A31(5),A33(5),RRCGX(5),
CRL(3,3),RI(3,3,5),RAX(5),RAY(5),RAZ(5),TMP(3),ZZERO(5),
CXR(5),YR(5),EPSLO(5),PA(5),FDLTA(5),
CFTRZ(5),RDX(5),ROY(5),RDZ(5),RDXG(5),RDYG(5),RDZG(5),
CVTX(5),VTY(5),VTZ(5),LZ(5),VGPT(5),FTRX(5),FTRY(5),
CDX(5),DY(5),DZ(5),FT(5),FDX(5),FDY(5),FF(5),AA(5),C2(5),
CSR(5),SF(5),PSKD(5),HUVF(5),HTFX(5),HTY(5),
CHTRZ(5),HA(5),RG11,RG13,RG31,RG33,IPRT,
CHTX,HTY,HTZ,SFTRX,SFTPY,SFIRZ,FTRA,
CFTRD,FTRC,SMTRX,SMTRY,SMTRZ
COMMON/TA3SRC/DUMH1(1,3),LOC(7)
REAL MUVP,HTPX,HTRY,HTRZ,MA,
CHTX,HTY,HTZ,LN,MM,NM
DIMENSION DELTA(5),ODELTA(5),P(5),
CSD2(2,5),SD1(2,5),S(2,5),S2D2(2,5),S211(2,5),S2(2,5),
COMET01(2,5),OMET(2,5)
DIMENSION TEMP1(3),TEMP2(3)
EQUIVALENCE (P(1),PRES(1))
EQUIVALENCE (DELTA(1),DELTA1),(ODELTA(1),ODELT1)
EQUIVALENCE

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C(S201(1),S202(1,1),S201(1),S201(1,1),S21(1),S21(1,1),
C(S202(1),S202(1,1),S201(1),S201(1,1),S21(1),S21(1,1)),
C(OMT01(1),OMETO(1,1),OMT1(1),OMET(1,1))
DO 13, I=1,NSTRUT
  FI=I
C  RI MATRIX ELEMENTS
  DO 2, J=1,3
    TEMP1(J)=1.
    TEMP2(J)=1.
    RI(1,J,I)=A11(I)*RL(1,J)+A13(I)*RL(3,J)
    RI(2,J,I)=RL(2,J)
    RI(3,J,I)=A31(I)*RL(1,J)+A33(I)*RL(3,J)
C 2J POSITION DEPENDENT CALCULATIONS
C  DO 11 ILP=1,NMOD
  MOD=(ILP-1)*NSTRUT+I
  TEMP1(1)=F-4P(1)+5X*MOD*MOD*GQ(ILP)
  TEMP1(2)=TEMP1(2)+5Y*MOD*MOD*GQ(ILP)
  11 TEMP1(3)=TEMP1(3)+5Z*MOD*MOD*GQ(ILP)
  TMP(1)=F(1)-5(1,E)
  TMP(2)=RX(1)+A31(I)*TMP(1)+TEMP1(1)
  TMP(3)=RX(1)+A33(I)*TMP(1)+TEMP1(3)
  RAX(I)=JCL1*TMP(2)+DCM1*(RY(I)+TEMP1(2))+DCN1*TMP(3)
  RAY(I)=JCL2*TMP(2)+DCM2*(PY(I)+TEMP1(2))+DCN2*TMP(3)
  RAZ(I)=JCL3*TMP(2)+DCM3*(RY(I)+TEMP1(2))+DCN3*TMP(3)
  TMP(1)=(XG77F-RGP+RAX(I))
  TMP(2)=ZG77F+RAY(I)
  ZZERO(I)=TMP(1)*RG31+TMP(2)*RG13
  XR(I)=TMP(1)*RG11+TMP(2)*RG13
  YR(I)=YG77F+RAY(I)
  IF(XR(I).LE.0.)GO TO 25
  IF(XR(I).GE.FLT)GO TO 25
  CALL TLU(XR(I),LOC(2),EPSLON(I))
  GO TO 24
  25 EPSLON(I)=0.
  24 DELTA(I)=ZZERO(I)+EPSLON(I)
  DDELTA(I)=DELTA(I)
  IF(DELTA(I).LE.0.)GO TO 26
  IF(DELTA(I).LE.DELTAM(I))GO TO 27
  W=ITE(6,28)I,DELTA(I)
  28 FORMAT(36X,24HTIRE DEFLECTION EXCEEDED,1X,6HDELTA(,I1,4H) = ,
  C(15.7)
  CALL LGASP
  INDSTE=1
  RETURN
  26 DELTA(I)=1.
  27 CONTINUE
  P(I)=PZERO(I)*VZERO(I)/(VZERO(I)+A2(I)*S2(1,I)-
  CS(1,I)*A(I))
  P2(I)=1.
  TMP(1)=V33(I)-A2(I)*S2(1,I)
  IF(TMP(1).EQ.0.)GO TO 31
  P2(I)=P2(I)*V2(I)/TMP(1)
  31 IF(IPD.EQ.0.)GO TO 32
  FDELTA(I)=1.
  IF(DELTA(I).NE.0.)FDELTA(I)=AI(I)*(DELTA(I))*BI(I)
  GO TO 33
  32 CALL HIHC(3,LOC(1),NDELTA,NSTRUT,OU,OU,DELTA(I),FI,OU,OU,FDELTA(I))
  1)
  33 FTRZ(I)=-HIIPES(I)*FDELTA(I)
  C  CALCULATION OF COMPONENTS OF GROUND PLANE
  C  VELOCITIES VTX(I) AND VTY(I)
  TMP(1)=(RF(I)-S(1,I))
  DO 12 IL2=1,NMOD
  NO=(IL2-1)*NSTRUT+I
  TEMP2(1)=TEMP2(1)+(QI77R*S2MOD(NO)-RI77R*SYM0D(NO))*GQ(IL2)

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C+SMOD(ND)*GCD1(IL2)
TEMP2(2)=TEMP2(1)+(RI77R*SMOD(ND)-PI77R*SZMOD(ND))*GQ(IL2)
C+SYM0D(ND)*GDD1(IL2)
12 TEMP2(3)=TEMP2(1)+(PI77R*SYM0D(ND)-QI77R*SMOD(ND))*GQ(IL2)
C+SZMOD(ND)*GDD1(IL2)
RDX(I)=-SD1(1,I)*A31(I)+QI77R*(TMP(1)*A33(I)+RZ(I))-RI77R
C*RY(I)=TEMP2(1)
RUY(I)=TMP(1)*(RI77R*A31(I)-PI77R*A33(I))+RI77R*RX(I)-PI77R
C*RZ(I)=TEMP2(2)
RDZ(I)=-SD1(1,I)*A33(I)-TMP(1)*QI77R*A31(I)+PI77R*RY(I)-QI77R
C*RX(I)=TEMP2(3)
RDXG(I)=XG77F1+UGL1*RDX(I)+DCN1*RUY(I)+DCN1*RDZ(I)
RJYG(I)=YG77F1+UGL2*RDX(I)+DCN2*RUY(I)+DCN2*RDZ(I)
RDZG(I)=ZG77F1+UGL3*RDX(I)+DCN3*RUY(I)+DCN3*RDZ(I)
TMP(1)=RZMOD(I)-ULLTA(I)
TMP(2)=OMET(1,I)*RI(2,2,I)*TMP(1)
TMP(3)=OMET(2,I)*RI(2,1,I)*TMP(1)
VTX(I)=RG11*POXG(I)+RG13*RDZG(I)+TMP(2)
VTY(I)=RG11*POYG(I)-TMP(3)
VTZ(I)=RG11*POZG(I)+RG33*RDZG(I)
C CALCULATION OF GROUND PLANE FORCES FTRX(I) AND FTRY(I)
TMP(1)=RG11*POXG(I)+RG13*POZG(I)
VAXLE(I)=SQRT(TMP(1)*TMP(1)+RDYG(I)*RDYG(I))
IF(CASK(I).GT.1.E-10)GO TO 34
VGPT(I)=SQRT(VTX(I)*VTX(I)+VTY(I)*VTY(I))
GO TO 35
34 TMP(1)=VAXLE(I)+OMET(1,I)*(RZERO(I)-DELTA(I))
VGPT(I)=ABS(TMP(1))
35 IF(VGPT(I).LE.VZ)GO TO 40
PSKD(I)=J.
IF(ABS(VAXLE(I)).LE.1.E-8)GO TO 42
PSKC(I)=VGPT(I)/VAXLE(I)
42 CALL TLV(PSKC(I),LOC(3),HUVPI(I))
FTRX(I)=HUVPI(I)*FTRZ(I)/VGPT(I)
IF(CASK(I).GT.1.E-10)GO TO 50
TMP(3)=VTY(I)
GO TO 51
50 TMP(3)=(VTY(I)+TMP(3))/VAXLE(I)*TMP(1)
51 FTRY(I)=FTRX(I)*TMP(3)
IF(CASK(I).GT.1.E-10)GO TO 52
TMP(2)=VTX(I)
GO TO 53
52 TMP(2)=(VTX(I)-TMP(2))/VAXLE(I)*TMP(1)
53 FTRX(I)=FTRX(I)*TMP(2)
GO TO 41
40 FTRX(I)=J.
FTRY(I)=U.
41 CONTINUE
C CALCULATION OF HTRX(I), HTRY(I), AND HTRZ(I)
DX(I)=RG11*RAX(I)+RG13*RAZ(I)
DY(I)=RAY(I)
DZ(I)=RG11*RAZ(I)+RG33*RAZ(I)+RZERO(I)-DELTA(I)
HTRX(I)=DY(I)*FTRZ(I)-DZ(I)*FTRY(I)
HTRY(I)=DZ(I)*FTRX(I)-DX(I)*FTRZ(I)
HTRZ(I)=DX(I)*FTRY(I)-DY(I)*FTRX(I)
C CALCULATION OF FI(I)
FI(I)=-FTRX(I)*RI(3,1,I)-FTRY(I)*RI(3,2,I)
C-FTRZ(I)*RI(3,3,I)
C CALCULATION OF FFI(I)
FDX(I)=RI(1,1,I)*FTRX(I)+RI(1,2,I)*FTRY(I)+RI(1,3,I)*FTRZ(I)
FDY(I)=RI(2,1,I)*FTRX(I)+RI(2,2,I)*FTRY(I)+RI(2,3,I)*FTRZ(I)
FF(I)=MUS(I)*SQRT(FDX(I)*FDX(I)+FDY(I)*FDY(I))
C CALCULATION OF GZ(I)
TMP(3)=-A2(I)/A(I)
C(I)=0.

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C2(I)=4
IF(SD1(1,I)+TMP(3)*S2D1(1,I).GE.3.)GO TO 43
IF(INDC(2,EQ.0)GO TO 44
CALL HIH(3,LOC(5),NSMAIN,NSTRUT,DU,DU,S(1,I),FI,DU,DU,C(I))
GO TO 44
43 IF(INDC(1,EQ.0)GO TO 44
CALL HIH(3,LOC(4),NSMAIN,NSTRUT,DU,DU,S(1,I),FI,DU,DU,C(I))
44 IF(SD1(1,I).GE.3.)GO TO 45
IF(INDC(4,EQ.0)GO TO 46
CALL HIH(3,LOC(7),NS2NDY,NSTRUT,DU,DU,S(1,I),FI,DU,DU,C2(I))
GO TO 46
45 IF(INDC(3,EQ.0)GO TO 46
CALL HIH(3,LOC(6),NS2NDY,NSTRUT,DU,DU,S(1,I),FI,DU,DU,C2(I))
46 GZ(I)=A31(1)*GX87F+A33(1)*GZ87F
C COMPUTATION OF SR(I)
TEMP3=0
TMP(1)=RX(I)*RI77R-RZ(I)*PI77R
DO 13 IL3=1,NMODE
NDO=(IL3-1)*NSTRUT+1
13 TEMP3=TEMP3+A31(1)*SXMOD(NDO)*GQ02(IL3)+A33(1)*SZMOD(NDO)
C GQ02(IL3)
SR(I)=A31(1)*FX87P/AMASS+A33(1)*FZ87P/AMASS
C+A31(1)*(RZ(I)*QI77R-RY(I)*RI77R)+A33(1)
C*(RY(I)*PI77R-RX(I)*QI77R)+A31(1)*(QI77R*
C*(RY(I)*PI77R-RX(I)*QI77R)-RI77R*TMP(1))
C+A33(1)*(PI77R*TMP(1)-QI77R*(RZ(I)*QI77R
C-RY(I)*RI77R))+TEMP3
100 CONTINUE
C SAVE EPSLON(2) FOR SACS SUBROUTINE
EPSLO2=EPSLON(2)
RETURN
END
SUBROUTINE FLEX1
C SUBROUTINE FLEX1 EMPLOYS A MATRIX APPROACH TO DETERMINE THE DYNAMIC
C RESPONSE OF SELECTED POINTS ON A FLEXIBLE AIRPLANE
COMMON/DIRCOM/SKIPUP,DUO(7),AMINCR,DM1(13),AA77P,DM2(81),AA77F,
*DM3(35),AA77F,DM4(9),AA77F,AA77P,DM5(12),AX77F,DM6,AY77F,
*DM7(2),AZ77F,DM8(12),YA77P,DM(183),PI77R,DM11,PI77RL,DM11(5),
*QI77F,DM12,QI77F,DM13(5),RI77R,DM14,RI77RL,DM15(15),
*U77F,DM16(19),W77F,DM17(3),W77F,DM18(93),NSTRUT,
*HASS(5),RX(5),RY(5),RZ(5),DM19(32),RF(5),DM20(97),SD21(2),
*SD22(2),SD23(2),SD24(2),SD25(2),DM21(99),IN,DM22(153),
*INDLG,DM23(151),INDFLX,NMODE,GMASS1(20),GFREQ(20),
*SXMOD(10),SYMOD(10),SZMOD(10),SKC(5),TXMOD(90),
*OCHODE(50),APMCDE(120),NPTS,OUTHOD(120),ROIS(60),
*PF(120),GJ(20),GQ02(20),GQ02(20),DDM24(20),
COMMON/FLXOP/GFORC2(100),GFORC3(100),GFORC4(100),
*T(5),FCX,FCY,FCZ,XU2F(20),XD2T(20),YU2F(20),YD2T(20),
*ZD2T(20),XU1F(20),XD1T(20),YU1F(20),YD1T(20),ZD1F(20),ZD1T(20),
*XU0F(20),YU0F(20),ZU0F(20)
COMMON/LGE/A11(5),A13(5),A31(5),A33(5),DM24(279)
COMMON/HTCOM/HT,DDMR(2)
REAL MASS
DIMENSION GHAS(400),SHASS(25),GSMOD(400),CORNAS(20,20),
*QS(20),QS1(20),GFORC1(60),DIFF(5),RZA11(25),RZA13(25),RKSY(25),
*SDD(10),VARY1(3),OMX01H(5),OMY01H(5),OMZ01H(5),GF(20),FDC(3),
*CTME1(120),GTF(20),SD0(3),SD1(3),SD2(3),TITL(16),LA(40),
*COEFF(20,20)
EQUIVALENCE (SD21(1),SDD(1))
DATA HDR/5H FLEX/, (TITL(I),I=1,16)/5HPOINT,4HXD2F,4HXD2T,4HYD2F,
*4HYD2T,4HZD2F,4HZD2T,4HXD1F,4HXD1T,4HYD1F,4HYD1T,4HZD1F,
*4HZD1T,4HXU0F,4HYU0F,4HZU0F/
C PRE DATA INITIALIZATION

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0 1 DO 1 I=1,400
    GHASS(I)=J.
    DO 2 I=1,25
    SHASS(I)=J.
    RZA11(I)=J.
    RXA13(I)=J.
    2 RKSY(I)=0.
    DO 15 I=1,40
    15 LA(I)=0
    NMODE=1
    RETURN

C ENTRY FLEX2
C IF(INDFLX.EQ.C.OR.INDLG.EQ.U)RETURN
HT=AMINER
NVAR=2*NMODE
CALL INUPD(NVAR,LA)

CCCCC FORMULATE TIME INVARIANT ARRAYS
FORM COUPLED GENERALIZED MASS MATRIX

DO 31 K=1,NMODE
NA=(K-1)*NMODE+K
30 GHASS(NA)=GHASS1(K)
DO 31 N=1,NSTRUT
    LLA=(N-1)*NSTRUT+N
    31 SHASS(LLA)=HASS(N)
    CALL GTPRO(SXMOD,SHASS,CTHP1,NSTRUT,NMODE,NSTRUT)
    CALL GHPRJ(CTHP1,SXMOD,GSMOD,NMODE,NSTRUT,NMODE)
    CALL GHADJ(GSMOD,GHASS,GHASS,NMODE,NMODE)
    CALL GTPRO(SYMOD,SHASS,CTHP1,NSTRUT,NMODE,NSTRUT)
    CALL GHPRJ(CTHP1,SYMOD,GSMOD,NMODE,NSTRUT,NMODE)
    CALL GHADJ(GSMOD,GHASS,GHASS,NMODE,NMODE)
    CALL GTPRO(SZMOD,SHASS,CTHP1,NSTRUT,NMODE,NSTRUT)
    CALL GHPRJ(CTHP1,SZMOD,GSMOD,NMODE,NSTRUT,NMODE)
    CALL GHADJ(GSMOD,GHASS,GHASS,NMODE,NMODE)
    CALL ARAY(1,NMODE,NMODE,2L,2,GHASS,COPHAS)
    CALL DECOMP(NMODE,COPHAS,COEF)

C FORM CONSTANT COMPONENTS OF TANGENTIAL ACCELERATION
CALL GTPRO(SXHCU,HASS,QS,NSTRUT,NMODE,1)
CALL GTPRO(SYMOD,HASS,QS1,NSTRUT,NMODE,1)
CALL CTIE(QS,QS1,CTHP1,NMODE,1,0,0,1)
CALL GTPRO(SZMOD,HASS,QS,NSTRUT,NMODE,1)
CALL CTIE(CTHP1,QS,GFORC1,NMODE,2,0,0,1)
DO 33 L=1,NSTRUT
    DIFF(L)=RF(L)-SKC(L)
    HA=(L-1)*NSTRUT+L
    RZA11(HA)=RZ(L)+DIFF(L)*A11(L)
    RXA13(HA)=RX(L)-DIFF(L)*A13(L)
    33 RKSY(HA)=RY(L)
    CALL GTPRO(SZMOD,RKSY,CTHP1,NSTRUT,NMODE,NSTRUT)
    CALL GTPRO(SYMOD,RZA11,GSMOD,NSTRUT,NMODE,NSTRUT)
    CALL GHSUB(CTHP1,GSMOD,GFORC2,NMODE,NSTRUT)
    CALL GTPRO(SXMOD,RZA11,CTHP1,NSTRUT,NMODE,NSTRUT)
    CALL GTPRO(SZMOD,RXA13,GSMOD,NSTRUT,NMODE,NSTRUT)
    CALL GHSUB(CTHP1,GSMOD,GFORC3,NMODE,NSTRUT)
    CALL GTPRO(SXHCU,RXA13,CTHP1,NSTRUT,NMODE,NSTRUT)
    CALL GTPRO(SXMOD,RKSY,GSMOD,NSTRUT,NMODE,NSTRUT)
    CALL GHSUB(CTHP1,GSMOD,GFORC4,NMODE,NSTRUT)

```

FORM INITIAL DISPLACEMENTS

```

SUM1=0.
SUM3=0.
DO 34 I=1,NSTRUT
SUM1=SUM1+A31(I)*SOD((I-1)*2+1)
34 SUM3=SUM3+A33(I)*SOD((I-1)*2+1)
VARY1(1)=AX77F-SUM1
VARY1(2)=AY77F
VARY1(3)=AZ77F-SUM3
CALL GMP40(GFORC1,VARY1,QS,NMODE,3,1)
DO 35 I=1,NSTRUT
OMXD1M(I)=PI7791*MASS(I)
OMYD1M(I)=OI77R1*MASS(I)
35 OMZD1M(I)=KI77R1*MASS(I)
CALL GMP40(GFORC1,OMXD1M,GF,NMODE,NSTRUT,1)
CALL GHAJJ(QS,GF,QS,NMODE,1)
CALL GMP40(GFORC3,OMYD1M,GF,NMODE,NSTRUT,1)
CALL GHAJJ(QS,GF,QS,NMODE,1)
CALL GMP40(GFORC4,OMZD1M,GF,NMODE,NSTRUT,1)
CALL GHAJJ(QS,GF,QS,NMODE,1)
CALL GTPRJ(TXMC0,I,GF,IN,NMODE,1)
CALL GMSUM(GF,QS,QS,NMODE,1)
FDC(1)=FCX
FJC(2)=FCY
FJC(3)=FCZ
CALL GTPRJ(DCHODE,FDC,GF,3,NMODE,1)
CALL GHAJJ(GF,QS,QS,NMODE,1)
DO 36 I=1,NMCO
NN=(I-1)*6+1
CTMP1(NN)=-ARMODE(NN)*AA77P
CTMP1(NN+1)=ARMODE(NN+1)*YA77P
CTMP1(NN+2)=-ARMODE(NN+2)*AA77P
CTMP1(NN+3)=ARMODE(NN+3)*AA77F
CTMP1(NN+4)=ARMODE(NN+4)*AA77F
36 CTMP1(NN+5)=ARMODE(NN+5)*AA77F
DO 37 II=1,NMODE
GF(II)=0.
DO 37 JJ=1,6
HJ=(II-1)*6+JJ
37 GF(II)=GF(II)+CTMP1(HJ)*PF(HJ)
CALL GHAJJ(GF,QS,QS,NMODE,1)
DO 38 IG=1,NMODE
GTF(IG)=MASS1(IG)*GFREQ(IG)**2.
38 GJ(IG)=QS(IG)/GTF(IG)
SKIPUP=.TRUE.
DO 39 I=1,NMODE
N22=2*I
CALL UPDAT(1,LA(N22),GQ(I),DU,DU,DU,DU)
39 CONTINUE
SKIPUP=.FALSE.
RETURN
ENTRY FLEX3
IF(INDFLX.EQ.0.OR.INDLG.EQ.0)RETURN
FORM VARYING COMPONENTS OF TANGENTIAL ACCELERATION

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```

SUM1=0.
SUM3=0.
DO 40 I=1,NSTRUT
SUM1=SUM1+A31(I)*SOD((I-1)*2+1)
40 SUM3=SUM3+A33(I)*SOD((I-1)*2+1)
VARY1(1)=AX77F-SUM1

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O VARY1(2)=AY77F
  VARY1(3)=AZ77F-SUM3
  CALL GMPRJ(GFORC1,VARY1,GTF,NMODE,3,1)
  DO 46 I=1,NMODE
46  QS(I)=0.
    CALL GHSUB(QS,GTF,OS,NMODE,1)
    DO 41 I=1,NSTRUT
      OMXD1H(I)=PI77R1*MASS(I)
      OMYD1H(I)=QI77R1*MASS(I)
41  OMZD1H(I)=KI77R1*MASS(I)

C   CALL GMPRJ(GFORC2,OMXD1H,GTF,NMODE,NSTRUT,1)
     CALL GHSUB(QS,GTF,OS,NMODE,1)
     CALL GMPRJ(GFORC3,OMYD1H,GTF,NMODE,NSTRUT,1)
     CALL GHSUB(QS,GTF,OS,NMODE,1)
     CALL GMPRJ(GFORC4,OMZD1H,GTF,NMODE,NSTRUT,1)
     CALL GHSUB(QS,GTF,OS,NMODE,1)

CCC FORM GENERALIZED THRUST MATRIX
    CALL GTPRJ(TXMOD,T,GTF,IN,NMODE,1)
    CALL GHADD(QS,GTF,OS,NMODE,1)

CCC FORM GENERALIZED DRAG CHUTE FORCES
    FDC(1)=FCX
    FDC(2)=FCY
    FDC(3)=FCZ
    CALL GTPRJ(DCMODE,FDC,GTF,3,NMODE,1)
    CALL GHADD(QS,GTF,OS,NMODE,1)

CCC FORM GENERALIZED AERO FORCES
    DO 42 I=1,NMODE
      NN=(I-1)*6+1
      CTMP1(NN)=-ARHODE(NN)*AA77P
      CTMP1(NN+1)=ARHODE(NN+1)*YA77P
      CTMP1(NN+2)=-ARHODE(NN+2)*ANA77P
      CTMP1(NN+3)=ARHODE(NN+3)*ALA77F
      CTMP1(NN+4)=ARHODE(NN+4)*AMA77F
42  CTMP1(NN+5)=ARHODE(NN+5)*ANA77F
      DO 43 II=1,NMODE
        GTF(II)=0.
        DO 43 JJ=1,6
          MJ=(II-1)*6+JJ
43  GTF(II)=GTF(II)+CTMP1(MJ)*PF(MJ)
        CALL GHADD(QS,GTF,OS,NMODE,1)

CCC FORM GENERALIZED STIFFNESS
    DO 44 IG=1,NMODE
      GTF(IG)=GQ(IG)*GHASS1(IG)*GFREQ(IG)**2.
44  QS(IG)=QS(IG)-GTF(IG)

CCC SOLVE FOR THE GENERALIZED ACCELERATION
    CALL SOLVE(NMODE,COEF,QS,GQD2)
    DO 45 I=1,NMODE
      NCON=(I-1)*2+1
      HCON=NCON+1
      CALL INTEG(LA(NCON),GQD2(I))
      CALL INTEG(LA(HCON),GQD1(I))
45  CONTINUE
    RETURN
  
```

```

C ENTRY FLEX4
C RETURN
C ENTRY FLEX5
C RETURN
C ENTRY FLEX6
C IF (INDFLX.EQ.0.OR.INDLG.EQ.0) RETURN
C IF (NPTS.EQ.1) RETURN
C FORM VARIABLES TO BE OUTPUT
C
CALL STFL(1,1,HDR)
CALL STFL(1,16,TITL)
DO 62 I=1,NPTS
DO 61 K=1,3
SJL(K)=0.
SOL(K)=0.
SJ2(K)=0.
DO 61 J=1,NMODE
NCON=((I-1)*3+K-1)*NMODE+J
SJL(K)=SJL(K)+OUTMOD(NCON)*GQ(J)
SOL(K)=SOL(K)+OUTMOD(NCON)*GQ01(J)
61 SD2(K)=SD2(K)+OUTMOD(NCON)*GQ02(J)
LX=(I-1)*3+1
LY=LX+1
LZ=LY+1
X02F(I)=S02(1)
X02T(I)=AX77F+X02F(I)+2.*(QI77R*S01(3)-RI77R*S01(2))+
*(PI77R*RI77R+QI77R)* (ROIS(LZ)+SDJ(3))+(PI77R*RI77R
*-RI77R)* (ROIS(LY)+SDJ(2))-(QI77R*QI77R+RI77R*RI77R)
* (ROIS(LX)+SDJ(1))
Y02F(I)=S02(2)
Y02T(I)=AY77F+Y02F(I)+2.*(RI77R*S01(1)-PI77R*S01(3))+
*(QI77R*PI77R+RI77R)* (ROIS(LX)+SDJ(1))+(QI77R*RI77R
*-PI77R)* (ROIS(LZ)+SDJ(3))-(RI77R*RI77R+PI77R*PI77R)
* (ROIS(LY)+SDJ(2))
Z02F(I)=S02(3)
Z02T(I)=AZ77F+Z02F(I)+2.*(PI77R*S01(2)-QI77R*S01(1))+
*(RI77R*QI77R+PI77R)* (ROIS(LY)+SDJ(2))+(RI77R*PI77R
*-PI77R)* (ROIS(LX)+SDJ(1))-(PI77R*PI77R+QI77R*QI77R)
* (ROIS(LZ)+SDJ(3))
X01F(I)=S01(1)
X01T(I)=U777F+X01F(I)+QI77R*(ROIS(LZ)+SDJ(3))-RI77R*
*(ROIS(LY)+SDJ(2))
Y01F(I)=S01(2)
Y01T(I)=V777F+Y01F(I)+RI77R*(ROIS(LX)+SDJ(1))-PI77R*
*(ROIS(LZ)+SDJ(3))
Z01F(I)=S01(3)
Z01T(I)=W777F+Z01F(I)+PI77R*(ROIS(LY)+SDJ(2))-QI77R*
*(ROIS(LX)+SDJ(1))
X00F(I)=S00(1)
Y00F(I)=S00(2)
Z00F(I)=S00(3)
PTN=FLOAT(I)
CALL STOVAR(8,PTN,X02F(I),X02T(I),Y02F(I),Y02T(I),Z02F(I),
*Z02T(I),X01F(I),
CALL STOVAR(8,X01T(I),Y01F(I),Y01T(I),Z01F(I),Z01T(I),X00F(I),
*Y00F(I),Z00F(I))
62 CONTINUE
RETURN

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C0 ENTRY FLEX7
  IF (INDFLX.EQ.3.OR.INDLG.EQ.6) RETURN
  RVAR=2.*FLOAT(NMODE)/4.
  K=IFIX(RVAR)
  IF (K.EQ.3) GO TO 71
  DO 70 I=1,K
    N=4*I-3
    MD1=2*I-1
    MD0=2*I
    CALL UPDAT(4,LA(N),GQD1(MD1),GQ(MD1),GQD1(MD0),GQ(MD0),DU)
70  CONTINUE
    L=2*K
    IF (L.EQ.NMODE) RETURN
71  M=4*K+1
    MP=2*K+1
    CALL UPDAT(2,LA(M),GQD1(MP),GQ(MP),DU,DU,DU)
    RETURN
  END
  SUBROUTINE DECCHP (NN,A,UL)
    DIMENSION A(20,20), UL(20,20), SCALES(20), IPS(20)
    COMMON IPS
    IF (NN.GT.1) GO TO 20
    UL(1,1)=A(1,1)
    RETURN
20  N=NN
C  INITIALIZE IPS, UL AND SCALES
    DO 5 I=1,N
      IPS(I)=I
      ROWNRH=J.J
      DO 2 J=1,N
        UL(I,J)=A(I,J)
        IF (ROWNRH-ABS(UL(I,J))) 1,2,2
1      ROWNRH=ABS(UL(I,J))
2      CONTINUE
        IF (ROWNRH) 3,4,3
3      SCALES(I)=1.0/ROWNRH
        GO TO 5
4      CALL SING(1)
        SCALES(I)=0.0
5      CONTINUE
C  GAUSSIAN ELIMINATION WITH PARTIAL PIVOTING
    NM1=N-1
    DO 17 K=1,NM1
      BIG=0.0
      DO 11 I=K,N
        IP=IPS(I)
        SIZE=ABS(UL(IP,K))*SCALES(IP)
        IF (SIZE-BIG) 11,11,10
10     BIG=SIZE
        IOXPIV=I
11     CONTINUE
        IF (BIG) 13,12,13
12     CALL SING(2)
        GO TO 17
13     IF (IOXPIV-K) 14,15,14
14     J=IPS(K)
        IPS(K)=IPS(IOXPIV)
        IPS(IOXPIV)=J
        KP=IPS(K)
15     PIVOT=UL(KP,K)
        KP1=K+1
        DO 16 I=KP1,N

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C      IP=IPS(I)
      EM=UL(IP,K)/PIVOT
      UL(IP,K)=-EM
      DO 16 J=KP1,N
      UL(IP,J)=UL(IP,J)+EM*UL(KP,J)
16    CONTINUE
17    CONTINUE
      KP=IPS(N)
      IF (UL(KP,N)) 19,18,19
18    CALL SING(2)
19    RETURN
      END
      SUBROUTINE SOLVE (NN,UL,B,X)
      DIMENSION UL(20,20), B(20), X(20), IPS(20)
      COMMON IPS
      IF (NN.GT.1) GO TO 5
      X(1)=B(1)/UL(1,1)
      RETURN
5     NN=N
      NP1=N+1
C
      IP=IPS(1)
      X(1)=B(IP)
      DO 2 I=2,N
      IP=IPS(I)
      IM1=I-1
      SUM=B(I)
1     DO 1 J=1,IM1
      SUM=SUM+UL(IP,J)*X(J)
2     X(I)=B(IP)-SUM
C
      IP=IPS(N)
      X(N)=X(N)/UL(IP,N)
      DO 4 IBACK=2,N
      I=NP1-IBACK
      I GUES (N-1),.....,1
C
      IP=IPS(I)
      IP1=I+1
      SUM=B(I)
      DO 3 J=IP1,N
      SUM=SUM+UL(IP,J)*X(J)
3     SUM=SUM+UL(IP,J)*X(J)
4     X(I)=(X(I)-SUM)/UL(IP,I)
      RETURN
      END
      SUBROUTINE SING (INHY)
11    FORMAT(54H,MATRIX WITH ZERO ROW IN DECOMPOSE. )
12    FORMAT(54H,SINGULAR MATRIX IN DECOMPOSE. ZERO DIVIDE IN SOLVE. )
      NOUT=6
C      NOUT=STANDARD OUTPUT UNIT
      GO TO (1,2),INHY
1     WRITE (NOUT,11)
      GO TO 1
2     WRITE (NOUT,12)
10    CALL EXERR(0)
      RETURN
      END
      SUBROUTINE AFAY (MODE,I,J,N,M,S,D)
      IDENT ARAY
      TITLE ARAY
      ADAPTED FROM S/360 SCIENTIFIC SUBROUTINE PACKAGE.
      (J6LA-CH-13X) VERSION III
      R. A. GARMOE. 68/16/69.
      .....

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* SUBROUTINE ARRAY
*
* PURPOSE
*   CONVERT DATA ARRAY FROM SINGLE TO DOUBLE DIMENSION OR VICE
*   VERSA. THIS SUBROUTINE IS USED TO LINK THE USER PROGRAM
*   WHICH HAS DOUBLE DIMENSION ARRAYS AND THE SSP SUBROUTINES
*   WHICH OPERATE ON ARRAYS OF DATA IN A VECTOR FASHION.
*
* .....
* DIMENSION S(1),D(1)
* IF (I.GT.1) GO TO 98
* IF (MODE.EQ.1) D(1)=S(1)
* IF (MODE.EQ.2) S(1)=D(1)
* RETURN
*
* 98 NI=N-I
*
* TEST TYPE OF CONVERSION
* IF(MODE-1) 100, 100, 120
*
* CONVERT FROM SINGLE TO DOUBLE DIMENSION
*
* 100 IJ=I*J+1
*   NM=N*J+1
*   DO 110 K=1,J
*   NM=NM-NI
*   DO 110 L=1,I
*   IJ=IJ-1
*   NM=NM-1
* 110 D(NM)=S(IJ)
*   GO TO 140
*
* CONVERT FROM DOUBLE TO SINGLE DIMENSION
*
* 120 IJ=0
*   NM=0
*   DO 130 K=1,J
*   DO 125 L=1,I
*   IJ=IJ+1
*   NM=NM+1
* 125 S(IJ)=D(NM)
* 130 NM=NM+NI
*
* 140 RETURN
* END
* SUBROUTINE CTIE(A,B,R,N,M,MSA,MSB,L)
*   IDENT CTIE
*   TITLE CTIE
*   ADAPTED FROM S/36L SCIENTIFIC SUBROUTINE PACKAGE.
*   (36JA-CH-J3X) VERSION III
*   R. A. GARMOE. 08/16/69.
*
* .....
* SUBROUTINE CTIE
*
* PURPOSE
*   ADJOIN TWO MATRICES WITH SAME ROW DIMENSION TO FORM ONE
*   RESULTANT MATRIX (SEE METHOD)
*
* .....

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C 32 TF=IX-JX) 36,32,36
G 36 IRX=IX
** IR=IRX
** RETURN
** END
SUBROUTINE GTPRD(A,B,R,N,M,L)
IDENT GTPRD
TITLE GTPRD
ADAPTED FROM S/360 SCIENTIFIC SUBROUTINE PACKAGE.
(36LA-CM-13X) VERSION III
R. A. GARMOE. 08/16/69.
.....
SUBROUTINE GTPRD
PURPOSE
PREMULTIPLY A GENERAL MATRIX BY THE TRANSPOSE OF ANOTHER
GENERAL MATRIX
.....
DIMENSION A(1),B(1),R(1)
IR=0
IK=-N
DO 10 K=1,L
IJ=0
IK=IK+N
DO 10 J=1,M
IB=IK
IR=IR+1
R(IR)=0
DO 10 I=1,N
IJ=IJ+1
IB=IB+1
10 R(IR)=R(IR)+A(IJ)*B(IB)
RETURN
END
SUBROUTINE GHSUB(A,B,P,N,M)
IDENT GHSUB
TITLE GHSUB
ADAPTED FROM S/360 SCIENTIFIC SUBROUTINE PACKAGE.
(36LA-CM-J3X) VERSION III
R. A. GARMOE. 08/16/69.
.....
SUBROUTINE GHSUB
PURPOSE
SUBTRACT ONE GENERAL MATRIX FROM ANOTHER TO FORM RESULTANT
MATRIX
.....
DIMENSION A(1),B(1),R(1)
CALCULATE NUMBER OF ELEMENTS
NM=N*M
SUBTRACT MATRICES
DO 10 I=1,NM

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10 R(I)=A(I)-B(I)
RETURN
END
SUBROUTINE GMADD(A,B,R,N,M)
  IDENT GMADD
  TITLE GMADD
  *** ADAPTED FROM S/360 SCIENTIFIC SUBROUTINE PACKAGE.
  *** (36)A-CH-03X) VERSION III
  *** R. A. GARMOE. 08/16/69.
  .....
  SUBROUTINE GMADD
  PURPOSE
  ADD TWO GENERAL MATRICES TO FORM RESULTANT GENERAL MATRIX
  .....
  DIMENSION A(1),B(1),R(1)
  CALCULATE NUMBER OF ELEMENTS
  NM=N*M
  ADD MATRICES
  DO 10 I=1,NM
10 R(I)=A(I)+B(I)
RETURN
END
SUBROUTINE GMPRO(A,B,R,N,M,L)
  IDENT GMPRO
  TITLE GMPRO
  *** ADAPTED FROM S/360 SCIENTIFIC SUBROUTINE PACKAGE.
  *** (36)A-CH-03X) VERSION III
  *** R. A. GARMOE. 08/16/69.
  .....
  SUBROUTINE GMPRO
  PURPOSE
  MULTIPLY TWO GENERAL MATRICES TO FORM A RESULTANT GENERAL
  MATRIX
  .....
  DIMENSION A(1),B(1),R(1)
  IR=0
  IK=-M
  DO 10 K=1,L
  IK=IK+M
  DO 10 J=1,N
  IR=IR+1
  JI=J-N
  IB=IK
  R(IR)=0
  DO 10 I=1,M
  JI=JI+1
  IB=IB+1
10 R(IR)=R(IR)+A(JI)*B(IB)
RETURN
END

```

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SUBROUTINE SDFLGP
COMMON/DIRCOM/DM1(74),TIMER,DM2(61),AMASS,DM20(27),AX77F,DM21(4),
*AZ77F,DM22(114),DCL1,DCM1,
*DCN1,DCL2,DCMC,DCNC,DCL3,DCM3,DCN3,DM3(99),FXD7P,
*DM4(3),FYH7P,DM23(3),FZD7P,DM5(17),GXU7F,DM6(8),
*GZB7F,DM24(6),HGC7F,DM25(211),INDSTE,DM12(47),PHIPD,DM26(23),
*PSIPD,
*DM27(156),THTPC,DM28(5),TIME,DM29(12),TMAX,DM8(274),
*PI77R,DM3,PI77R1,DM3(5),QI77R,DM31,QI77R1,DM13(5),
*RI77R,DM33,RI77R1,DM11(49),XG77F,DM33,XG77F1,
*DM34(11),YG77F,DM35,YG77F1,DM36(11),
*ZG77F,DM37,ZG77F1,DM13(53),
CNSTRUI,MASS(5),RX(5),PY(5),RZ(5),THETAD(5),ERDEG,RGR,
CNFIRE(5),KZERO(5),W(5),DELTAM(5),MOMENT(5),
CRF(5),VZ,IFD,PZERO(5),VZERO(5),A(5),P2C(5),V20(5),
CA2(5),IL,SCT(5),CS2(5),C2L(5),MASS2(5),HUS(5),
CCC(5),GE(5),C2C(5),C2E(5),NVGPT,NPP,MB(5),RLT,NDELTA,
CES(5),SB(5),SD21(2),SD22(2),SD23(2),SD24(2),SD25(2)
COMMON/DIRCOM/
CSD11(2),SD12(2),SD13(2),SD14(2),SD15(2),
CS1(2),SS2(2),S21(2),S4(2),S5(2),
CS2D21(2),S2D22(2),S2D23(2),S2D24(2),S2D25(2),
CS2D11(2),S2D12(2),S2D13(2),S2D14(2),S2D15(2),
CS21(2),S22(2),S23(2),S24(2),S25(2),
COMTD11(2),OMTD12(2),OMTD13(2),OMTD14(2),OMTD15(2),
COMT1(2),OMT2(2),OMT3(2),OMT4(2),OMT5(2),
CAI(5),D(5),DELTA1,DELTA2,DELTA3,DELTA4,DELTA5,
DOELT1,DOELT2,DOELT3,DOELT4,DOELT5,ISTAGE,
CPRTHIN,IPL1,ISUP,ISTPL1,ISTPL2,ISTPL3,ISTPL4,ISTPL5,
COM14(154),INDLG,DM15(151),DM16(67),NPTS,OPH17(144),IFLX(20)
COMMON/FLXUP/DM17(319),XD2F(20),XD2T(20),YD2F(20),YD2T(20),
*ZD2F(20),ZD2T(20),XD1F(20),XD1T(20),YD1F(20),YD1T(20),
*ZD1F(20),ZD1T(20),XD,F(20),YD,F(20),ZD,F(20)
REAL MASS,MOMENT,MASS2,HUS,NFIRE,MB
COMMON/LGDE/LA(25),FC2(5),P2(5),PRES(5),C(5),IPPT,LTPT
COMMON/LG/FXP,FYM,FZM,LH,MH,NH
COMMON/LG/A11(5),A13(5),A31(5),A33(5),RRCGX(5),
CRL(3,3),RI(3,3,5),RAX(5),RAY(5),RAZ(5),THP(3),ZZERO(5),
CXR(5),YR(5),EPSLON(5),PA(5),FDELTA(5),
CFTRZ(5),RDX(5),RDY(5),ROZ(5),RDXG(5),RDYG(5),ROZG(5),
CVTX(5),VTY(5),VTZ(5),GZ(5),VGPT(5),FTRX(5),FTRY(5),
CDX(5),CY(5),DZ(5),FT(5),FDX(5),FDY(5),FF(5),AA(5),C2(5),
CSR(5),SF(5),PSKO(5),MUVP(5),MTRX(5),MTRY(5),
CHTRZ(5),MA(5),PG11,RG13,RG31,RG33,IPRT,
CHTX,MTY,MTZ,SFTRX,SFTRY,SFTRZ,FTRA,
CFTRD,FTRC,SMTPX,SMTRY,SMTRZ,
REAL MUVP,MTRX,MTRY,MTRZ,MA,
CHTX,MTY,MTZ,LH,MH,NH
DIMENSION DELTA(5),DOELTA(5),P(5),
CSD2(2,5),SD1(2,5),S(2,5),S2D2(2,5),S2D1(2,5),S2(2,5),
COMETD1(2,5),OMET(2,5)
EQUIVALENCE (P(1),PRES(1))
EQUIVALENCE (DELTA(1),DELTA1),(DOELTA(1),DOELT1)
EQUIVALENCE
C(SD21(1),SD2(1,1)),(SD11(1),SD1(1,1)),(S1(1),S(1,1)),
C(S2D21(1),S2D2(1,1)),(S2D11(1),S2D1(1,1)),(S21(1),S2(1,1)),
C(OMETD1(1),OMETD(1,1)),(OMET1(1),OMET(1,1))
DIMENSION OP16(8),OP17(8),OP18(8),OP19(4),OP20(8),OP21(8),
*DAT2(15),DAT3(6),DAT4(15)
DATA
* (OP16(1),I=1,8)/SHDELTA,1HP,2HF2,2HFT,2HSR,2HSF,2HAA,3HFG2/,
* (OP17(1),I=1,8)/3HSO2,3HSD1,1HS,4HS2D2,4HS2D1,2HS2,
* 6HOMETD1,4HOMET/,
* (OP18(1),I=1,8)/4HFTRA,4HFTRB,4HFTRC,3HMTX,3HMTY,
* 3HMTZ,3HFXM,3HFYM/,

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*OP19(I),I=1,4)/3HFZM,2HLM,2HMM,2HNM,
*OP21(I),I=1,8)/4HMOVP,4HVGP,4HFTRX,4HFTRY,4HFTRZ,
*2HMA,2HMH,6HDELTA/,
*OP21(I),I=1,8)/5HDELTA,2HFT,4HMOVP,4HFTRX,4HFTRY,
*4HFTRZ,6HDELTA,1HS/
DATA HRCI/5HGEAR /
DATA DAT1/4HTIME/, (DAT2(I),I=1,15)/2HLM,2HMM,2HNM,5HQI77R,
*5HTHPO,5HPSIP,5HPHPO,3HFZM,5HAZ77F,6HZG77F1,5HAGC7F,
*5HXG77F,5HYG77F,5HAX77F,6HXG77F1/,
*(DAT3(I),I=1,6)/2HFT,2HSP,5HDELTA,1HP,2HP2,2HMA/,
*(DAT4(I),I=1,15)/4HXD2F,4HXD2T,4HYD2F,4HYD2T,4HZD2F,4HZD2T,
*4HXD1F,4HXD1T,4HYD1F,4HYD1T,4HZD1F,4HZD1T,4HXD0F,4HYD0F,4HZD0F/
DATA DAT5/6HLASTPT/, N1/1/, N15/15/, N14/14/
C
SAVE DATA ON TAPE
IF(IPLT.EQ.0)RETURN
LASTPT=0
IF(IPLT.GT.1) GO TO 201
NHL=2
IF(ISDF.NE.C) NHL=NHL+1
ISUM1=ISTPL1+ISTPL2+ISTPL3+ISTPL4+ISTPL5
IF(ISUM1.NE.J) NHL=NHL+1
ISUM2=
DO 105 I=1,NPTS
105 ISUM2=ISUM2+IFLX(I)
IF(ISUM2.NE.J) NHL=NHL+1
WRITE(13)NHL
WRITE(13)N1,N1,DAT1
IF(ISDF.NE.C) WRITE(13)N15,N1,DAT2
IF(ISUM1.NE.J) WRITE(13)N14,ISUM1,DAT3,OP17
IF(ISUM2.NE.J) WRITE(13)N15,ISUM2,DAT4
WRITE(13)N1,N1,DAT5
IPLT=IPLT+1
201 WRITE(13) TIME
IF(ISDF.NE.C) WRITE(13) LM,MM,NM,QI77R,ITHPO,PSIPO,PHIPO,FZM,
*AZ77F,ZG77F1,HGC7F,XG77F,YG77F,AX77F,XG77F1
IF(ISTPL.NE.0) WRITE(13) FT(1),SF(1),DELTA(1),P(1),P2(1),MA(1),
*SD2(1,1),SD1(1,1),S(1,1),S2D2(1,1),S2D1(1,1),S2(1,1),OMETD1(1,1),
*OMET(1,1)
IF(ISTPL.NE.J) WRITE(13) FT(2),SF(2),DELTA(2),P(2),P2(2),MA(2),
*SD2(1,2),SD1(1,2),S(1,2),S2D2(1,2),S2D1(1,2),S2(1,2),OMETD1(1,2),
*OMET(1,2)
IF(ISTPL3.NE.C) WRITE(13) FT(3),SF(3),DELTA(3),P(3),P2(3),MA(3),
*SD2(1,3),SD1(1,3),S(1,3),S2D2(1,3),S2D1(1,3),S2(1,3),OMETD1(1,3),
*OMET(1,3)
IF(ISTPL4.NE.0) WRITE(13) FT(4),SF(4),DELTA(4),P(4),P2(4),MA(4),
*SD2(1,4),SD1(1,4),S(1,4),S2D2(1,4),S2D1(1,4),S2(1,4),OMETD1(1,4),
*OMET(1,4)
IF(ISTPL5.NE.J) WRITE(13) FT(5),SF(5),DELTA(5),P(5),P2(5),MA(5),
*SD2(1,5),SD1(1,5),S(1,5),S2D2(1,5),S2D1(1,5),S2(1,5),OMETD1(1,5),
*OMET(1,5)
DO 17 I=1,NPTS
IF(IFLX(I).NE.J) WRITE(13) XD2F(I),XD2T(I),YD2F(I),YD2T(I),
*ZD2F(I),ZD2T(I),XD1F(I),XD1T(I),YD1F(I),YD1T(I),ZD1F(I),ZD1T(I),
*XD0F(I),YD0F(I),ZD0F(I)
17 CONTINUE
GO TO 24
ENTRY LGEAR6
IF(IPLT.EQ.0)RETURN
IF(LTPT.EQ.0)RETURN
LTPT=
LASTPT=1
BACKSPACE 13
24 WRITE(13)LASTPT
IF(LASTPT.EQ.C)RETURN
END FILE 13
RETURN
G
ENTRY LGEAR6
TIME HISTORY PRINT
IF(INDLG.EQ.1)RETURN
CALL STPL(3,1,HRCI)

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C   IF(INDLG.20.2)GO TO 30
    CALL STFL(2,8,OP16)
    DO 121 I=1,NSTRUT
    CALL STOVAR(8,DELTA(I),P(I),P2(I),FT(I),SR(I),SF(I),AA(I),FC2(I))
121  CONTINUE
    CALL STFL(2,8,OP20)
    DO 123 I=1,NSTRUT
    CALL STOVAR(8,MUVP(I),VGPT(I),FTRX(I),FTRY(I),FTRZ(I),
*MA(I),HB(I),ODELTA(I))
123  CONTINUE
    CALL STFL(2,8,OP17)
    DO 122 I=1,NSTRUT
    CALL STOVAR(8,S02(1,I),SD1(1,I),S(1,I),S202(1,I),
    GS2D1(1,I),S2(1,I),OMETD1(1,I),OMET(1,I))
122  CONTINUE
    GO TO 32
30   CALL STFL(2,8,OP21)
    DO 31 I=1,NSTRUT
    CALL STOVAR(8,DELTA(I),FT(I),MUVP(I),FTRX(I),FTRY(I),
    CFTRZ(I),ODELTA(I),S(1,I))
31   CONTINUE
32   CALL STFL(2,8,OP18)
    CALL STOVAR(8,FTRA,FTRB,FTRC,HTX,HTY,HTZ,
    CFXM,FYM)
    CALL STFL(2,4,OP19)
    CALL STOVAR(4,FZH,LX,MH,NM,DU,CU,DU,DU)
    RETURN
C   *****
C   ENTRY LGEAR5
C   *****
C   COMPUTE AND PRINT CODES
C   RETURN
C   ENTRY LGEAR7
C
    IF(INDLG.20.0)RETURN
    IF(INDLG.20.2)RETURN
    DO 6 I=1,NSTRUT
    IF(IL.NE.3)GO TO 5
    I1=2*I+3*NSTRUT-1
    CALL UPDAT(2,LA(I1),S2D1(1,I),S2(1,I),DU,DU,DU)
5    I1=2*I+NSTRUT-1
    CALL UPDAT(2,LA(I1),SD1(1,I),S(1,I),DU,DU,DU)
6    CALL UPDAT(1,LA(I),OMET(1,I),DU,DU,DU,DU)
    CONTINUE
    RETURN
    END
    OVERLAY(TOLA,1,0)
    PROGRAM TOLAN1
    COMMON/CONTROL/ICONT,CONTR1,ICONT2,ICONT3
    IF(ICONT-2)1,2,3
1    CALL READ
    GO TO 19
2    CALL TFFS2
    GO TO 19
3    IF(ICONT-4)4,5,6
4    CALL SAC32
    GO TO 13
5    CALL VPCTAB
    GO TO 19
6    IF(ICONT-6)7,8,9
7    CALL OPTAB
    GO TO 13
8    CALL LGTAB
    GO TO 19

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19 CALL DSRCH(CONTR1,ICONT2,ICONT3)
   CONTINUE
   END
   SUBROUTINE TFFS2
   COMMON/TABSRC/LOCTFF(2),LOCSAC(79),LOCVPC(18),LOCSD(4),LOCLG(7)
   SETTING UP TABLES FOR TFFS
   CALL TSRCH(6HTTAB1,LOCTFF,2,IER)
   RETURN
   SETTING UP TABLES FOR SACS
   ENTRY SACS2
   CALL TSRCH(6HATAB1,LOCSAC(1),79,IER)
   RETURN
   SETTING UP TABLES FOR VPCS2
   ENTRY VPCTAB
   CALL TSRCH(6HVTAB1,LOCVPC(1),18,IER)
   RETURN
   SETTING UP TABLES FOR OPT2
   ENTRY OPTTAB
   CALL TSRCH(6HBTAB1,LOCSD(1),4,IER)
   RETURN
   SETTING UP TABLES FOR LGEAR
   ENTRY LGTAB
   CALL TSRCH(6HFTAB1,LOCLG(1),3,IER)
   CALL TSRCH(6HCTAB1,LOCLG(4),4,IER)
   RETURN
   END
   SUBROUTINE READ
   COMMON /READ1/ FI(56),ITABLE, IIO, IDO,
   *IBC,K,IBCRW,INX,SLTSYM,JBC,INXQ
   DIMENSION MSG(58),RA(55),RA1(6)
   EQUIVALENCE (MSG(1),SYM), (MSG(2),OP)
   EQUIVALENCE (MSG(3),RA), (MSG(58),INC)
   REAL F(2,28),MRG,NOXEQ
   LOGICAL STSWCH, TABSTP
   COMMON /STOPIT/ STSWCH, TABSTP
   DATA BCU,AINT,STCASE,TRA,MRG,NOXEQ,OCT,COMMA/
   * 3HBC,3HINT,6HSTCASE,3HTRA,3HMRG,1HN,3HOCT,1H,/
   DATA BLANK,POINT,EL,1H,1H,,1HE
   DATA TABL2 / 3HTAB /
   FORMAT (11L12.0)
   FORMAT (5X,16,10E12.0)
   FORMAT (11O12)
   FORMAT (A6,1X,A3,1X,55A1,6A1)
   FORMAT (2)HERROR,THE SYMBOL **A6,26H** IS NOT IN THE DIRECTORY/
   1H)
   FORMAT (22A6)
   FORMAT (16)
   FORMAT (40H ERROR,AN STCASE MRG CARD HAS BEEN ENCOUNTERED,
   * 42H FOR WHICH NO BASE CASE IS AVAILABLE,ERROR)
   FORMAT (52H ERROR,INPUT DECK NOT STARTED WITH STCASE CARD,ERROR)
   9 FORMAT (18X,A6,1X,A3,1X,55A1,16)
   10 FORMAT (25H ERROR,COLUMN 12 IS BLANK/1H)
   11 FORMAT (27H,NO-EXECUTE OPTION SELECTED)
   12 FORMAT (11I12)
   13 FORMAT (55A1)

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O  FORMAT (I1, 9A6)
    K = 1
    DO 16 I=1,2
    DO 16 J=1,28
16  FU(I,J)=J.
100 READ(5,4) SYM,OP,RA,RA1
    IF (EOF,5) 18,19
18  REWIND 13
    STOP 22
19  CALL DIPLAC(RA1,INC,BLANK)
C
20  IF (SYM .NE. STCASE) GO TO 150
21  STSWCH = .FALSE.
    CALL DEF
101  IF (OP .NE. MRG ) GO TO 115
    IF (JBC .LT. 0) GO TO 735
    IF (IBC .EQ. 0) GO TO 110
C TERMINATE BASE CASE AUXILIARY FILE
    IID = -1
    WRITE (16) IID,IID,FI,SYM,OP,RA,INC,ITABLE
    ENDFILE 16
110  IBC = 0
    REWIND 16
    IBCRW = J
    K = 1
    GO TO 120
115  IBC = 1
    INX = 1
    JBC = 1
    K = 1
    IF (OP .NE. TABLED) GO TO 120
    CALL TABR
    IF (TABSTD) GO TO 306
120  INX = 1
    IF ( RA(1) .NE. NOXEQ) GO TO 124
    INX = 0
    CALL LINES (2)
    WRITE (6,12)
124  IF ( IBC .EQ. 0) GO TO 130
    REWIND 16
    IBCRW = 1
    GO TO 130
130  IF (INX .EQ. 0) GO TO 811
    IF (IBC .EQ. 0) CALL READA (IBCRW)
    GO TO 130
150  IF (JBC .NE. 1) GO TO 735
    IF (STSWCH) GO TO 306
    IF (K .EQ. 0) GO TO 170
152  IF (OP .NE. TRA) GO TO 204
    CALL LINES (1)
    WRITE (6,13) SYM,OP
    IF (IBC .EQ. 0) GO TO 160
    IID = -1
    WRITE (16) IID,IID,FI,SYM,OP,RA,INC,ITABLE
160  IF (INX .EQ. 0) GO TO 100
    IF (INX .EQ. 1) GO TO 100
    SLTSYM = SYM
    RETURN
170  IF (IBC .NE. 0) GO TO 152
175  CALL READA (IBCRW)
    K = 1
    GO TO 152
200  IF (K .NE. 0) GO TO 300
    IF (INX .EQ. 0) GO TO 295
179  IF (IBC .EQ. 0) CALL READA (IBCRW)

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305 K = 1
300 CALL WRCARD (MSG)
301 IF (RA(1) .NE. BLANK) GO TO 302
24 CALL LINES (2)
WRITE (6,11)
GO TO 801
302 IF (SYH .EQ. SLTSYH) GO TO 310
CALL OSERCH (SYH,IDD,ITABLE)
IF (ITABLE .LT. 1) GO TO 310
CALL LINES (3)
WRITE (6,5) SYH
306 IF (IBC.NE. 1) GO TO 307
INX = 0
JBC = -1
307 INX = J
GO TO 801

C
C DECODE CARD SECTION
C
310 IF (OP .NE. BCD) GO TO 430
C
C DATA IS BCD
C
DECODE(1,1001,RA)N
1001 FORMAT(I1)
K1=2
KK=7
DO 1088 I=1,N
ENCODE(1,888,FI(I))(RA(L),L=K1,KK)
K1=K1+5
KK=KK+6
1088 CONTINUE
888 FORMAT(5A1)
CALL STORE(N,INC,INX,L)
IF (IBC .EQ. 0) GO TO 350
WRITE (16) IID,N,FI,SYH,OP,RA,INC ,ITABLE
350 SLTSYH = SYH
GO TO 100

C
C NUMERIC TYPE DATA
C
400 IFI = 1
C OCTAL TYPE
IF (OP .EQ. OCT) IFI=1
C INTEGER TYPE
IF (OP .EQ. AINT) IFI=4
405 IQ=J
LQ=J
JJ=1
410 KU = LQ + 1
415 LQ = LQ+1
IF (LQ .GT. 55) GO TO 418
IF (RA(LQ) .EQ. COMMA) GO TO 420
IF (RA(LQ) .NE. BLANK) GO TO 415
418 IQ=1
420 MU=LQ-1
IF (IFI .NE. 0) GO TO 500
425 JJ=KU-1
430 JJ=JQ+1
IF (RA(JQ) .EQ. POINT) GO TO 435
IF (RA(JQ) .NE. EE ) GO TO 440
435 IFI = 2
GO TO 500
440 IF (JQ .LT. MQ) GO TO 430
IFI = 3

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03 CALL PACKRR(RA(KQ),EQ(1,JJ),NQ-KQ+1)
   IF(IQ.NE.0)GO TO 525
520 JJ=JJ+1
   GO TO 410
525 CALL RTE(IFI,FU,FI,JJ)
600 CALL STORE(JJ,INC,INX,0)
   IF (IBC.NE.0) WRITE (16) IID,JJ,FI,SYH,OP,RA,INC,ITABLE
   GO TO 355
700 CALL LINES (1)
   WRITE (5,8)
   GO TO 801
705 CALL LINES (1)
   CALL DEF
   WRITE (6,3)
   SLTSYM = SYH
801 READ (5,4) SYH,OP,RA,INC
802 IF (EOF,5) 25,26
25 REWIND 13
   STOP 25
26 IF (SYH.EQ.STCASE)GO TO 21
   CALL WRCARD (MSG)
   IF (OP .EQ. TRA) GO TO 802
   IF (RA(1) .EQ. BLANK) GO TO 24
   IF (SYH .EQ. SLTSYM) GO TO 802
   CALL DSEARCH (SYH,IID,ITABLE)
   IF (ITABLE.LT.1) GO TO 801
   CALL LINES (1)
   WRITE (6,5) SYH
   GO TO 801
END
SUBROUTINE DIPLAC(RA1,INC,BLANK)
  DIMENSION RA1(6)
  DIMENSION RC(2)
  *****
CPICK UP COLUMN 67 TO 72 AND
RIGHT JUSTIFY FOR USE IN THE INPUT ROUTINE
*****
00 7 I=1,6
  IF (RA1(I) .NE. BLANK) GO TO 2
  DO 1 N=1,6
    N1=7-N
    N2=6-N
    RA1(N1)=RA1(N2)
    RA1(1)=BLANK
    INC=0
1 7
*****
00 00
IF EXIT THROUGH GO STATEMENT 2
THEN A VALID NUMBER EXIST.
GO TO 6
2 CALL PACKRR(RA1,RC,6)
  CALL RTE(5,PC,INC,1)
6 RETURN
END
SUBROUTINE TABRE
COMMON/TABDIR/TABLE(1)
COMMON /STOPIT/ STSCH , TABSTP
COMMON/TABCOH/LOGS(115),STABLE(115)
DIMENSION IS(115),RA1(6)
LOGICAL STSCH , TABSTP
DATA BLANK , BCOTRA / 1H ,3HTRA /

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DATA MAXT, MAXTAB / 115,800/
TABSTP = .FALSE.
DO 2 I=1,MAXT
5  IS(I) = 0
   SYMTRA = BLANK
   NSUM = 0
   NTR = 0
   WRITE (6,3)
3  FORMAT (3X,43HTABLE SIZES FOR EACH TABLE USED IN THIS RUN)
10 READ (5,11) SYM, SYMTRA, RA1
11 FORMAT (A6,1X,A3,1X,A41)
   CALL DIPLAC (RA1,NTSIZE,BLANK)
   CALL LINES (1)
   IF (SYMTRA .EQ. 000000) GO TO 21
   WRITE (6,4) SYM,SYMTRA,NTSIZE
4  FORMAT (18X,A6,1X,A3,1X,I4)
   DO 15 J=1,MAXT
   IF (SYM .NE. STABLE(J)) GO TO 15
   IS(J) = NTSIZE
   NSUM = NSUM + NTSIZE
   NTR = NTR + 1
   GO TO 15
15 CONTINUE
   TABSTP = .TRUE.
   CALL LINES (2)
   WRITE (6,24) SYM
24 FORMAT (14X,36X,A6,29H DOES NOT EXIST IN TABLE LIST)
   GO TO 15
21 CALL LINES (2)
   WRITE (6,4) BLANK,SYMTRA
   NSUM = NSUM + MAXT - NTR
   WRITE (6,22) NSUM
22 FORMAT (3X,39HTOTAL NUMBER OF CELLS FOR ALL TABLES = I4)
   IF (NSUM .LE. MAXTAB) GO TO 200
   TABSTP = .TRUE.
   CALL LINES (2)
   WRITE (6,23) MAXTAB, NSUM
23 FORMAT (14X,1X,25HTOTAL TABLE SIZES EXCEED I4,4H . ,
*36HCHANGE MAXIMUM TOTAL TABLE SIZES TO ,I4/
*25H IN THE MAIN PROGRAM TOLA)
200 KONT = 1
   DO 250 I=1,MAXT
   LOC3(I) = KONT
250 KONT = KONT + IS(I)
   RETURN
END
SUBROUTINE READA (IDCRW)
COMMON/READ1/FI(56),ITABLE,IID,IOD,DM(7)
INTEGER MSG(58)
IF (IDCRW .NE. 0) RETURN
100 READ (16) IID,J,FI,MSG,ITABLE
   IF (IID .GE. 1) GO TO 105
   IDCRW = 1
   RETURN
145 CALL WRDARD (MSG)
   IF (IID .LT. 0) RETURN
   CALL STORC(J,IIDUM1,IIDUM2,1)
   GO TO 100
END
SUBROUTINE STORC (N,INC,INX,STAPE)
INTEGER STAPE
COMMON/READ1/FI(56),ITABLE,IID,IOD,DM(7)
COMMON/DIACOM/DATA(3959)
COMMON/TABLEIR/TABLE(11)
IF (STAPE .NE. 0) GO TO 50

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O      M10R0 = J
      IF (INC.GT.0) M10R0 = -1
      IID = IOD+INC+M10R0
      IF (INX.EQ.0) RETURN
50     J=IID
      IF (ITABLE.LT.0) GO TO 2
      DO 1 I=1,N
      DATA (J) = FI(I)
1      J = J+1
      RETURN
2      DO 3 I=1,N
      TABLE(J) = FI(I)
3      J = J+1
      RETURN
      END
      SUBROUTINE HRCARD(MSG)
      INTEGER MSG(58)
C
      CALL LINES (1)
      J = 58
      IF (MSG(58).LE.0) J = 57
      WRITE (6,1) (MSG(I),I=1,J)
10     FORMAT (18X,A6,1X,A3,1X,55A1,I6)
      RETURN
      END
      SUBROUTINE PACK (I1,I2,N)
      DIMENSION I1(1)
      DATA IBL / 6H
1     FORMAT (6A1)
2     FOPHAT (A6)
      REWIND 31
      IF (N.GE.6) GO TO 3
      K = 6 - N
      WRITE (31,1) (IBL, I = 1,K), (I1(I), I = 1,N)
      GO TO 4
3     WRITE (31,1) (I1(I), I = 1,6)
4     REWIND 31
      READ (31,2) I2
      RETURN
      END
      SUBROUTINE DSERCH (SYH,IOC,IER)
      COMMON/FIXDIP/ANAME(900),LOG(900),NCGUNT
      DO 50 I=1,NCGUNT
      IF (SYH.NE. ANAME(I)) GO TO 50
      IER = 1
      IOC = LOG(I)
      RETURN
50     CONTINUE
      CALL TSERCH (SYH,IOC,1,IER)
      RETURN
C
      END
      SUBROUTINE PACKRR(I1,I2,NNN)
      DIMENSION I1(1)
1000    FORMAT(1H(,I2,2HX,I2,3HA1))
      K=2J=NNN
      ENCODE(10,100,XHAT)K,NNN
      ENCODE(2J,XHAT,I2)(I1(I),I=1,NNN)
      RETURN
      END
      SUBROUTINE RITE(FI,FJ,FI,JJ)
      DIMENSION FI(56),FJ(56)
      GO TO (10J,200,300,400),FI
100     II=1
      DO 1,1 I=1,JJ

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** 6HEPS1 6HEPS16 6HEPS21 6HEPS26 6HEPS31 6HEPS36 6HEPS41 6HEPS46 6HEPS51
** 6HEPS17 6HEPS22 6HEPS27 6HEPS32 6HEPS37 6HEPS42 6HEPS47 6HEPS52 6HEPS57
** 6HEPS18 6HEPS23 6HEPS28 6HEPS33 6HEPS38 6HEPS43 6HEPS48 6HEPS53 6HEPS58
** 6HEPS19 6HEPS24 6HEPS29 6HEPS34 6HEPS39 6HEPS44 6HEPS49 6HEPS54 6HEPS59
** 6HFYB7P 6HFYE7P 6HFZB7P 6HFZE7P 6HGAMOD 6HGAMIF 6HGAMIF1 6HGAMIF2
** 6HGAMIF3 6HGAMIF4 6HGAMIF5 6HGAMIF6 6HGAMIF7 6HGAMIF8 6HGAMIF9 6HGAMIF10
** 6HGYB7F 6HGYE7F 6HGYZ7F 6HGYZ7F 6HGXZ7F 6HGXZ7F 6HGXZ7F 6HGXZ7F
** 6HHA77D 6HHG 6HHG 6HHG 6HHG 6HHG 6HHG 6HHG 6HHG 6HHG 6HHG 6HHG 6HHG 6HHG
** 6HIA83Y 6HIA84Y 6HIA85Y 6HIA86Y 6HIA87Y 6HIA88Y 6HIA89Y 6HIA90Y 6HIA91Y
** 6HIA92Y 6HIA93Y 6HIA94Y 6HIA95Y 6HIA96Y 6HIA97Y 6HIA98Y 6HIA99Y 6HIA100Y
DATA (LOC(1),I=1,126)/
** 23 11 24 25 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000 1001 1002 1003 1004 1005 1006 1007 1008 1009 1010 1011 1012 1013 1014 1015 1016 1017 1018 1019 1020 1021 1022 1023 1024 1025 1026 1027 1028 1029 1030 1031 1032 1033 1034 1035 1036 1037 1038 1039 1040 1041 1042 1043 1044 1045 1046 1047 1048 1049 1050 1051 1052 1053 1054 1055 1056 1057 1058 1059 1060 1061 1062 1063 1064 1065 1066 1067 1068 1069 1070 1071 1072 1073 1074 1075 1076 1077 1078 1079 1080 1081 1082 1083 1084 1085 1086 1087 1088 1089 1090 1091 1092 1093 1094 1095 1096 1097 1098 1099 1100 1101 1102 1103 1104 1105 1106 1107 1108 1109 1110 1111 1112 1113 1114 1115 1116 1117 1118 1119 1120 1121 1122 1123 1124 1125 1126 1127 1128 1129 1130 1131 1132 1133 1134 1135 1136 1137 1138 1139 1140 1141 1142 1143 1144 1145 1146 1147 1148 1149 1150 1151 1152 1153 1154 1155 1156 1157 1158 1159 1160 1161 1162 1163 1164 1165 1166 1167 1168 1169 1170 1171 1172 1173 1174 1175 1176 1177 1178 1179 1180 1181 1182 1183 1184 1185 1186 1187 1188 1189 1190 1191 1192 1193 1194 1195 1196 1197 1198 1199 1200 1201 1202 1203 1204 1205 1206 1207 1208 1209 1210 1211 1212 1213 1214 1215 1216 1217 1218 1219 1220 1221 1222 1223 1224 1225 1226 1227 1228 1229 1230 1231 1232 1233 1234 1235 1236 1237 1238 1239 1240 1241 1242 1243 1244 1245 1246 1247 1248 1249 1250 1251 1252 1253 1254 1255 1256 1257 1258 1259 1260 1261 1262 1263 1264 1265 1266 1267 1268 1269 1270 1271 1272 1273 1274 1275 1276 1277 1278 1279 1280 1281 1282 1283 1284 1285 1286 1287 1288 1289 1290 1291 1292 1293 1294 1295 1296 1297 1298 1299 1300 1301 1302 1303 1304 1305 1306 1307 1308 1309 1310 1311 1312 1313 1314 1315 1316 1317 1318 1319 1320 1321 1322 1323 1324 1325 1326 1327 1328 1329 1330 1331 1332 1333 1334 1335 1336 1337 1338 1339 1340 1341 1342 1343 1344 1345 1346 1347 1348 1349 1350 1351 1352 1353 1354 1355 1356 1357 1358 1359 1360 1361 1362 1363 1364 1365 1366 1367 1368 1369 1370 1371 1372 1373 1374 1375 1376 1377 1378 1379 1380 1381 1382 1383 1384 1385 1386 1387 1388 1389 1390 1391 1392 1393 1394 1395 1396 1397 1398 1399 1400 1401 1402 1403 1404 1405 1406 1407 1408 1409 1410 1411 1412 1413 1414 1415 1416 1417 1418 1419 1420 1421 1422 1423 1424 1425 1426 1427 1428 1429 1430 1431 1432 1433 1434 1435 1436 1437 1438 1439 1440 1441 1442 1443 1444 1445 1446 1447 1448 1449 1450 1451 1452 1453 1454 1455 1456 1457 1458 1459 1460 1461 1462 1463 1464 1465 1466 1467 1468 1469 1470 1471 1472 1473 1474 1475 1476 1477 1478 1479 1480 1481 1482 1483 1484 1485 1486 1487 1488 1489 1490 1491 1492 1493 1494 1495 1496 1497 1498 1499 1500 1501 1502 1503 1504 1505 1506 1507 1508 1509 1510 1511 1512 1513 1514 1515 1516 1517 1518 1519 1520 1521 1522 1523 1524 1525 1526 1527 1528 1529 1530 1531 1532 1533 1534 1535 1536 1537 1538 1539 1540 1541 1542 1543 1544 1545 1546 1547 1548 1549 1550 1551 1552 1553 1554 1555 1556 1557 1558 1559 1560 1561 1562 1563 1564 1565 1566 1567 1568 1569 1570 1571 1572 1573 1574 1575 1576 1577 1578 1579 1580 1581 1582 1583 1584 1585 1586 1587 1588 1589 1590 1591 1592 1593 1594 1595 1596 1597 1598 1599 1600 1601 1602 1603 1604 1605 1606 1607 1608 1609 1610 1611 1612 1613 1614 1615 1616 1617 1618 1619 1620 1621 1622 1623 1624 1625 1626 1627 1628 1629 1630 1631 1632 1633 1634 1635 1636 1637 1638 1639 1640 1641 1642 1643 1644 1645 1646 1647 1648 1649 1650 1651 1652 1653 1654 1655 1656 1657 1658 1659 1660 1661 1662 1663 1664 1665 1666 1667 1668 1669 1670 1671 1672 1673 1674 1675 1676 1677 1678 1679 1680 1681 1682 1683 1684 1685 1686 1687 1688 1689 1690 1691 1692 1693 1694 1695 1696 1697 1698 1699 1700 1701 1702 1703 1704 1705 1706 1707 1708 1709 1710 1711 1712 1713 1714 1715 1716 1717 1718 1719 1720 1721 1722 1723 1724 1725 1726 1727 1728 1729 1730 1731 1732 1733 1734 1735 1736 1737 1738 1739 1740 1741 1742 1743 1744 1745 1746 1747 1748 1749 1750 1751 1752 1753 1754 1755 1756 1757 1758 1759 1760 1761 1762 1763 1764 1765 1766 1767 1768 1769 1770 1771 1772 1773 1774 1775 1776 1777 1778 1779 1780 1781 1782 1783 1784 1785 1786 1787 1788 1789 1790 1791 1792 1793 1794 1795 1796 1797 1798 1799 1800 1801 1802 1803 1804 1805 1806 1807 1808 1809 1810 1811 1812 1813 1814 1815 1816 1817 1818 1819 1820 1821 1822 1823 1824 1825 1826 1827 1828 1829 1830 1831 1832 1833 1834 1835 1836 1837 1838 1839 1840 1841 1842 1843 1844 1845 1846 1847 1848 1849 1850 1851 1852 1853 1854 1855 1856 1857 1858 1859 1860 1861 1862 1863 1864 1865 1866 1867 1868 1869 1870 1871 1872 1873 1874 1875 1876 1877 1878 1879 1880 1881 1882 1883 1884 1885 1886 1887 1888 1889 1890 1891 1892 1893 1894 1895 1896 1897 1898 1899 1900 1901 1902 1903 1904 1905 1906 1907 1908 1909 1910 1911 1912 1913 1914 1915 1916 1917 1918 1919 1920 1921 1922 1923 1924 1925 1926 1927 1928 1929 1930 1931 1932 1933 1934 1935 1936 1937 1938 1939 1940 1941 1942 1943 1944 1945 1946 1947 1948 1949 1950 1951 1952 1953 1954 1955 1956 1957 1958 1959 1960 1961 1962 1963 1964 1965 1966 1967 1968 1969 1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981 1982 1983 1984 1985 1986 1987 1988 1989 1990 1991 1992 1993 1994 1995 1996 1997 1998 1999 2000 2001 2002 2003 2004 2005 2006 2007 2008 2009 2010 2011 2012 2013 2014 2015 2016 2017 2018 2019 2020 2021 2022 2023 2024 2025 2026 2027 2028 2029 2030 2031 2032 2033 2034 2035 2036 2037 2038 2039 2040 2041 2042 2043 2044 2045 2046 2047 2048 2049 2050 2051 2052 2053 2054 2055 2056 2057 2058 2059 2060 2061 2062 2063 2064 2065 2066 2067 2068 2069 2070 2071 2072 2073 2074 2075 2076 2077 2078 2079 2080 2081 2082 2083 2084 2085 2086 2087 2088 2089 2090 2091 2092 2093 2094 2095 2096 2097 2098 2099 2100 2101 2102 2103 2104 2105 2106 2107 2108 2109 2110 2111 2112 2113 2114 2115 2116 2117 2118 2119 2120 2121 2122 2123 2124 2125 2126 2127 2128 2129 2130 2131 2132 2133 2134 2135 2136 2137 2138 2139 2140 2141 2142 2143 2144 2145 2146 2147 2148 2149 2150 2151 2152 2153 2154 2155 2156 2157 2158 2159 2160 2161 2162 2163 2164 2165 2166 2167 2168 2169 2170 2171 2172 2173 2174 2175 2176 2177 2178 2179 2180 2181 2182 2183 2184 2185 2186 2187 2188 2189 2190 2191 2192 2193 2194 2195 2196 2197 2198 2199 2200 2201 2202 2203 2204 2205 2206 2207 2208 2209 2210 2211 2212 2213 2214 2215 2216 2217 2218 2219 2220 2221 2222 2223 2224 2225 2226 2227 2228 2229 2230 2231 2232 2233 2234 2235 2236 2237 2238 2239 2240 2241 2242 2243 2244 2245 2246 2247 2248 2249 2250 2251 2252 2253 2254 2255 2256 2257 2258 2259 2260 2261 2262 2263 2264 2265 2266 2267 2268 2269 2270 2271 2272 2273 2274 2275 2276 2277 2278 2279 2280 2281 2282 2283 2284 2285 2286 2287 2288 2289 2290 2291 2292 2293 2294 2295 2296 2297 2298 2299 2300 2301 2302 2303 2304 2305 2306 2307 2308 2309 2310 2311 2312 2313 2314 2315 2316 2317 2318 2319 2320 2321 2322 2323 2324 2325 2326 2327 2328 2329 2330 2331 2332 2333 2334 2335 2336 2337 2338 2339 2340 2341 2342 2343 2344 2345 2346 2347 2348 2349 2350 2351 2352 2353 2354 2355 2356 2357 2358 2359 2360 2361 2362 2363 2364 2365 2366 2367 2368 2369 2370 2371 2372 2373 2374 2375 2376 2377 2378 2379 2380 2381 2382 2383 2384 2385 2386 2387 2388 2389 2390 2391 2392 2393 2394 2395 2396 2397 2398 2399 2400 2401 2402 2403 2404 2405 2406 2407 2408 2409 2410 2411 2412 2413 2414 2415 2416 2417 2418 2419 2420 2421 2422 2423 2424 2425 2426 2427 2428 2429 2430 2431 2432 2433 2434 2435 2436 2437 2438 2439 2440 2441 2442 2443 2444 2445 2446 2447 2448 2449 2450 2451 2452 2453 2454 2455 2456 2457 2458 2459 2460 2461 2462 2463 2464 2465 2466 2467 2468 2469 2470 2471 2472 2473 2474 2475 2476 2477 2478 2479 2480 2481 2482 2483 2484 2485 2486 2487 2488 2489 2490 2491 2492 2493 2494 2495 2496 2497 2498 2499 2500 2501 2502 2503 2504 2505 2506 2507 2508 2509 2510 2511 2512 2513 2514 2515 2516 2517 2518 2519 2520 2521 2522 2523 2524 2525 2526 2527 2528 2529 2530 2531 2532 2533 2534 2535 2536 2537 2538 2539 2540 2541 2542 2543 2544 2545 2546 2547 2548 2549 2550 2551 2552 2553 2554 2555 2556 2557 2558 2559 2560 2561 2562 2563 2564 2565 2566 2567 2568 2569 2570 2571 2572 2573 2574 2575 2576 2577 25
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END
BLOCK DATA DIR2DA
COMMON/FIXDIR/NAME(9),LOC(9),NCOUNT

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DATA NCOUNT/894/

DATA (NAME (M), M=565, 6371/

```
* 6HRH0A5, 6HRH0SP, 6HRI77R, 6HRI77R1, 6HRM77R, 6HRNCR, 6HRNGMN,
* 6HRNKHG, 6HRNKHL, 6HRNFHG, 6HRNRHL, 6HRNTP, 6HRNTR, 6HPNTY,
* 6HRNYHL, 6HRNYHL, 6HRPHLF, 6HRPLZF, 6HRP77F, 6HR777F, 6HSGDCB,
* 6HSIDLP, 6HSIGDD, 6HSIGN, 6HSIGZD, 6HSIG7D, 6HSIG7R1, 6HSTEST,
* 6HSTESTD, 6HTA1, 6HTA2, 6HTA3, 6HTA4, 6HTA5, 6HTA6,
* 6HTA7, 6HTA10, 6HTA11, 6HTA14, 6HTA77R, 6HTE77P, 6HTHLZD,
* 6HTHL7D, 6HTHTD, 6HTHTPJ, 6HTHTRD, 6HTHTTD, 6HTIME, 6HTIMLS,
* 6HTIME1, 6HTIME3, 6HTIME4, 6HTIMSX, 6HTIUPH, 6HTMAX, 6HTR77R,
* 6HTSTGR, 6HTSTGR1, 6HTS77R, 6HTS77R1, 6HTVACP, 6HTXA7P, 6HTX87P,
* 6HTXE7P, 6HTYA7P, 6HTYD7P, 6HTYE7P, 6HTZA7P, 6HTZ87P, 6HTZE7P,
* 6HT1, 6HUM77F, 6HUPSI, 6HUPSI1, 6HUPSI2, 6HUPSI7F, 6HU777F1,
* 6HVA77F, 6HVD77F, 6HVGRUF, 6HVG77F, 6HVI77F, 6HVM77F, 6HVP77F,
* 6HVS77F, 6HVTHEF, 6HV777F, 6HV777F1, 6HWM77F, 6HWTR7P, 6HW777F,
* 6HW777F1, 6HXCGBF, 6HXCGRF, 6HXD77D, 6HXD77N, 6HXC77F, 6HXC77F1,
* 6HXGZ7F, 6HXG77F, 6HXI77F, 6HXN77F, 6HYA77P, 6HYCGBF, 6HYD77D,
* 6HYD77N, 6HYE77F, 6HYGN7F, 6HYGZ7F, 6HYG77F, 6YI77F, 6HYN77F,
* 6HZCGBF, 6HZE77F, 6HZG77F, 6HZGZ7F, 6HZG77F, 6HZI77F, 6HZN77F,
* 6HZZJ1, 6HNUBUG, 6HCDEB, 6HMPASS, 6HNSHAIN, 6HNS2NDY, 6HINTDMP,
* 6HOBTYPE, 6HNSTRUT, 6HMASS, 6HRX, 6HRY, 6HRZ, 6HTHETAD/
```

DATA (LOC (M), M=565, 6371/

```
* 774, 775, 1186, 1188, 779, 782, 1188,
* 783, 784, 785, 785, 787, 788, 789,
* 790, 791, 792, 793, 794, 795, 808,
* 809, 812, 815, 816, 818, 835,
* 839, 842, 851, 852, 853, 854, 855,
* 856, 857, 858, 861, 864, 865, 866,
* 1190, 872, 876, 878, 881, 882, 883,
* 886, 887, 888, 889, 890, 895, 897,
* 898, 899, 1200, 1202, 900, 901, 902,
* 903, 904, 905, 906, 907, 908, 909,
* 910, 922, 927, 928, 929, 1204, 1206,
* 933, 1208, 1212, 1213, 938, 942, 1216,
* 945, 1221, 1224, 1226, 952, 956, 1228,
* 123, 960, 961, 962, 963, 1232, 967,
* 968, 1238, 1242, 973, 981, 983, 984,
* 985, 1246, 993, 992, 1252, 1256, 999,
* 1006, 1260, 1011, 1266, 1270, 1017,
* 1200, 1272, 1314, 1315, 1316, 1317,
* 1318, 1322, 1323, 1328, 1333, 1338, 1343
```

DATA (NAME (N), N=638, 7691/

```
* 6HERDES, 6HGR, 6HNTIRES, 6IPZERO, 6HW, 64DELTAH,
* 6HMMOMENT, 6HMF, 6HVZ, 6HIFD, 6HPZERO, 64VZERO, 6HA,
* 6HP2J, 6HV2L, 6HA2, 6HIL, 6HS2T, 64ES2, 6HC2L,
* 6HMASS2, 6HMUS, 6HCC, 64CE, 6HC2C, 6HC2E, 6HNVGPT,
* 6HNP, 6HMB, 6HRLT, 6HNOELTA, 6HES, 64SB, 6HS021,
* 6HSD22, 6HSD23, 6HSD24, 6HSD25, 6HSD11, 64SD12, 6HSD13,
* 6HSD14, 6HSD15, 6H31, 6HSS2, 6H3, 64S4, 6HS5,
* 6HSD21, 6HSD22, 6HSD23, 6HSD24, 6HSD25, 64SD11, 6HSD212,
* 6HSD213, 6HSD214, 6HSD215, 6HSD21, 6HSD2, 64SD23, 6HS24,
* 6HSD5, 6HOMTD11, 6HOMTD12, 6HOMTD13, 6HOMTD14, 6HOMTD15, 6HOMT1,
* 6HOMT2, 6HOMT3, 6HOMT4, 6HOMT5, 6HAI, 6H0I, 6HDELTA1,
* 6HDELTA2, 6HDELTA3, 6HDELTA4, 6HDELTA5, 6HDELTA1, 6HDELTA2, 6HDELTA3,
* 6HDELTA4, 6HDELTA5, 6HISTAGE, 6HPRIMIN, 6HIPLT, 6HISDF, 6HISTPL1,
* 6HISTPL2, 6HISTPL3, 6HISTPL4, 6HISTPL5, 6HIN, 6HZN, 6HYN,
* 6HN, 6HICS, 6HCDCH, 6HSSH, 6HXCH, 6HYCH, 6HZCH,
* 6HIB, 6HIFO, 6HMF, 6HNF, 6HXRf, 6HHRF, 6HDELTAH,
* 6HKP, 6HTI, 6HNLRI, 6HVS, 6HXS, 6HTS, 6HVATO,
* 6HALPHTO, 6HHS, 6HALPDES, 6HIAP, 6HVD, 64DELVE, 6HEPSGS,
* 6HALPHDS, 6HALPHOL, 6HHC, 6HDELEPS, 6HRFH, 6HPGS, 6HDELSIG/
```

DATA (LOC (N2), N2=638, 7691/

```
* 1348, 1349, 1350, 1355, 1360, 1365, 1392,
* 1370, 1375, 1380, 1381, 1382, 1387, 1423,
* 1397, 1402, 1407, 1412, 1413, 1418
```

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* 1458 ,1433 ,1438 ,1443 ,1448 ,1453 ,1458 ,
* 1459 ,1460 ,1465 ,1466 ,1467 ,1472 ,1477 ,
* 1479 ,1481 ,1483 ,1485 ,1487 ,1489 ,1491 ,
* 1493 ,1495 ,1497 ,1499 ,1501 ,1503 ,1505 ,
* 1507 ,1511 ,1513 ,1515 ,1517 ,1519 ,1521 ,
* 1523 ,1525 ,1527 ,1529 ,1531 ,1533 ,
* 1535 ,1537 ,1539 ,1541 ,1543 ,1545 ,
* 1547 ,1551 ,1553 ,1555 ,1557 ,1559 ,1561 ,
* 1563 ,1565 ,1567 ,1569 ,1571 ,1573 ,
* 1575 ,1577 ,1579 ,1581 ,1583 ,1585 ,
* 1587 ,1589 ,1591 ,1593 ,1595 ,1597 ,
* 1599 ,1601 ,1603 ,1605 ,1607 ,1609 ,
* 1611 ,1613 ,1615 ,1617 ,1619 ,1621 ,
* 1623 ,1625 ,1627 ,1629 ,1631 ,1633 ,
* 1635 ,1637 ,1639 ,
DATA (NAME (N3),N3=77,874)/
* 6HRTY ,6HRTIC ,6HTTD ,6HXTD ,6HHTD ,6HVXTD ,6HVHTD ,
* 6HTR ,6HLO ,6HQA ,6HTL ,6HKE ,6HPM ,
* 6HTSP ,6HTRV ,6HTCH ,6HTBK ,6HTSS ,6HIL ,6HTS ,
* 6HIC ,6HXPF1 ,6HT1 ,6HXF2 ,6HT2 ,6H1 ,6HT1 ,
* 6H2 ,6H2 ,6H2 ,6H2 ,6H2 ,6H2 ,6H2 ,
* 6HTR1 ,6HTR2 ,6HTK1 ,6HTK1 ,6HTK2 ,6HTK2 ,
* 6HDELPH ,6HDELPH ,6HDELAL ,6HPSH ,6HTST ,6HDELQF ,6HDELFD1 ,
* 6HDELLO ,6HDELLO ,6HDELLO ,6HINDLG ,6HIF8 ,6HDELBA ,6HPSR ,
* 6HPSI ,6HPSIA ,6HPSPI ,6HDELRL ,6HOLLRU ,6HREPHI ,6HOPHIA ,
* 6HPSA ,6HDELPL ,6HDELPU ,6ITF ,6HNOF ,6HIR ,6HNR ,
* 6HNL ,6HNTD ,6HK2 ,6HK3 ,6HMOU ,6HDELHS ,6HDELRRD ,6HDELA ,
* 6HDELTAH ,6HCHC01 ,6HMBL ,6HMOU ,6HDELHS ,6HDELRRD ,6HDELA ,
* 6HNE01 ,6HNR ,6HDELQD ,6HMANLOG ,6HDELALP2 ,6HPSH2 ,6HDELQD ,
* 6HDELQD2 ,6HALPOL ,6HAUXICP ,6HPTCHP ,6HYAWAUP ,6HROLLAP ,6HRAKAP ,
* 6HCONTAP ,6HTR0AP ,6HINDICP ,6HRRHGR ,6HHRD1 ,6HXR ,6HXR01 ,
DATA (LOC (N4),N4=77,874)/
* 1640 ,1641 ,1642 ,1643 ,1644 ,1645 ,1646 ,
* 1647 ,1648 ,1649 ,1650 ,1651 ,1652 ,1653 ,
* 1654 ,1655 ,1656 ,1657 ,1658 ,1659 ,1660 ,
* 1661 ,1662 ,1663 ,1664 ,1665 ,1666 ,1667 ,
* 1668 ,1669 ,1670 ,1671 ,1672 ,1673 ,1674 ,
* 1675 ,1676 ,1677 ,1678 ,1679 ,1680 ,1681 ,
* 1682 ,1683 ,1684 ,1685 ,1686 ,1687 ,1688 ,
* 1689 ,1690 ,1691 ,1692 ,1693 ,1694 ,1695 ,
* 1696 ,1697 ,1698 ,1699 ,1700 ,1701 ,1702 ,
* 1703 ,1704 ,1705 ,1706 ,1707 ,1708 ,1709 ,
* 1710 ,1711 ,1712 ,1713 ,1714 ,1715 ,1716 ,
* 1717 ,1718 ,1719 ,1720 ,1721 ,1722 ,1723 ,
* 1724 ,1725 ,1726 ,1727 ,1728 ,1729 ,1730 ,
* 1731 ,1732 ,1733 ,1734 ,1735 ,1736 ,1737 ,
* 1738 ,1739 ,1740 ,1741 ,1742 ,1743 ,1744 ,
* 1745 ,1746 ,1747 ,1748 ,1749 ,1750 ,1751 ,
* 1752 ,1753 ,1754 ,1755 ,1756 ,1757 ,1758 ,
* 1759 ,1760 ,1761 ,1762 ,1763 ,1764 ,1765 ,
* 1766 ,1767 ,1768 ,1769 ,1770 ,1771 ,1772 ,
* 1773 ,1774 ,1775 ,1776 ,1777 ,1778 ,1779 ,
* 1780 ,1781 ,1782 ,1783 ,1784 ,1785 ,1786 ,
* 1787 ,1788 ,1789 ,1790 ,1791 ,1792 ,1793 ,
* 1794 ,1795 ,1796 ,1797 ,1798 ,1799 ,1800 ,
* 1801 ,1802 ,1803 ,1804 ,1805 ,1806 ,1807 ,
* 1808 ,1809 ,1810 ,1811 ,1812 ,1813 ,1814 ,
* 1815 ,1816 ,1817 ,1818 ,1819 ,1820 ,1821 ,
* 1822 ,1823 ,1824 ,1825 ,1826 ,1827 ,1828 ,
* 1829 ,1830 ,1831 ,1832 ,1833 ,1834 ,1835 ,
* 1836 ,1837 ,1838 ,1839 ,1840 ,1841 ,1842 ,
* 1843 ,1844 ,1845 ,1846 ,
DATA NAME (875)/4HCASK/
DATA LOC (875)/1848/
END
BLOCK DATA DIR (0A)
COMMON/FIXDIR/NAME (9),LOC (900),NCOUNT
DATA (NAME (K3),K3=875,894)/
* 6HNOFLX ,6HNRMODE ,6HGMASS1 ,6HGFREQ ,6HSXMOD ,6HSYMOD ,6HSZMOD ,
* 6HSCC ,6HTXMOD ,6HOCMODE ,6HARMODE ,6HNPIS ,6HOUTMOD ,6HROIS ,
* 6HPP ,6HCO ,6HCO1 ,6HCO2 ,6HIFLX ,
DATA (LOC (K4),K4=875,894)/
* 1892 ,1893 ,1894 ,1914 ,1934 ,2034 ,2134 ,
* 2234 ,2239 ,2319 ,2379 ,2499 ,2500 ,3700 ,
* 3760 ,3880 ,3900 ,3320 ,3940 ,
END
OVERLAY (TOLA,2,4)
PROGRAM TOLAN2
COMMON/CONTR/CONTR,CONTR1,CONTR2,CONTR3

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Q IF (ICNTR-2) 1,2,2
CALL AUTS
GO TO 19
CALL AUTSPR
CONTINUE
END
SUBROUTINE AUTS

AUXILIARY COMPUTATIONS

INPUT REQUIRED (FROM DIRCOM)

XG77F, YG77F, ZG77F - LOCAL GEODESIC DISPLACEMENTS
XG77F1, YG77F1, ZG77F1, AL2, AL27S1, AN2, AN277S, AM2, AM27S1
RGR

COMMON/DIRCOM/DH1(73), TRN, DM2(42), ALPHD, DM2(3), ALPHR1, DM3(15),
*AHASS, DM4(25), ARCLFF, DM5(11), DETAD, DM6(3), DETAR1, DM7(147),
*DELPO, DM8, DELQD, DM9, DELQD, DM11(61), FXH7P, DM12(23),
*GREFF, DM13(17), HGC7F, DM14(211), INOSTE, DM15(47), PHIPD,
*DM15(23), PSIPD, DM35(54), RHOAS, DM38(31),
*SGAMA, DM16(75), TIME, DM17(53), VA77F,
*DM18(3), VG77F, DM7(23), XG77F1, DM19(22),
*YG77F1, DM21(18), ZG77F1, DM36(124), AL2, DM65,
*AL27S1, DM32(13), AML, DM69, AM27S1, DM33(9),
*ANE, DM66, AN277S, DM34(43),
*U777F, DM24(33), XG77F, DM63, XG77F, DM61(11),
*YG77F, DM62, YG77F1, DM63(11), ZG77F, DM64, ZG77F1, DM25(53)
COMMON/DIRCOM/NGSTRUT, DM26(26), RGR, NTIRES(5),
*RZ, RO(5), DM27(13), MOMENT(5), DM28(85), MB(5), DM29(82),
*DMT1(2), DMT2(2), DMT3(2), DMT4(2), DMT5(12),
*DELTA1, DELTA2, DELTA3, DELTA4, DELTA5, DM30(14)
COMMON/DIRCOM/
1IN, ZN(5), YN(5), N(5), ICS, COGH, SSH, XCH, YCH, ZCH,
2IJ(5), ITO, HF, NF, XRF, HRF, DELTAH, KP, FI, NLRI, VS, XS, TS,
3VATO, ALPHD, HS, ALPDES, IAP, VO, DELVE, EPSGS, ALPHDS, ALPHDL,
4HCG, DELEPS, RFH, PGS, DELSIG, RFY, PHIC, TTD, XTO, HTD, VXTD,
5VHTD, IIR, LO, CA, FI, TU, KE(5), PM, TSP, TRV, ICH, TBK, ISS,
6ILR, IBS, IC(5), XRF1, II1(5), XRF2, IT2(5), H1, IH1(5),
7H2, IH2(5), HR1, IHR1(5), HR2, IHR2(5), TR1, ITR1(5),
8TR2, ITR2(5), TUK1, IUK1(5), TUK2, IEK2(5), DELUN,
9RFALPH, DELALA, PSH, TST, DELOF, DELF01, DELQTO, DELQL, DELQU, INOLG
COMMON/DIRCOM/
1RFD, DELBA, PSA, RPSI, OPSIA, PSPSI, DELRL, DELRU, RFPHI, OPHIA,
2PSA, DELPL, DELPU, TF(5), NDF(5), IR(5), NB(5), NLR(5), NTO(5), K2,
3K1(5), K4(11), MBO(5), PD, DELTAH, DMED01, DM67(4), MBL(5), MBO(5),
4DELHS, DELRD, DELA, NED1, HR, DELQD, DM68, RFALP2, PSH2,
*DELQC, DELQD2, ALPOL, DM31(9), XR, XRD1, HRD1, DELQ1, DM39(44),
*DM40(2468)

INPUT REQUIRED FROM LGEAR

RG11, RG13, RG31, RG33

COMMON/LGAUTS/RG11, RG13, RG31, RG33, HA(5), VAXLE(5)

OUTPUT GENERATED

XR, YR, ZR - C.G. POSITION RELATIVE TO RUNWAY COORDINATE SYSTEM
XRD1, YRD1, ZRD1 - VELOCITY IN RUNWAY COORDINATE SYSTEM
HR, HRD1 - ALTITUDE AND ALT. RATE IN RUNWAY COORDINATE SYSTEM
PSIPD1 - YAW RATE IN EARTH AXES FOR P-Y-R SEQUENCE
PHIPD1 - ROLL RATE IN EARTH AXES FOR P-Y-R SEQUENCE

COMMON/AUTSC/IR, TC, TOX,

1TUA, TDB, D(5), IRA, IRB, IRC, ICA, ICB,
2KA, KB, KEA, KEB, KT, NA, NNB, NC, ND(5), NBA, NBB, NBC,
3NLRA, NLRB, NLRC, NDA, NDB, NDC, NTOA, NTOB, NTOC

REAL KA, KH, HA, ANH, HC, ND, NHA, NBS, NUC, NLRA,
1NLRB, NLRG, NDA, NDU, NDC, NIOA, NTOH, NTOC,
2H3C, HBL, HAU, MO, NTIMES, MOMENT, MA, LR, N, NCDI,
3NUI, ISS

COMMON/AUTPRC/YR, ZF, YRD1, ZRD1, PSIPD1, PHIPD1,
1VE, VAO, GAMPRL, OR, CLP, COR, LR, UR, HGS, RR, HEA, HE,
2HET, HPA, HPT, PHIDES, TX, TH, XRF01, XRF01, AXR, AHR,
3ALPHA2, ALD01, ALPHET, DELRN, BETAET, DELRDE, OH,
4PHIE, PHILT, DILPOL, DILQ1, DELRD1, DELPD1,
5ND1(5), OMEGTH(5), OMTD1(5), OMEG'E(5), PSTE, PSIET
COMMON/EXE/AUT/ADJIM1, SWT1, TIME1, ALPD01, PNOES(5)
COMMON/AUTSAC/ALPD01, QOESR, CLRR, ALPO, CORR, DELRNN

POSITION AND VELOCITY RELATIVE TO RUNWAY COORDINATE SYSTEM

LOGICAL SWT1, SWT2
DIMENSION DELTA(5), OMET(2, 5)
EQUIVALENCE (DELTA1, DELTA(1)), (OMT1(1), OMET(1, 1))
DATA RADNEG, DEGRAD/57.2957795, .01745329/
IPR=1
GO TO 2
ENTRY AUTSPR
IPR=1
2 DELTS=TIME-TIME1
TIME1=TIME
XR=RG11*(XG77F-RGR)+RG13*ZG77F
YR=YG77F
ZR=RG31*(XG77F-RGR)+RG33*ZG77F
XRD1=RG11*XG77F1+RG13*ZG77F1
YRD1=YG77F1
ZRD1=RG31*XG77F1+RG33*ZG77F1
HR=-ZR
HRD1=-ZRD1

EULER ANGLE DER. FOR PITCH, YAW, ROLL SEQUENCE

PSIPD1=0.
IF((1.-AL2*AL2).LT.0.)GO TO 1
PSIPD1=AL27S1/30*PI*(1.-AL2*AL2)
PHIPD1=(AL2*AM27S1/AM2-AN277S)/(AM2*(1.+(AN2/AM2)**2))
IF(IPR.EQ.1)CALL AUTPR1

LOGIC TO DETERMINE PROBLEM PHASE

INPUT REQUIRED(FROM DIRCOM)
ITO = 1, FOR LANDING
ITO NOT = 1, FOR TAKE OFF
HF FLARE ALTITUDE
NF INDICATOR TO STOP AT END OF GLIDE SLOPE(NF=1)
XRF, HRF - INITIAL VALUES OF DESIRED TOUCHDOWN POINT
IN RUNWAY COORDINATE SYSTEM
DELTAH - ALTITUDE ABOVE HRF FOR HOLD MODE
KP - IMPACT INDICATOR
TI - IMPACT TIME SET, IF KP=0, NO TI NEEDED
NLRI - INDICATOR TO STOP AT IMPACT
=1, STOP AT IMPACT
VS, XS, TS - RUNWAY STOPPING CONDITIONS
VAIO - AIRSPEED FOR TAKEOFF
ALPHIO - ANGLE OF ATTACK FOR TAKEOFF
HS - ALTITUDE ABOVE RUNWAY TO TERMINATE TAKEOFF

INPUT REQUIRED FROM LGEAR(DIRCOM)
DELTA1, DELTA2, DELTA3, DELTA4, DELTA5 - TIRE DEFLECTION FOR EACH GEAR

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0000 INPUT FROM SDF2 (DIRCOM)
0001 TIME, HGC7F, NSTRUT
0002 IF (ITO.N=.) GO TO 2J
0003 IF (HGC7F.GE..HF) GO TO 7C
0004 IF (NF.EQ.1) GO TO 14
0005 IF ((XR.GE.XRF).OR.(HR.LE.(HRF+DELTAH))) GO TO 13
0006 CALL FLARE(ENTRY 1)
0007 CALL FLARE1(IPR)
0008 CALL ENGINE FAILURE LOGIC
0009 CALL ENGL
0010 GO TO PITCH AUTOPILOT
0011 GO TO 9J
0012 IF (KP.EQ.1) GO TO 10
0013 DO 11 I=1,NSTRUT
0014 IF (DELTA(I).GT.0.) GO TO 12
0015 CONTINUE
0016 CALL FLARE(ENTRY 2)
0017 CALL FLARE2(IPR)
0018 CALL ENGINE FAILURE LOGIC
0019 CALL ENGL
0020 GO TO PITCH AUTOPILOT
0021 GO TO 9J
0022 KP=1
0023 TI=TIME
0024 IF (NLRI.EQ.1) GO TO 16
0025 IF ((XROI.LT.VS).OR.(XR.GT.XS).OR.
0026 C((TIME-TI).GT.TS)) GO TO 16
0027 GO TO LANDING ROLL
0028 GO TO 8J
0029 WRITE(6,15)
0030 FORMAT(10X,18HEND OF GLIDE SLOPE)
0031 INDSTE=J
0032 RETURN
0033 WRITE(6,17)
0034 FORMAT(10X,21HAIRCRAFT HAS IMPACTED)
0035 INDSTE=J
0036 RETURN

```

G L I D E S L O P E

```

INPUT REQUIRED FOR GLIDE SLOPE (FROM DIRCOM)
VD - DESIRED INERTIAL VELOCITY DOWN THE GLIDE SLOPE
DELVE - ALLOWED ERROR IN VE
EPSGS - GLIDE SLOPE ELEVATION ANGLE
ALPHOS - LOWER LIMIT ON ALPHA
ALPHDL - UPPER LIMIT ON ALPHA
TTO - DESIRED THRUST (INPUT ONLY IF IAP GREATER OR =3)
HCG - DISTANCE BETWEEN WHEEL BOTTOM SURFACE AT S.C.
DELEPS - ALLOWED ANGULAR ERROR IN GLIDE SLOPE VERTICAL
POSITION FROM ORIGIN
RFH - RATE FEED BACK CONTRIBUTION TO HET
PGS - PHNGOID CONTROL SENSITIVITY
DELSIG - ALLOWED ANGULAR ERROR IN GLIDE SLOPE
HORIZONTAL POSITION FROM ORIGIN
RFY - RATE FEED BACK CONTRIBUTION TO HPT
PHIC - CONSTANT EULER ROLL ANGLE FOR GROSS RANGE CONTROL

```

INPUT FROM SDF2(DIRCOM)
VG77F, RHOAS, AMASS, GREFF, AREFF, XGN7F1, YGN7F1

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IF (ABS (HET), GE, HEA) ALPOES=ALPOES-PGS*HET
IF (ALPOES.L1,ALPHDS)ALPOES=ALPHDS
IF (ALPOES.GT,ALPHDL)ALPOES=ALPHDL
HPA=RR*UELSIG*DEGRAD
HPT=YG77F+KFF*YG77F1
IF (HPT.GT,HPA)GO TO 72
IF (HPT.L1,(-HPA))GO TO 73
PHIDES=J,
GO TO 74
72 PHIDES=-PHIC
GO TO 74
73 PHIDES=PHIC
CALL ENGINE FAILURE LOGIC
74 CALL ENGFL
IF (IPR.EQ,1)CALL AUTPR2
GO TO PITCH AUTOPILOT
GO TO 9J

      TAKE OFF ROLL

      INPUT REQUIRED (FROM DIRCOM)
VATO -AIRSPEED FOR TAKEOFF
ALPHTO-ANGLE OF ATTACK FOR TAKEOFF
HS -ALTITUDE ABOVE RUNWAY TO TERMINATE TAKEOFF

      INPUT FROM SDF2 (DIRCOM)
VA77F

      OUTPUT GENERATED
ALPOES- DESIRED ANGLE OF ATTACK INPUT WHEN IAP GREATER OR =3)
IAP -PROBLEM PHASE INDICATOR

20 IAP=5
IF (VA77F.L1,VATO)GO TO 21
IAP=6
ALPOES=ALPHTO
21 IF (HR.GT,HS)GO TO 22
CALL ENGINE FAILURE LOGIC
CALL ENGFL
C GO TO PITCH AUTOPILOT
QDESK=J,
GO TO 90,
22 WRITE (6,23)HR,HS
23 FORMAT (1H,5X,42HALTITUDE ABOVE RUNWAY TO TERMINATE TAKEOFF/
*5X,5HHR = E15.8,10X,5HHS = E15.8)
INDSTE=U
RETURN

      L A N D I N G R O L L

      INPUT REQUIRED FOR LANDING ROLL (FROM DIRCOM)
TSP - TIME AFTER IMPACT TO STAGE SPOILERS
TRV - TIME AFTER IMPACT TO REVERSE SIGNAL
TCH - TIME AFTER IMPACT TO CHUTE SIGNAL
TBR - TIME AFTER IMPACT TO BRAKE SIGNAL
ISS = 0, SPOILER SIGNAL INITIALIZATION
ILR = 0, REVERSE SIGNAL INITIALIZATION
ICS = 0, CHUTE SIGNAL INITIALIZATION
IBS=0, BRAKE SIGNAL INITIALIZATION

      INPUT FROM SDF2 (DIRCOM)
TIME

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O IF(IAP.EQ.4)GO TO 93
IF(IAP.EQ.5)GO TO 91
ALPD=ALPDES
CALL SACS11
IF(IAP.LT.2)GO TO 97
RFALPH=RFALP2
PSH=PSH2
DELQOE=DELQOC2
97 ALPHAE=ALPHO-ALPDES
IF(DELTS.LE.1.E-6)GO TO 96
ALPDD1=(ALPDES-ADD1M1)/DELTS
96 IF(ABS(ALPDD1).GT.ALPO1)ALPDD1=0.
ADD1M1=ALPDES
ALDD1=ALPO1
ALPHRE=ALPHR1*RAO0EG-ALPDD1
ALPHET=ALPHAE+RFALPH*ALPHRE
DELQOE=DELQN
SIGNN=SIGN(1.,ALPHAE)
IF(ABS(ALPHET).GE.DELALA)DELQOE=DELQN+PSH*ALPHET+SIGNN*DELQOE
GO TO 92
93 IF(TR.LE.TST)GO TO 95
TMP1=0.5*DELQ1*(TR-TST)
IF((DELQ1-DELQF).GE.0.)GO TO 94
DELQOE=DELQ1+TMP1
IF(DELQOE.GE.DELQF)DELQOE=DELQF
GO TO 92
95 DELQ1=DELQOE
GO TO 92
94 DELQOE=DELQ1-TMP1
IF(DELQOE.LE.DELQF)DELQOE=DELQF
GO TO 92
91 DELQOE=DELQTO
92 IF(DELQOE.LE.DELQL)DELQOE=DELQL
IF(DELQOE.GE.DELQU)DELQOE=DELQU
IF(IPR.EQ.0)CALL AUTPRS

```

Y A W A U T O P I L O T

```

INPUT REQUIRED FOR YAW AUTOPILOT(DIRCOM)
RFB -RATE FEED BACK FOR SIDESLIP
DELBA -SIDE SLIP ERROR ALLOWED
PSR -PILOT SENSITIVITY IN SIDE SLIP OVER CONTROL
RFPSI -RATE FEED BACK FOR PSIE
DPSIA -EULER YAW ERROR ALLOWED
PSPSI -PILOT SENSITIVITY IN EULER YAW CONTROL
DELRL -LOWER RUDDER LIMIT ON DELRDE
DELRU -UPPER RUDDER LIMIT ON DELRDE
IAP -PROBLEM PHASE INDICATOR

```

```

INPUT FROM SDF2(DIRCOM)
BETA0,BETA1,PSIP0

```

```

OUTPUT GENERATED BY YAW AUTOPILOT
DELRN -NOMINAL RUDDER TRIM POSITION
BETA0 -SIDE SLIP POSITION ERROR
BETA1 -TOTAL SIDE SLIP ERROR
DELRDE -DESIRED RUDDER POSITION
PSIE -EULER YAW ANGLE POSITION ERROR
PSIET -TOTAL EULER YAW POSITION ERROR

```

```

CALL SACS11
DELRN=DELRN
IF(IAP.GT.2)GO TO 100
BETA0=BETA0
BETA1=BETA0+RFB*BETA1*RAO0EG

```

```

DELROE=DELRN
IF(ABS(BETAET).GE.UELNA)DELROE=DELRN+PSR*BETAET
GO TO 101
100 PSIE=PSIP0
PSIET=PSIE+RFPST*PSIP0*RAO0EG
UELROE=UELRN
IF(ABS(PSIET).GE.DPSIA)DELROE=DELRN+PSPST*PSIET
101 IF(DELROE.LT.UELRL)DELROE=UELRL
IF(DELROE.GT.UELRL)DELROE=UELRL
IF(IPR.EQ.0)CALL AUTPR6

      R O L L   A U T O P I L O T

      INPUT REQUIRED FOR ROLL AUTOPILOT(DIRCOM)
RPHI -ROLL ANGLE RATE FEEDBACK
DPHIA -ROLL ANGLE ERROR ALLOWED
PSA -PILOT SENSITIVITY IN ROLL OVER CONTROL
DELPL -LOWER AILERON LIMIT ON DELPDE
DELPD -UPPER AILERON LIMIT ON DELPDE
IAP -PRUULEH PHASE INDICATOR

      INPUT FROM SOF2(DIRCOM)
PHIP0

      OUTPUT GENERATED BY ROLL AUTOPILOT
PHIE -ROLL ANGLE ERROR
PHIET -TOTAL ROLL ANGLE ERROR
DELPDE-DESIGNED AILERON POSITION

IF(IAP.GT.0)GO TO 102
PHIE=PHIP0-PHICES
PHIET=PHIE+RPHI*PHIP0*RAO0EG
IF(ABS(PHIET).LT.DPHIA)GO TO 102
DELPDE=PSA*PHIET
GO TO 103
102 DELPDE=0
103 IF(DELPDE.LT.DELPL)DELPDE=DELPL
IF(DELPDE.GT.DELPD)DELPDE=DELPD
IF(IPR.EQ.0)CALL AUTPR7

CALL THROTTLE AUTOPILOT
33 CALL THAUTS(IPR)

      B R A K E   A U T O P I L O T

      INPUT REQUIRED (FROM DIRCOM)
HBC(I) - BRAKING CONSTANT FOR STRUT I
PD - PER CENT SKID FOR CONTROLLED BRAKING
DELTAW - PER CENT SPEED ERROR ALLOWED
OMEGTR(I) -ACCELERATION TO OMEGTR(I) DESIRED
HBL(I) - LOWER BRAKING MOMENT ALLOWED FOR STRUT I
HBU(I) - UPPER BRAKING MOMENT ALLOWED FOR STRUT I
HB(I) - BRAKING MOMENT INITIALLY READ IN
NSTRUT - NUMBER OF INDEPENDENT STRUTS(LGEAR MOD)
RZERD(I) - RADIUS OF TIRES ON EACH STRUT(LGEAR MOD)
NTIRES(I) - NUMBER OF TIRES ON EACH STRUT(LGEAR MOD)
MOMENT(I) - MOMENT OF INERTIA OF SINGLE ROTATING
WHEEL ON EACH STRUT(LGEAR MOD)
DELTA(I) - TIRE DEFLECTION FOR EACH GEAR(LGEAR MOD)

      OUTPUT GENERATED
OMEGTR(I) - DESIRED WHEEL SPEED FOR PD FOR STRUT I
OMEGTRD(I) - DESIRED WHEEL SPEED DECELER FOR STRUT I
OMEGTE(I) - WHEEL SPEED ERROR FOR STRUT I

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MB(I) - BRAKING MOMENT FOR STRUT I
      OUTPUT GENERATED FOR LGEAR (IN DIRCOM)
OMET(1,I),

      INPUT REQUIRED-(FROM LGEAR)
MA(I), OMET(1,I), VAXLE(I)

      INPUT REQUIRED SDF2(DIRCOM)
AHASS, FX37P

DO 48 I=1,NSTRUT
IF(INS.NE.1)GO TO 41
IF((IH(1))42,43,44
OMET(1,I)=J.
GO TO 41
42 MB(I)=0.
GO TO 41
43 IF(IB(I).GT.1)GO TO 45
TMP1=-((1.-PO)/(RZERO(I)-DELTA(I)))
OHEGTR(I)=VAXLE(I)*TMP1
OHTRD1(I)=FXB7P*TMP1/AHASS
OHEGE(I)=OMET(1,I)-OHEGTR(I)
TMP1=J.
IF(ABS(OMET(1,I)).LE.1.E-16)GO TO 48
TMP1=ABS(OMET(1,I))/OMET(1,I)
48 IF(ABS(OHEGE(I)).LT.ABS(DELTA*I*OHEGTR(I)))GO TO 46
IF(OHEGE(I).GT.1.)GO TO 47
M3(I)=TMP1*(MA(I)-OMECDI*MOMENT(I)*NTIRES(I))
GO TO 41
45 MB(I)=MBC(I)
GO TO 41
46 MB(I)=TMP1*(MA(I)+OMECDI*MOMENT(I)*NTIRES(I))
GO TO 41
47 MB(I)=TMP1*(MA(I)+OMECDI*MOMENT(I)*NTIRES(I))
41 IF(MB(I).LT.MBL(I))MB(I)=MBL(I)
IF(MB(I).GT.MBU(I))MB(I)=MBU(I)
40 CONTINUE
IF(IPR.EQ.1)CALL AUTPR9

      C O N T R O L   R E S P O N S E

      INPUT REQUIRED(FROM DIRCOM)
DELPD - CONTROL SURFACE DEFLECTION(INPUT AND OUTPUT)
DELQD - CONTROL SURFACE DEFLECTION(INPUT AND OUTPUT)
DELRD - CONTROL SURFACE DEFLECTION(INPUT AND OUTPUT)
DELHS - HORIZONTAL STABILIZER TIME RATE
DELRD - RUDDER TIME RATE
DELA - AILERON TIME RATE
NEO1 - ENGINE TIME RATE
IN - NO. OF ENGINES
DELTS - MAXIMUM INTEGRATION INTERVAL
N(I) - THROTTLE POSITION FOR EACH ENGINE(INPUT AND OUTPUT)

DELDQ1=DELQS
IF(DELDQE.LT.DEHQD)DELDQ1=-DELQS
DELRD1=DELRD
IF(DELRDE.LT.DEHRD)DELRD1=-DELRD
DELPD1=DELA
IF(DELPDE.LT.DELPD)DELPD1=-DELA
DO 50 I=1,IN
IF(ND(I).EQ.0.)GO TO 51
IF(SMT(I))GO TO 52
IF(ND(I))56,58,58
51 IF(PNDES(I))52,59,59

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52 IF (PND=5(I)) 59,52,52
53 N(I)=-N(I)
54 IF (ND(I)-N(I)) 53,54,54
55 ND(I)=-ND(I)
56 GO TO 57
57 ND1(I)=ND(I)
58 GO TO 59
59 N(I)=.
60 ND1(I)=0.
61 CONTINUE
62 SW1=.FALSE.
63 DO 55 I=1,IN
64 PND=5(I)=ND(I)
65 IF (ABS(DELQD1*DELTS).GE.ABS(DELQDE-DELQD)) GO TO 66
66 DELQD=DELQD+DELQD1*DELTS
67 GO TO 61
68 DELQD=DELQDE
69 IF (ABS(DELRO1*DELTS).GE.ABS(DELRODE-DELRO)) GO TO 62
70 DELRO=DELRO+DELRO1*DELTS
71 GO TO 63
72 DELRO=DELRODE
73 IF (ABS(DELPO1*DELTS).GE.ABS(DELPODE-DELPO)) GO TO 64
74 DELPO=DELPO+DELPO1*DELTS
75 GO TO 65
76 DELPO=DELPODE
77 DO 67 I=1,IN
78 IF (ABS(ND1(I)*DELTS).GE.ABS(ND(I)-N(I))) GO TO 66
79 N(I)=N(I)+ND1(I)*DELTS
80 GO TO 67
81 N(I)=ND(I)
82 CONTINUE
83 IF (IPR.EQ.1) CALL AUTPL
84 RETURN
85 END
86 SUBROUTINE FLARE1(IPR)
87 EXTERNAL ASIN

```

FLARE

```

      INPUT REQUIRED(FROM DIRCOM)
XTD - INITIAL SELECTED TOUCHDOWN CONDITIONS
HTD - INITIAL SELECTED TOUCHDOWN CONDITIONS
VXTD - INITIAL SELECTED TOUCHDOWN CONDITIONS
VHTD - INITIAL SELECTED TOUCHDOWN CONDITIONS
IIR - IF=0, INITIALLY SET XRF, HRF, XRFD1, HRFD1 TO XTD,
      HTD, VXTD, VHTD
LD - SUSPECTED LANDING DISTANCE
DA - NUMBER OF INCREMENTS/DEG IN ALPHA SEARCH
TL - LOWER THRUST LIMIT ALLOWED IN FLARE
TU - UPPER THRUST LIMIT ALLOWED IN FLARE
PH - MAX. TAIL DOWN INTERFERENCE ANGLE AT TOUCHDOWN
ALPHDS- LOWER LIMIT ON ALPHA
ALPHOL- UPPER LIMIT ON ALPHA
HR

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      INPUT REQUIRED(FROM LGEAR-DIRCOM)
RLT - RUNWAY LENGTH(USED ALSO IN LGEAR)
ERDEG - RUNWAY ELEVATION ANGLE IN DEG(USED ALSO IN LGEAR)

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      INPUT REQUIRED(FROM SDF2-DIRCOM)
AMASS,DYNPP,AREFF,WTR7P
SGAMA,GAM7D,VG77F

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COMMON/DIRCOM/DM1(136),AMASS,DM2(25),AREFF,
*DM3(191),DYNPP,DM19(58),GAM7D,DM4(391),

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*ZKAA, DM13(13), VG77F, DM18(18), HTR7P, DM5(365)
COMMON/DIRCOM/DM5(26), ERDEG, DM7(116), RLT, DM8(126)
COMMON/DIRCOM/DM9(36), XRF, HRF, DM15(10), ALPDES, IAP, DM16(13),
*ALPHOS, ALPHOL, DM11(7), TTD, XTO, H.D,
*VXTD, VHTD, IIR, LD, DA, TL, TU, DM11(5), PM, DM12(169), HR, DM14(16),
*XR, XRD1, HRD1, DM17(45), DM28(2068)

INPUT REQUIRED(FROM AUTS)
XR, XRD1, HRD1

OUTPUT GENERATED BY FLARE1
XRF - ACTUAL SELECTED TOUCHDOWN CONDITIONS(DIRCOM)
HRF - ACTUAL SELECTED TOUCHDOWN CONDITIONS(DIRCOM)
XRFD1 - ACTUAL SELECTED TOUCHDOWN CONDITIONS
HRFD1 - ACTUAL SELECTED TOUCHDOWN CONDITIONS
TX - TIME TO TOUCHDOWN X CONSTRAINT
TH - TIME TO TOUCHDOWN Y CONSTRAINT
DM - INCREASE OF TOUCHDOWN POINT PAST XTO
RSR - TOUCHDOWN ALTITUDE RATE REQUIRED TO MEET TX=TH CONSTRAINT
AKR - REQUIRED ACCELERATION TO MEET TOUCHDOWN CONDITIONS
AHR - REQUIRED ACCELERATION TO MEET TOUCHDOWN CONDITIONS
GAMPD - AIRSPEED FLIGHT PATH ANGLE RELATIVE TO RUNWAY
TTD - REQUIRED THRUST SATISFY AKR(DIRCOM)
IAP - PROBLEM PHASE INDICATOR (DIRCOM)
ALPDES - DESIRED ANGLE OF ATTACK (DIRCOM)

COMMON/AUTSC/TR, TC, TOX,
1TOA, TOR, TO(5), IRA, IRB, IRC, ICA, ICB,
2KA, KB, KEA, KEB, KT, NA, NNB, NC, NO(5), NRA, NRB, NBC,
3NLA, NLRB, NLRC, NDA, NDB, NDC, NTOA, NTOB, NTOC

COMMON/AUTPRC/YR, ZR, YRD1, ZRD1, PSTPD1, PHIPD1,
1VE, VAD, GAMPD, OR, CLR, COR, LR, DR, HGS, RR, HEA, HE,
2HET, HPA, HPT, PHUES, TX, TH, XRFD1, HRFD1, AKR, AHR,
3ALPHA, ALPHOL, ALPHET, DELRN, BETAET, DELRDE, DH,
4PHIE, PHIE, DELPDE, DELQD1, DELRD1, DELPD1,
5ND1(5), CMGTR(5), DMTRD1(5), OHEGTE(5), PSIE, PSIET

COMMON/AUTSAC/ALPOR1, QDES, GL1, A1, CD1, DELRNN
LOGICAL SWT1
REAL LD, LI
DATA RADDEG, DEGRAD/57.2957795, .01745329/
IAP=2

IF(IIR.EQ.1160 TO 10
IIR=1

XRF=XTO
HRF=HTD

XRFD1=VXTD

HRFD1=VHTD

TMP1=XRF-XR

TMP2=XRD1+XRFD1

TMP3=HRF-HR

TMP4=HRFD1+HRD1

TMP5=TMP3+TMP2/TMP4+XR-XTO

TX=2.*TMP1/TMP2

TH=2.*TMP3/TMP4

IF(TX-TH)11,30,13

DM=TMP5

IF((LD+DM).GT.RLT)GO TO 14

XRF=XTO+DM

TMP1=XRF-XR

GO TO 33

XRF=XTO+RLT-LD

TMP1=XRF-XR

HRFD1=TMP2+TMP3/TMP4-HRD1

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GO TO 30
DM=TMP5
IF(DM.LT.0.)DM=0.
XRF=XTD+DM
TMP1=XRF-XR
TX=2.*TMP1/TMP2
IF(TX.LE.TH)GO TO 30
RSR=2.*TMP3/TX-HRD1
IF(RSR.GT.0.)GO TO 12
HRFD1=RSR
GO TO 30
12 HRFD1=0.
30 XRF01=HRD1*TMP1/TMP3-XRD1
TMP2=XRD1+XRF01
TMP4=HRFD1+HRD1
AXR=(XRF01-XPD1)*TMP2/(2.*TMP1)
AHR=(HRFD1-HPD1)*TMP4/(2.*TMP3)
GAMERR=(GAM7D-ERRDEG)*DEGRAD
TMP1=SIN(GAMERR)
TMP2=COS(GAMERR)
QESR=ALPOR1+(AHR*TMP2-AXR*TMP1)/VG77F
GAMHAD=ASIN(SGAMA)*PADEG
GAMAPD=GAMHAD-ERRDEG
GAMAPR=DEG*AD*GAMAPD
TMP1=SIN(GAMAPR)
TMP2=COS(GAMAPR)
ERRAD=ERR*G*DEGRAD
TMP3=WT*7P*SIN(ERRAD)
TMP4=WT*7P*COS(ERRAD)
TMP5=AMASS*AXR
SWT1=.FALSE.
A1=ALPHD5
5 CALL SACS TO FIND CL1 AND CD1 FOR ALPHA = A1
CALL SACS1
CALL SACS3
L1=CL1*DYNPP*AREFF
D1=CD1*DYNPP*AREFF
TMP6=DEGRAD*(A1+GAMAPD)
TTH=(TMP5+L1*TMP1+D1*TMP2+TMP3)/COS(TMP6)
IF(TTH.LT.TL)TTH=TL
IF(TTH.GT.TU)TTH=TU
IF(SWT1)GO TO 6
TTD=TTH
ALPOES=A1
6 AX=(TTH*COS(TMP6)-L1*TMP1-D1*TMP2-TMP3)/AMASS
AH=(TTH*SIN(TMP6)+L1*TMP2+D1*TMP1-TMP4)/AMASS
TAE=SQRT((AXR-AX)**2+(AHR-AH)**2)
IF(SWT1)GO TO 7
AE=TAE
SWT1=.TRUE.
7 IF(TAE.GT.AE)GO TO 8
AE=TAE
TTD=TTH
ALPOES=A1
8 A1=A1+DA
IF(A1.LE.ALPHD1)GO TO 5
PHIOES=0.
IF(IPR.EQ.0)CALL AUTPR3
RETURN
ENTRY FLARE2
GAMHAD=ASIN(SGAMA)*RADDEG
GAMAPD=GAMHAD-ERRDEG
IAP=3
PHIOES=0.
IF((ALPOES+GAMAPD).GT.PH)ALPOES=PH-GAMAPD

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IE IPR-CC-ICALL AUTP11

RETOPN

END

SUBROUTINE AUTPR1

COMMON/DIRCOM/DM1(16),ALPHD,DM2(3),ALPHR1,DM3(15),
*A4AS,DM4(16),ARLFF,DM5(11),DELTD,DM6(3),DETR1,DM7(147),
*DELTD,DM8,DELTD,DM9,DELTD,DM10,DELTD,DM11(59),EXD7P,DM12(23),
*GREFF,DM13(17),HGC7F,DM14(259),PHIPD,DM15(23),PSIPD,
*DM35(54),RHOA,DM36(31),
*SGAMA,DM16(75),TIME,DM17(51),V77F,
*DM18(3),V77F,DM37(23),XG77F,DM19(22),
*Y677F,DM20(18),ZG77F,DM38(18),AL2(3),
*AL27S1(2),DM32(12),AM2(2),AM27S(2),DM13(18),
*A4C(2),A4277S(2),DM34(42),
*U777F,DM24(33),XG77F(2),XG77F1(2),
*Y677F(2),Y677F1(2),ZG77F(2),ZG77F1(2),DM25(52)
COMMON/DIRCOM/ASTRUT,DM26(26),RGR,NTIPLS(5),
*RZERD(1),DM27(15),MOMLNT(5),DM2(15),MS(5),DM29(82),
*DMT1(2),DMT2(2),DMT3(2),DMT4(2),DMT5(12),
*JELT1,DELTA2,DELTA3,DELTA4,DELTA5,DM30(14)
COMMON/DIRCOM/
111,ZN(5),YN(5),N(5),ICS,CCCH,SSH,XCH,YCH,ZCH,
213(5),ITC,HF,HF,XRF,HMF,DELTAH,KP,TI,NLW1,VS,XS,TS,
3VATO,ALPHD,MS,ALPDS,AP,VO,VE,EPDS,ALPHDS,ALPHD,
4HCG,DELEPS,XFH,PDS,DLSIG,REY,PIIS,TTG,XTD,HTD,VXTD,
5VHTD,IR,LD,DA,TL,TU,K5(5),PH,TJP,IRV,ICH,TBK,ISS,
6ILR,HS,IC(5),XRF1,IT1(5),XRF2,IT2(5),H1,INH(5),
7H2,INH(5),HPI,INH1(5),H2,INH2(5),TR1,ITP1(5),
8TR2,ITP2(5),THK1,THK2(5),THK2,THK2(5),DELQN,
9RFALPH,DLALA,PSH,TST,DELQF,DELQD1,DELQTO,DELQL,DELQU,INDLG
COMMON/DIRCOM/
1RFD,DELQA,PSF,RFPST,SPSTIA,SPSTIA,DELRL,DELRL,DEPHI,DPHIA,
2PSA,DELPL,DELPU,TF(5),NDF(5),IR(5),NR(5),NLR(5),NTO(5),K2,
3K3(5),K4(11),HRC(5),PI,DELTAH,OMECN1(5),MBL(5),HQB(5),
4DELMS,DELPRD,DELA,DED,HR,DELQDL,MANLOG,DM40(5),AUXICP,
5PITCHP,YAWAUP,ROLLAP,BRAKAP,CONTRP,THROAP,INDICP,DM31,
*XR,XRD,HRU1,DM39(45),DM40(2168)
COMMON/AUTSC/TRA,TC,TEX,
1TUA,TOD,TD(5),IRA,IRJ,IRC,ICA,ICB,
2KA,KB,KCA,KCB,KT,NA,NNA,NC,NC(5),NRA,NRH,NBC,
3NLRA,NLRB,NLRC,NDA,NDB,NDC,NTOA,NTOB,NTOC,
COMMON/AUTPRC/YR,ZA,YR01,ZR01,PSIPD1,PHIPD1,
1VE,VAD,GAIPRD,QR,CLR,COR,LK,DR,HGS,RR,HCA,HE,
2HET,HPA,HOT,PHIDES,IX,TH,XRF01,IPF01,AXR,AHR,
3ALPHA,ALP01,ALPHT,DELAN,BCTAET,DELRDE,DM,
4PHIE,PHIE,DELQD,DELQD1,DELRL,DELRL,
5N01(5),OMEGT(5),DMTRU1(5),OMEGE(5),PSIE,PSIE,
INTEGER AUXICP,PITCHP,YAWAUP,ROLLAP,THROAP,BRAKAP,CONTRP
REAL LP,ISS,NO,MU,N01,N
DIMENSION PRT1(8),PRT2(17),PRT3(16),PRT4(3),
CPRT(2),PRT6(5),PRT7(7),PRT8(3),PRT9(6)
DATA TITLE/NAUTS /
DATA
1(PRT1(1),I=1,8)/2HXR,2HYP,2H2P,4HXRD,4HYR01,4HZP01,6HPSIPD1,
26PHIPD1/(PRT2(1),I=1,17)/2HVE,3HVA0,6HGAHMP,2HQR,3HCLR,
36HALPDS,2HLA,2HUR,2HTD,3HGS,2IRR,3HHA,2HHE,3HET,
43HHA,3HPT,6PHIDES/(PRT3(1),I=1,16)/2HTX,2HT4,
53HXTJ,3HHTD,4HVXTD,4VHTD,3HXR,5HXRF01,3HHRF,
63HHRF01,3HXR,3HHR,6HALPDS,2HTD,6PHIDES,2HDM/
7(PRT4(1),I=1,3)/6HALPDS,6PHIDES,3HTD/
8(PRT5(1),I=1,2)/2HTT,2HTT/(PRT6(1),I=1,6)/5HDELQN,
96HALPDS,6HALPDS,6HALPDS,6HALPDS,6HETAD,6HETAD,6HETAD,6HETAD,
A(PRT7(1),I=1,7)/6HDELOR,5HDELOR,6HETAD,6HETAD,6HETAD,
B6HDELOR,6HPSIE,5HPSIE/(PRT8(1),I=1,3)/4HPHIE,5HPHIE,
C6HDELOR/(PRT9(1),I=1,6)/6HDELQD1,6HDELQD1,6HDELQD1,


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00000 05HDELQU,5HDELRD,5HDELDP/
00000 WRITE TITLE AND AUXILIARY COMPUTATIONS OF AUTS
00000 CALL STFL(3,1,TITLE)
00000 IF (AUXICP.EQ.0) RETURN
00000 CALL LINES(2)
00000 WRITE(6,1)
10 00000 FORMAT(5X,22H AUXILIARY COMPUTATIONS)
00000 CALL STFL(2,8,PRT1)
00000 PSPD10=PSIPD1*57.2957795
00000 PHDD10=PHIPD1*57.2957795
00000 CALL STOVAR(8,XR,YR,ZR,XRD1,YRD1,ZRD1,PSPD10,PHDD10)
00000 CALL STFL(3,1,DU)
00000 RETURN

00000 GLIDE SLOPE PRINTOUT
00000 ENTRY AUTPR2
00000 IF (MANLOG.LD.0) RETURN
00000 CALL LINES(1)
00000 WRITE(6,2)
20 00000 FORMAT(5X,12H GLIDE SLOPE)
00000 CALL STFL(2,8,PRT2)
00000 CALL STFL(2,8,PRT2(9))
00000 CALL STFL(2,1,PRT2(17))
00000 CALL STOVAR(8,VE,VAD,GAMPRD,QR,3LR,ALPOES,LR,OR)
00000 CALL STOVAR(8,TTO,HGS,RR,HEA,HE,HET,HPA,HPT)
00000 CALL STFL(1,1,PHIDES)
00000 CALL STFL(3,1,DU)
00000 RETURN

00000 FLARE ENTRY NUMBER 1
00000 ENTRY AUTPP3
00000 IF (MANLOG.LD.0) RETURN
00000 CALL LINES(1)
00000 WRITE(6,3)
30 00000 FORMAT(5X,5H FLARE)
00000 CALL STFL(2,8,PRT3)
00000 CALL STFL(2,8,PRT3(9))
00000 CALL STOVAR(8,TA,TH,XTO,HTD,VXTJ,VHTD,XRF,XRFD1)
00000 CALL STOVAR(8,HRF,HRFD1,AXR,AHR,ALPOES,TTO,PHIDES,DM)
00000 CALL STFL(3,1,DU)
00000 RETURN

00000 FLARE ENTRY NUMBER 2
00000 ENTRY AUTP11
00000 IF (MANLOG.LD.0) RETURN
00000 CALL LINES(1)
00000 WRITE(6,3J)
00000 CALL STFL(2,3,PRT4)
00000 CALL STOVAR(3,ALPOES,PHIDES,TTO,DU,DU,DU,DU,DU)
00000 CALL STFL(3,1,DU)
00000 RETURN

00000 ENTRY FOR PRINTING LANDING ROLL DATA
00000 ENTRY AUTPN4
00000 IF (MANLOG.LD.0) RETURN
00000 CALL LINES(2)
00000 WRITE(6,4J) ISS,ILR,ICS,IBS
40 00000 FORMAT(6X,12H LANDING ROLL/37X,6H ISS = F2.0,10X,6H ILR = I1,
00000 6X,6H ICS = I1,10X,6H IBS = I1)

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CALL STFL(2,2,PRT5)
CALL STVAR(2,T1,T2,DU,DU,DU,DU,DU,DU)
CALL STFL(,1,DU)
RETURN

400 ENTRY FOR PRINTING PITCH AUTOPILOT DATA

ENTRY AUTPM5
IF(PITCHP.EQ.J)RETURN
CALL LINES(1)
WRITE(6,50)
50 FORMAT(58X,15HPITCH AUTOPILOT)
CALL STFL(2,6,PRT6)
ALPHD1=ALPHA1*57.2957795
CALL STVAR(6,DELQN,ALPHA,ALPHD1,ALPD01,ALPHET,DELQDE,
1DU,DU)
CALL STFL(,1,DU)
RETURN

400 ENTRY FOR PRINTING YAW AUTOPILOT DATA

ENTRY AUTPR6
IF(YAWAP.EQ.J)RETURN
CALL LINES(1)
WRITE(6,60)
60 FORMAT(58X,13HYAW AUTOPILOT)
CALL STFL(2,7,PRT7)
BETAD1=BETAR1*57.2957795
CALL STVAR(7,DELRN,BETAD,BETAD1,BETAET,DELRDE,
1PSIE,PSIET,DU)
CALL STFL(,1,DU)
RETURN

400 ENTRY FOR PRINTING ROLL AUTOPILOT

ENTRY AUTPR7
IF(ROLLAP.EQ.J)RETURN
CALL LINES(1)
WRITE(6,70)
70 FORMAT(58X,14HROLL AUTOPILOT)
CALL STFL(2,3,PRT8)
CALL STVAR(3,PHIE,PHIET,DELPDE,DU,DU,DU,DU,DU)
CALL STFL(,1,DU)
RETURN

400 ENTRY FOR PRINTING THROTTLE AUTOPILOT

ENTRY AUTPR8
IF(THROAP.EQ.J)RETURN
CALL LINES(3)
WRITE(6,80)
80 FORMAT(58X,18HTHROTTLE AUTOPILOT)
WRITE(6,81) (NO(I),I=1,IN)
81 FORMAT(21X,9HNO(IN) = E15.8,4(5X,E15.8))
WRITE(6,82) (TD(I),I=1,IN)
82 FORMAT(21X,9HTD(IN) = E15.8,4(5X,E15.8))
RETURN

400 ENTRY FOR PRINTING BRAKE AUTOPILOT

ENTRY AUTPR9
IF(BRAKAP.EQ.J)RETURN
CALL LINES(2)
WRITE(6,90) (MB(I),I=1,NSTRUT)
90 FORMAT(53X,15HBRAKE AUTOPILOT/21X,9HMB(I) = E15.8,

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C4(15.8,E15.8))
IF(LBS.NE.1) RETURN
CALL LINES(3)
WRITE(6,11) (OMEGTR(I), I=1, NSTRT)
91 FORMAT(17X, 13HOMEGATE(I) = E15.8, 4(5X, E15.8))
WRITE(6,12) (OMTR01(I), I=1, NSTRT)
92 FORMAT(15X, 13HOMEGATE01(I) = E15.8, 4(5X, E15.8))
WRITE(6,93) (OMEGTE(I), I=1, NSTRT)
93 FOPHAT(17X, 13HOMEGATE(I) = E15.8, 4(5X, E15.8))
RETURN

CCC
ENTRY FOR PRINTING CONTROL RESPONSE DATA

ENTRY AUTPL
IF(CONTRP.EQ.0) GO TO 12
CALL LINES(1)
WRITE(6,100)
100 FORMAT(28X, 13HCONTROL RESPONSE)
CALL STFL(2, 6, PRT9)
CALL STOVAR(6, CELQD1, DELR01, DELP01, DELQD, DELRD,
1DELPO, DU, DU)
CALL STFL(1, 1, DU)
CALL LINES(2)
WRITE(6,101) (NO1(I), I=1, IN)
101 FORMAT(24X, 6HNO1 = E15.8, 4(5X, E15.8))
WRITE(6,102) (IN(I), I=1, IN)
102 FORMAT(24X, 6HIN = E15.8, 4(5X, E15.8))

CCC
WRITING OF INDICATORS
12 IF(INDICP.EQ.C) RETURN
CALL LINES(2)
WRITE(6,11) IAP, (IC(I), I=1, 4), (IC(J), J=1, 5)
11 FORMAT(61X, 10HINDICATORS/34X, 5HIAP = I2, 10X,
C7HIC(I) = I2, 1H,, I2, 1H,, I2, 1H,, I2, 1H,, I2, 1JX,
C7HIB(I) = I2, 1H,, I2, 1H,, I2, 1H,, I2, 1H,, I2)
RETURN
END
SUBROUTINE THAUTS(IPR)

THROTTLE AUTOPILOT

INPUT REQUIRED (FROM DIRCOM)
TF(I) - FIX ARRAY FOR ENGINE I
NUF(I) - THROTTLE SETTING FOR TF(I)
IR(I) - REVERSE CAPABILITY ARRAY FOR ENGINE I
NR(I) - THROTTLE CONSTRAINT ARRAY FOR REVERSE FOR ENG. I
NLR(I) - REVERSE THROTTLE SETTING FOR REVERSE SIGNAL ON LANDING
NTO(I) - TAKE OFF THROTTLE SETTING FOR ENGINE I
KE(I) - KILL ENGINE OPTION FOR ENG. I FOR HOLD MODE
THE FOLLOWING ARE ENGINE LOAD CONSTANTS FOR VARIABLE
ENGINE COMBINATIONS
K2 - K(2)121
K3(I) - K(3)131, K(3)232, K(3)121, K(3)1231, K(3)1232
K4(I) - K(4)141, K(4)232, K(4)343, K(4)242, K(4)2342,
K(4)2343, K(4)1341, K(4)1343, K(4)12341,
K(4)12342, K(4)12343
IN - NUMBER OF ENGINES
ILR - REVERSE SIGNAL INITIALIZATION
IAP - PROBLEM PHASE INDICATOR
ITD - DESIRED THRUST

N(I) INPUT FROM SDF2(DIRCOM)

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COMMON/DI3COM/DH1(1585),IN,DM2(11),N(5),DM3(27),IAP,DM8(12),TTO,
*DM4( 9),KE(5),DM5(6),ILA,DM9,IC(5),DM6(84),
*TF(5),NDF(5),IR(5),NB(5),
*NLRC(5),NTO(5),K2,K3(5),K4(11),DM7(91),DDH8(2068)

      INPUT FROM AUTS
      TD(1),TDA,TDB,IC(1),NDA,NDB,NDC

      OUTPUT GENERATED FOR AUTS
      TO(1),TC,TDX,IRA,IRB,IRC,NA,NC,ND(1),NBA,NBB,NBC,
      NLRA,NLRB,NLRC,NTOA,NTOB,NTOC,KA,KB,KT,KEA,
      KEB,ICA,ICB,NNB

COMMON/AUTSC/TR,TC,TDX,
1TDA,TDB,TJ(5),IRA,IRB,IRC,ICA,ICB,
2KA,KB,KEA,KEB,KT,NA,NNB,NC,ND(5),NBA,NBB,NBC,
3NLRA,NLRB,NLRC,NDA,NDB,NDC,NTOA,NTOB,NTOC

      REAL NDF,NB,N,NNB,NLR,NTO,K2,K3,K4,KA,KB,
1NA,NC,ND,NBA,NBB,NBC,NLRA,NLRB,NLRC,
2NTOA,NTOB,NTOC,NDA,NDB,NDC

COMMON/AUTPRC/YR,ZR,YRD1,ZRD1,PSIPD1,PHIPD1,
1VE,VAD,GAMPPD,QR,CLR,CDR,LR,DR,HGS,RR,HEA,HE,
2HET,HPT,HPT,PHIDES,IX,TH,XRFD1,PRFD1,AXR,AHR,
3ALPHA,ALPD1,ALPHET,DELRN,BETAET,DELROE,DM,
4PHIE,PHIT,DELPDE,DELD01,DELR01,DELPD1,
5NJ1(5),OMEGIR(5),OMTRD1(5),OMEGTE(5),PSIE,PSIET

      INTEGER TF
      CHECK ENGINE NO.
      DO 1 I=1,IN
      ND(I)=0.
      TD(I)=0.
      IF(IN-2)10,20,5
      IF(IN-4)30,40,40

      SINGLE ENGINE LOGIC

10      IF(TF(1).EQ.1)GO TO 11
      IF(IC(1).EQ.0)GO TO 12
      SET UP DATA FOR COMMON ENGINE LOGIC
      TD(1)=TTO
      IRC=IR(1)
      NC=N(1)
      NDC=NB(1)
      NLRC=NLRC(1)
      NTOC=NTO(1)
      TC=TD(1)
      KT=KE(1)
      CALL COMMON ENGINE LOGIC
      CALL CENGL
      ND(1)=NOC
      GO TO 20
11      ND(1)=NDF(1)
      IF(ILR.EQ.1)ND(1)=ENGREV(IR(1),N(1),NB(1),NLR(1))
      IF(IC(1).NE.0)GO TO 200
      ND(1)=0.
      GO TO 200
12      TWO ENGINE LOGIC
20      IF((TF(1).EQ.1).OR.(TF(2).EQ.1))GO TO 21
      TDX=TTO
      ICA=IC(1)

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O IRA=IR(1)
  NA=N(1)
  NBA=NB(1)
  NLRA=NLR(1)
  NTOA=NT0(1)
  KEA=KE(1)
  KA=K2
  ICB=IC(2)
  IRB=IR(2)
  NNB=N(1)
  NBA=NB(2)
  NLRB=NLR(2)
  NTOB=NT0(2)
  KEB=KE(2)
  KB=1.-K2
C CALL COMMON TWO ENGINE LOGIC
  CALL GTENGL
  TJ(1)=TDA
  TJ(2)=TDB
  NJ(1)=NDA
  NJ(2)=NDB
21 GO TO 23J
  ND(1)=NOF(1)
  ND(2)=NOF(2)
  IF(ILR.EQ.1)ND(1)=ENGREV(IR(1),N(1),NB(1),NLR(1))
  IF(ILR.EQ.1)ND(2)=ENGREV(IR(2),N(2),NB(2),NLR(2))
  IF(IC(1).EQ.0)ND(1)=0.
  IF(IC(2).EQ.0)ND(2)=0.
  GO TO 20J
  THREE ENGINE LOGIC
  NOTE: ONCE AN ENGINE IS STOPPED, IT STAYS FIXED
  EXCEPT TO FAIL
CCCCC
30 DO 31 I=1,3
  IF(TF(I).NE.1)GO TO 22
31 CONTINUE
  DO 23 I=1,3
  NJ(I)=NOF(I)
  IF(ILR.EQ.1)ND(I)=ENGREV(IR(I),N(I),NB(I),NLR(I))
  IF(IC(I).EQ.0)ND(I)=0.
23 CONTINUE
  GO TO 20J
22 IF((TF(1).EQ.1).AND.(TF(3).EQ.1))GO TO 24
  IF(TF(2).NE.1)GO TO 50
  ND(2)=NOF(2)
  IF(ILR.EQ.1)ND(2)=ENGREV(IR(2),N(2),NB(2),NLR(2))
  IF(IC(2).EQ.0)ND(2)=0.
  CALL TFFS3(ND(2),T0(2))
26 TOX=TTD-T0(2)
  I1=1
  I2=3
  I3=0
27 ICA=IC(I1)
  ICB=IC(I2)
  IRA=IR(I1)
  IRB=IR(I2)
  NA=N(I1)
  NBA=N(I2)
  NLRA=NLR(I1)
  NLRB=NLR(I2)
  NTOA=NT0(I1)

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) NTOB=NT0(I2)
  KEA=KE(I1)
  KEB=KE(I2)
  I4=I1+I3
  KA=K3(I4)
  K3=1.-K3(I4)
C  CALL COMMON TWO ENGINE LOGIC
  CALL CTENGL
  TD(I1)=TUA
  TD(I2)=TOB
  ND(I1)=NDA
  ND(I2)=NDB
  GO TO 24
24 ND(1)=NOF(1)
  ND(3)=NOF(3)
  IF(ILR.EQ.1)ND(1)=ENGREV(IR(1),N(1),NB(1),NLR(1))
  IF(ILR.EQ.1)ND(3)=ENGREV(IR(3),N(3),NB(3),NLR(3))
  IF(IC(1).EQ.1)ND(1)=J.
  IF(IC(3).EQ.1)ND(3)=J.
  CALL TFFS9(NC(1),TD(1))
  CALL TFFS9(ND(3),TD(3))
  IF(IC(2).EQ.0)GO TO 51
  TD(2)=TTD-TD(1)-TD(3)
  I1=2
  I3=1
28 IRC=IR(I1)
  NC=N(I1)
  NDC=NB(I1)
  NLRC=NLR(I1)
  NTOC=NT0(I1)
  TC=TD(I1)
  KT=KE(I1)
C  CALL COMMON ENGINE LOGIC
  CALL CTENGL
  ND(I1)=NDC
  GO TO (29,56,57,29),I3
29 GO TO 200
51 ND(2)=J.
  GO TO 24
50 IF(IC(1).EQ.1)GO TO 60
  IF(IC(2).NL.0)GO TO 55
  ND(2)=J.
  CALL TFFS9(ND(2),TD(2))
  GO TO 26
60 ND(1)=J.
  CALL TFFS9(ND(1),TD(1))
  TD(1)=TTD-TD(1)
  I1=2
  I2=3
  I3=0
  GO TO 27
55 IF(IC(3).EQ.1)GO TO 58
  TD(1)=TTD*K3(4)
  I1=1
  I3=2
  GO TO 28
56 TD(2)=TTD*K3(5)
  I1=2
  I3=3
  GO TO 28
57 TD(3)=TTD-TD(1)-TD(2)
  I1=3
  I3=4
  GO TO 28
O  ND(3)=J.

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81 IF (IC(1).NE.0) GO TO 93
   CONTINUE
   GO TO 95
90 DO 82 I=1,3
   IF (IC(I).NE.0) GO TO 91
82 CONTINUE
   GO TO 97
91 IF ((IC(1).NE.0).OR.(IC(2).NE.0)) GO TO 100
   IF (IC(4).NE.0) GO TO 100
   ND(1)=0.
   ND(2)=J.
   ND(4)=0.
   CALL TFFS3(0.,TD(1))
   TD(2)=TD(1)
   TD(4)=TD(1)
   TD(3)=TTO-TD(1)-TD(2)-TD(4)
   I1=3
   I2=1
83 IRC=IR(I1)
   NC=N(I1)
   NRC=NR(I1)
   NLRC=NLR(I1)
   NTOC=NTC(I1)
   IC=TD(I1)
   KT=KE(I1)
   CALL GENGL
   ND(I1)=NRC
84 GO TO (84,101,102,103,111,121,131,141,151,152,161,162),I2
95 GO TO 23J
96 DO 96 I=1,4
   ND(I)=J.
   GO TO 20J
97 DO 98 I=1,3
   ND(I)=0.
98 CALL TFFS3(0.,TD(1))
   TD(2)=TD(1)
   TD(3)=TD(1)
   TD(4)=TTO-TD(1)-TD(2)-TD(3)
   I1=4
   I2=1
   GO TO 83
100 IF ((IC(1).EQ.0).AND.(IC(2).EQ.0)) GO TO 110
   IF ((IC(1).EQ.J).AND.(IC(3).EQ.0)) GO TO 120
   IF ((IC(1).EQ.J).AND.(IC(4).EQ.0)) GO TO 130
   IF ((IC(2).EQ.0).AND.(IC(3).EQ.0)) GO TO 140
   IF (IC(1).EQ.0) GO TO 15J
   IF (IC(2).EQ.0) GO TO 160
   I1=1
   I2=2
   TD(1)=TTO*K4(9)
   GO TO 83
101 TD(2)=TTO*K4(10)
   I1=2
   I2=3
   GO TO 83
102 TD(3)=TTO*K4(11)
   I1=3
   I2=4
   GO TO 83
103 TD(4)=TTO-TD(1)-TD(2)-TD(3)
   I1=4
   I2=1
   GO TO 83
110 ND(1)=0.
   ND(2)=J.

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```

○ CALL TFE39(0.,TD(1))
  TD(2)=TD(1)
  TD(3)=(TTD-TD(1)-TD(2))*K4(3)
  I1=3
  I2=5
  GO TO 83
111 TD(4)=(TTD-TD(1)-TD(2))*(1.-K4(3))
  I1=4
  I2=1
  GO TO 83
120 ND(1)=0.
  ND(3)=0.
  CALL TFE39(0.,TD(1))
  TD(3)=TD(1)
  TD(2)=(TTD-TD(1)-TD(3))*K4(4)
  I1=2
  I2=6
  GO TO 83
121 TD(4)=(TTD-TD(1)-TD(3))*(1.-K4(4))
  I1=4
  I2=1
  GO TO 83
130 ND(1)=0.
  ND(4)=0.
  CALL TFE39(0.,TD(1))
  TD(4)=TD(1)
  TD(2)=(TTD-TD(1)-TD(4))*K4(2)
  I1=2
  I2=7
  GO TO 83
131 TD(3)=(TTD-TD(1)-TD(4))*(1.-K4(2))
  I1=3
  I2=1
  GO TO 83
140 ND(2)=0.
  ND(3)=0.
  CALL TFE39(0.,TD(2))
  TD(3)=TD(2)
  TD(1)=(TTD-TD(2)-TD(3))*K4(1)
  I1=1
  I2=8
  GO TO 83
141 TD(4)=(TTD-TD(2)-TD(3))*(1.-K4(1))
  I1=4
  I2=1
  GO TO 83
150 ND(1)=0.
  CALL TFE39(0.,TD(1))
  TD(2)=(TTD-TD(1))*K4(5)
  I1=2
  I2=9
  GO TO 83
151 TD(3)=(TTD-TD(1))*K4(6)
  I1=3
  I2=10
  GO TO 83
152 TD(4)=(TTD-TD(1))*(1.-K4(5)-K4(6))
  I1=4
  I2=1
  GO TO 83
160 ND(2)=0.
  CALL TFE39(0.,TD(2))
  TD(1)=(TTD-TD(2))*K4(7)
  I1=1
  I2=11
○

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161 GO TO 83
   TD(3)=(TD-TD(2))*K4(8)
   I1=3
   I2=12
   GO TO 83
162 TD(4)=(TD-TD(2))*(1.-K4(7)-K4(8))
   I1=4
   I2=1
   GO TO 83
280 IF (IPR.EQ.1) CALL AUTPR8
   RETURN
END
FUNCTION ENGREV(IRC,NC,NBC,NLRC)
REAL NC,NBC,NLRC
IF (IRC.EQ.1) GO TO 1
ENGREV=1.
RETURN
1 IF (NC.GT.NBC) GO TO 2
ENGREV=NLRC
RETURN
END
SUBROUTINE ENGFL

```

```

      INPUT REQUIRED (FROM DIRCOM)
XRF1 - FIRST RUNWAY POSITION TO STAGE ENGINE FAILURE
IT1(I) - ARRAY ASSOCIATED WITH XRF1
XRF2 - SECOND RUNWAY POSITION TO STAGE ENGINE FAILURE
IT2(I) - ARRAY ASSOCIATED WITH XRF2
H1 - FIRST ALT. TO STAGE ENGINE FAILURE IN GLIDE SLOPE
IH1(I) - ARRAY ASSOCIATED WITH H1
H2 - SECOND ALT. TO STAGE ENGINE FAILURE IN GLIDE SLOPE
IH2(I) - ARRAY ASSOCIATED WITH H2
HR1 - FIRST ALT. TO STAGE ENGINE FAILURE IN FLARE
IHR1(I) - ARRAY ASSOCIATED WITH HR1
HR2 - SECOND ALT. TO STAGE ENGINE FAILURE IN FLARE
IHR2(I) - ARRAY ASSOCIATED WITH HR2
TR1 - FIRST TIME AFTER IMPACT TO STAGE ENGINE FAILURE
ITR1(I) - ARRAY ASSOCIATED WITH TR1
TR2 - SECOND TIME AFTER IMPACT TO STAGE ENGINE FAILURE
ITR2(I) - ARRAY ASSOCIATED WITH TR2
IAP - PROBLEM PHASE INDICATOR

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      INPUT FROM SDF (DIRCOM)
HGC7F

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```

COMMON/DIRCOM/DM1(434),HGC7F,DM2(1193),IAP,DM3(35),
*IC(5),XRF1,IT1(5),XRF2,IT2(5),H1,IH1(5),H2,IH2(5),
*HR1,IHR1(5),HR2,IHR2(5),TR1,ITR1(5),TR2,ITR2(5),DM4(109),HR,
*DM5(16),XR,DM6(47),DM7(2068)

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      INPUT FROM AUTS
XR, TR

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```

      OUTPUT GENERATED
IC(I) - INITIALIZATION OF FAILURE INDICATOR OF ENGINE I

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```

COMMON/AUTSC/TR,IC,TDX,
1TDA,TDB,TD(5),IRA,IRB,IRC,ICA,IUB,
2KA,KB,KLA,KLB,KT,NA,NNB,NC,ND(5),NBA,NBB,NBC,
3NLRA,NLRB,NLRC,NDA,NDB,NDC,NTOA,NTOB,NTOC

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```

ENGINE FAILURE LOGIC
(ONCE AN ENGINE FAILS-MUST REMAIN FAILED)
IF (IAP-211, 2C, 3)
IF (HGC7F.GT.H1) GO TO 11

```

```

12 DO 12 I=1,4
11 IC(I)=IH1(I)
13 IF(HGO7F.GT.H2)RETURN
DO 13 I=1,4
13 IC(I)=IH2(I)
RETURN
20 IF(HR.GT.HR1)GO TO 21
DO 22 I=1,4
22 IC(I)=IH3(I)
21 IF(HR.GT.HR2)RETURN
DO 23 I=1,4
23 IC(I)=IH2(I)
RETURN
30 IF(IAP-4)20,40,50
40 IF(TR.LT.TR1)GO TO 41
DO 42 I=1,4
42 IC(I)=ITR1(I)
41 IF(TR.LT.TR2)RETURN
DO 43 I=1,4
43 IC(I)=ITR2(I)
RETURN
50 IF(XR.LT.XRF1)GO TO 51
DO 52 I=1,4
52 IC(I)=IT1(I)
51 IF(XR.LT.XRF2)RETURN
DO 53 I=1,4
53 IC(I)=IT2(I)
RETURN
END
SUBROUTINE CENGL

COMMON ENGINE LOGIC

      INPUT FROM DIRCOM
      ILR, IAP

COMMON/DIRCOM/DH1(1628),IAP,DH2(133),ILR,DH3(228),DH4(2066)

      INPUT FROM AUTS
      TC, IRC, NC, NBC, KT, NTOC, NLRC

      OUTPUT GENERATED FOR AUTS
      NJC

COMMON/AUTSC/TR,TC,TOX,
1TOA,TOB,TO(5),IRA,IRB,IRC,ICA,ISB,
2KA,KB,KEA,KEB,KT,NA,NNE,NC,ND(5),NDA,NDB,NBC,
3NLCA,NLRC,NLRC,NDA,NDB,NDC,NTOA,NTOB,NTOC

REAL N,NC,NBC,NLRC,NTOC,NDC
IF(ILR.EQ.1)GO TO 10
IF(IAP-3)11,12,13
11 CALL TFFS8(IC,N)
IF(N.GT.1)GO TO 20
IF(IRC.NE.1)GO TO 21
IF(NC.GT.NBC)GO TO 21
20 NDC=N
RETURN
21 NDC=1.
RETURN
12 IF(KT.NE.1)GO TO 11
GO TO 21
13 IF(IAP.LT.5)GO TO 12
NDC=NTOC
RETURN

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1 IF(IRC.NE.1)GO TO 21
  IF(IRC.GT.NBC)GO TO 21
  NDC=NLRC
  RETURN
  END
  SUBROUTINE CTENGL

COMMON TWO ENGINE LOGIC

      INPUT FROM AUTS
      ICA, ICB, IRR, NNB, NUB, NLRB, NTOB, TOB, KEB, NDC, TOX,
      IRA, NA, NBA, NLRA, NTOA, TOA, KEA, KA, KB
      TOR

      OUTPUT GENERATION FOR AUTS
      NDA, NDB, IRC, NC, NDC, NLRC, NTOC, TC, KT, NOB
      TDA, TUB

      COMMON/AUTSC/TR,TC,TOX,
      1 TU, TOB, TO(5), IRA, IRR, IRC, ICA, ICB,
      2 KA, KB, KEA, KEB, KT, NA, NNB, NC, NO(5), NBA, NBB, NBC,
      3 NLRA, NLRB, NLRC, NDA, NDB, NDC, NTOA, NTOB, NTOC

C      REAL KA,KB,NA,NNB,NC,NBA,NBB,NBC,NDA,NDB,NDC,NLRA,
      1 NLRB, NLRC, NTOA, NTOB, NTOC
      IF((ICA.EQ.0).AND.(ICB.EQ.0))GO TO 30
      IF(ICA.EQ.0)GO TO 20
      IF(ICB.EQ.0)GO TO 10
      TDA=KA+TUX
      IRC=IRA
      NC=NA
      NDC=NBA
      NLRC=NLRA
      NTOC=NTOA
      TC=TOA
      KT=KEA
      CALL CTENGL
      NJA=NDC
      5 TDB=KB+TOX
      IRC=IRR
      NC=NNB
      NDC=NBB
      NLRC=NLRB
      NTOC=NTOB
      TC=TOB
      KT=KEB
      CALL CTENGL
      NDB=NDC
      RETURN
      10 NDB=0.
      CALL TFFS9(J.,TOB)
      TDA=TOX-TOB
      IRC=IRA
      NC=NA
      NDC=NBA
      NLRC=NLRA
      NTOC=NTOA
      TC=TOA
      KT=KEA
      CALL CTENGL
      NJA=NDC
      RETURN
      20 NDA=0.
      CALL TFFS9(J.,TDA)
      TDB=TOX-TDA
      GO TO 5

      NDA=0.
      NDB=0.
      RETURN
      END

```

APPENDIX B

DERIVATION OF AERODYNAMIC WEIGHTING FACTORS

AERODYNAMIC WEIGHTING FACTORS

In the TOLA computer program, the aerodynamic effects are treated as concentrated loads in the form of total aerodynamic forces and moments acting at a reference point on the airframe. These quantities are calculated in the aerodynamics subprogram (SACS) and are defined as follows:

- a - axial force (body axis)
- y - side force (body axis)
- n_f - normal force (body axis)
- l - moment about body X axis
- m - moment about body Y axis
- n - moment about body Z axis

To obtain realistic flexible body response to these aerodynamic loads, weighting effects or participation factors, PF(I), for the response of each normal mode are required.

An approach to determine the weighting effect for the Z translational degree of freedom is given below. A similar method can be used to determine the remaining participation factors.

In TOLA, the generalized aerodynamic force is calculated as the product of the total lift, the vertical modal deflection at the reference point, and a participation factor

$$Q_{AZ} = n_f \phi_{Z_R} PF$$

If the actual generalized force due to aerodynamics is obtained by integrating the product of the pressure distribution and modal deflection over the lifting area, the expression for this quantity would be given as

$$Q_{AZ} = \int_A \phi_Z(x,y) P(x,y) dA$$

Equating the two force expressions, an equation for the participation factor can be obtained.

$$PF = \frac{\int_A \phi_Z(x,y) P(x,y) dA}{n_f \phi_{Z_R}}$$

APPENDIX C

PROGRAM LISTING, PLTDAT COMPUTER PROGRAM

```

PROGRAM PLTOAT(INPUT,TAPE3,TAPE1,OUTPUT,TAPE4)
DIMENSION TITLE(15),BUF(400),NOIL(28),TBUF(400),
* AVAL(4,6),
* BHM(2,400),CHMDS(5),DEPVAR(5),LINE(7),NOVA(5)
DATA CHMDS/4HPLOT,6HTITLE1,6HTITLE2,6HINOVAR,6HDEPVAR/
DATA INPUT/SLINPUT/
READ(INPUT,105)NPTS
105 FORMAT(I6)
READ(3) NHL
NH=C
NOL=
NHL=NHL-1
DO 16 N=1,NHL
READ(3) NI,ND,(TITLE(I),I=1,NI)
106 FORMAT(2I6,3A6)
IF (ND.GT.1) GO TO 7
NS=NW+1
NOL=NOL+1
NOIL(NOL)=NI
103 FORMAT(13A16)
ENCODE(13J,100,TBUF(NS))(TITLE(I),I=1,NI)
NH=NW+NI
GO TO 10
7 DO 8 J=1,ND
NS=NW+1
NOL=NOL+1
NOIL(NOL)=NI
IF(J.LE.9)GO TO 111
ENCODE(13J,11,TBUF(NS))(J,TITLE(I),I=1,NI)
111 FORMAT(13(12,A8))
GO TO 112
111 ENCODE(13J,113,TBUF(NS))(J,TITLE(I),I=1,NI)
113 FORMAT(13(+C*,I1,A8))
112 NH=NW+NI
CONTINUE
8 CONTINUE
10 CONTINUE
READ(3) IX
DO 15 I=1,NH
BHM(1,I)=1.E60
15 BHM(2,I)=-1.E60
K=
NDI=
DO 35 N=1,NOL
NIL=NOIL(N)
READ(3) (BUF(I+NDI),I=1,NIL)
IF(EOF,3) 50,35
35 NDI=NDI+NIL
READ(3) ENDPNT
WRITE(4) (BUF(I),I=1,NH)
DO 36 I=1,NH
BHM(1,I)=AMIN1(BHM(1,I),BUF(I))
36 BHM(2,I)=AMAX1(BHM(2,I),BUF(I))
K=K+1
IF(K.GT.NPTS) GO TO 50
GO TO 30
50 DO 51 I=1,15
51 TITLE(I)=10H
NIV=
NOV=
KT1=
KT2=
CALL PLOTS(DUH,DUH,1.)
CALL PLOT(.,1,-3)
60 READ(INPUT,99)CHMO,LINE
99 FORMAT(10A10)

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59 IF (EOF, INPUT) 9., 59
   DO 61 K=1,5
   IF (CHMD, EQ. CHMDS(K)) GO TO (80, 62, 63, 65, 66), K
61 CONTINUE
   PRINT 300, CHMD
300 FORMAT(* IMPROPER COMMAND-*, A10)
   STOP
62 ENCODE(40, 100, TITLE(1)) (LINE(I), I=1, 4)
   KT1=KTB(TITLE(1), 40)
   GO TO 60
63 ENCODE(40, 100, TITLE(5)) (LINE(I), I=1, 4)
   KT2=KTB(TITLE(5), 40)
   GO TO 60
65 CALL FIND(TBUF, NH, LINE(1), NIV)
   IF (NIV, NE. J) GO TO 70
   PRINT 31., LINE(1)
31. FORMAT(* IMPROPER INDEPENDENT VARIABLE-*, A10)
   STOP
70 AVAL(1, 1)=BHM(1, NIV)
   AVAL(2, 1)=BHM(2, NIV)
   GO TO 60
66 NDV=1
   DO 69 N=1, 5
   IF (LINE(N), EQ. 1H ) GO TO 67
   CALL FIND(TBUF, NH, LINE(N), NOVA(N))
   IF (NOVA(N), NE. J) GO TO 68
   PRINT 320, LINE(N)
320 FORMAT(* IMPROPER DEPENDENT VARIABLE *, A10)
   STOP
67 NDV=N+1
   GO TO 60
68 NDX=NOVA(N)
   AVAL(1, N+1)=BHM(1, NDX)
   AVAL(2, N+1)=BHM(2, NDX)
   CALL SCALE(AVAL(1, N+1), 6., 2, 1)
69 CONTINUE
   NDV=5
   GO TO 60
80 IF (NIV, NE. J) GO TO 81
   PRINT 33.
33. FORMAT(* NO INDEPENDENT VARIABLE*)
   STOP
81 IF (NDV, NE. J) GO TO 82
   PRINT 34.
34. FORMAT(* NO DEPENDENT VARIABLES*)
   STOP
82 IF (KT1, NE. J) CALL LABEL(1., 6.5, 10., 6.5, TITLE(1), KT1,
   * 3, 2, 0., 0., 0.)
   IF (KT2, NE. J) CALL LABEL(1., 6.1, 10., 6.1, TITLE(5), KT2,
   * 2, 2, 0., 0., 0.)
   CALL PLOT(NDV, 6+5, 0., -3)
   AXLEN=10.-NDV*.6
   CALL SCALE(AVAL(1, 1), AXLEN, 2, 1)
   CALL AXIS(0., 0., TBUF(NIV), -10, AXLEN, 0., AVAL(3, 1), AVAL(4, 1))
   DO 89 J=1, NDV
   JD=NOVA(J)
   RCHIND 4
   IP=3
83 READ(4) (JUF(I), I=1, NH)
   IF (EOF, 4) 85, 84
84 VARIND=(BUF(NIV)-AVAL(3, J+1))/AVAL(4, 1)
   VARDEP=(BUF(JD)-AVAL(3, J+1))/AVAL(4, J+1)
   IF (IP, EQ. J) CALL SYMBOL(VARIND, VARDEP, 1, J, 0., -1)
   IF (IP, NE. J) CALL PLOT(VARIND, VARDEP, 2)
   IP=2

```

```

85 GO TO 83
   NSUB=NSUBA(J)
   CALL AXIS(-(J-1)*.6,.1,TBUF(NSUB),10,6.,90.,AVAL(3,J+1),
   *AVAL(4,J+1))
   CALL SYMBOL(-(J-1)*.6-.4,1.,.14,J,90.,-1)
89 CONTINUE
   CALL PLOT(AXLEN+1.,0.,-3)
   GO TO 66
93 CALL PLOT(.,0.,999)
   STOP
END
FUNCTION KTB(ISTRG,IST)
  DIMENSION ISTRG(1)
  DO 2, I=1,IST
    KTB=IST+1-I
    NH0=(KTB+3)/13
    NBITS=8*MOD(KTB,16)
    IIST=ISHIFT(ISTRG(NH0),NBITS).AND.778
    IF (IIST.NE.558) RETURN
20 CONTINUE
    KTB=
    RETURN
END
SUBROUTINE FIND(TBUF,NH,COMP,N)
  DIMENSION TBUF(1)
  DO 1, N=1,NH
    IF (TBUF(N).EQ.COMP) RETURN
10 CONTINUE
    N=
    RETURN
END

```

APPENDIX D

AIRPLANE A RIGID BODY EXAMPLE 1

D-2

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0010 STCASE TAB 2
0011 ATAB1 2
0012 ATAB2 2
0013 ATAB1 2
0014 ATAB1 2
0015 ATAB1 2
0016 ATAB1 2
0017 ATAB1 2
0018 ATAB1 2
0019 ATAB1 2
0020 ATAB1 2
0021 ATAB1 2
0022 ATAB1 2
0023 ATAB1 2
0024 ATAB1 2
0025 ATAB1 2
0026 ATAB1 2
0027 ATAB1 2
0028 ATAB1 2
0029 ATAB1 2
0030 ATAB1 2
0031 ATAB1 2
0032 ATAB1 2
0033 ATAB1 2
0034 ATAB1 2
0035 ATAB1 2
0036 ATAB1 2
0037 ATAB1 2
0038 ATAB1 2
0039 ATAB1 2
0040 ATAB1 2
0041 ATAB1 2
0042 ATAB1 2
0043 ATAB1 2
0044 ATAB1 2
0045 ATAB1 2
0046 ATAB1 2
0047 ATAB1 2
0048 TRA 49
0049 STCASE
0050 REM BCD 3SDF2-GEAR-MOD
0051 NCASE BCD 1G-MOD
0052 REM BCD +INTERGRATION INFORMATION
0053 IVARBH .10L
0054 IMAX .00005
0055 AMINER .4
0056 PRIMIN .1
0057 AMAXER .1
0058 DELTS .1
0059 PRINT .4
0060 REM BCD 3REQ*D FOR SDF-2
0061 AMASS 29702.852
0062 HG37F 120.824
0063 THIBU 3.5896
0064 GAM7D -3.
0065 VG77F 22L
0066 KR10K .
0067 INJAPC .
0068 INJADD 1
0069 INJFPA 1
0070 INJPLA 1
0071 INOACH 1
0072 INJGRT 1
0073 INJHGT 1
0074 REM BCD 5VEHICLE PHYSICAL PROP. DATA

```

```

1.75-INJWPC
1.76-XUSXRF
1.77-VTAB1
1.78-VTAB2
1.79-VTAB3
1.80-VTAB4
1.81-INJXZS
1.82-VTAB6
1.83-REM
1.84-INJACR
1.85-ARFFF
1.86-ORFFF
1.87-URFFF
1.88-INJA1
1.89-ATAB1
1.90-INJA2
1.91-ATAB2
1.92-INJA1
1.93-ATAB1
1.94-INJA1
1.95-ATAB1
1.96-INJA2
1.97-ATAB2
1.98-INJA1
1.99-ATAB2
1.10-INJA1
1.11-ATAB1
1.12-INJA2
1.13-ATAB2
1.14-INJA2
1.15-ATAB2
1.16-INJA3
1.17-ATAB3
1.18-INJA4
1.19-ATAB4
1.20-INJA4
1.21-ATAB4
1.22-INJA5
1.23-ATAB5
1.24-INJA5
1.25-ATAB5
1.26-INJA6
1.27-ATAB6
1.28-INJA6
1.29-ATAB6
1.30-INJA7
1.31-ATAB7
1.32-INJA7
1.33-ATAB7
1.34-INJA7
1.35-ATAB7
1.36-INJA8
1.37-ATAB8
1.38-REM
1.39-INDTFF

```

BCU AERODYNAMIC INPUT DATA

BCU ENGINE THRUST DATA

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144. IUTSO	1	
141. IUTSO	1	
142. ITAB1	4	
143. ITAB1	-2.0, -1.5, -1.0, -0.5, 0.0, 0.5, 1.0, 1.5, 2.0	
144. ITAB1	-0.5, 0.0, 0.5, 1.0, 1.5, 2.0	1
145. ITAB1	-1.0, 0.0, -0.5, 0.0, 0.5, 1.0, 1.5, 2.0	14
146. ITAB1	1.0, 0.0, 0.5, 1.0, 1.5, 2.0, 2.5, 3.0	19
147. ITAB1	-2.0, 0.0, -1.0, 0.0, -0.5, 0.0, -0.25, 0.0, -0.125	23
148. ITAB1	0.0, 1.0, 0.0, 1.0, 0.0, 1.0, 0.0, 1.0, 0.0	28
149. ITAB1	-0.5, 0.0, -0.25, 0.0, -0.125, 0.0, -0.0625, 0.0, -0.03125	32
150. ITAB1	-0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0	37
151. ITAB1	-4.0, 0.0, -2.0, 0.0, -1.0, 0.0, -0.5, 0.0, -0.25	41
152. ITAB1	-1.0, 0.0, -0.5, 0.0, -0.25, 0.0, -0.125, 0.0, -0.0625	46
153. RZ	BCJ 3 LANDING GEAR DATA	
154. NSTRUT	5	
155. MASS	46.02149, 132.1942, 132.1942, 132.1942	
156. MASS	132.1942	5
157. RX	02.34333, -1.42, -1.42, -1.42, -1.42, -1.42, -1.42, -1.42, -1.42	
158. RY	0.0, -12.9375, 12.9375, -12.9375, 12.9375, -12.9375, 12.9375, -12.9375, 12.9375	
159. RZ	0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0	
160. THETA	1917.	
161. ERJEG	4.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0	
162. RZ	2.0, 1.0, 0.0, 2.0, 1.0, 0.0, 2.0, 1.0, 0.0	5
163. RZ	2.0, 1.0, 0.0, 2.0, 1.0, 0.0, 2.0, 1.0, 0.0	
164. RZ	2.0, 1.0, 0.0, 2.0, 1.0, 0.0, 2.0, 1.0, 0.0	
165. RZ	2.0, 1.0, 0.0, 2.0, 1.0, 0.0, 2.0, 1.0, 0.0	
166. W	1.41000, 1.41000, 1.41000, 1.41000, 1.41000, 1.41000, 1.41000, 1.41000, 1.41000	
167. DELTAM	0.83333, 0.83333, 0.83333, 0.83333, 0.83333, 0.83333, 0.83333, 0.83333, 0.83333	
168. RLI	1.0	
169. IFD	1.0	
170. AI	125472.2, 141992.9, 141992.9, 141992.9, 141992.9	5
171. AI	141992.9	
172. BI	1.32, 1.293, 1.293, 1.293, 1.293	
173. FTAB0	0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0	
174. FTAB0	0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0	
175. FTAB0	0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0	10
176. FTAB0	0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0	20
177. MOMENT	10.0, 10.0, 10.0, 10.0, 10.0, 10.0, 10.0, 10.0, 10.0	
178. M3	0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0, 0.0	
179. RF	18.13000, 18.55410, 18.55410, 18.55410, 18.55410	5
180. RF	18.55410	
181. VZ	0.0	
182. PZERO	3.470.4, 4.1530.24, 4.1530.24	4
183. PZERO	4.1530.24, 4.1530.24	
184. VZERO	0.573801, 1.162062, 1.162062	4
185. VZERO	1.162062, 1.162062	
186. A	0.452222, 0.722222, 0.722222	4
187. A	0.722222, 0.722222	
188. PZ	0.72040, 0.340194, 0.340194, 0.340194	4
189. PZ	0.340194, 0.340194	
190. VZ	0.0, 0.243, 1.1179398, 1.1179398	4
191. VZ	1.1179398, 1.1179398	
192. A2	0.394444, 0.518.55, 0.518.55	4
193. A2	0.518.55, 0.518.55	
194. IL	0.0	
195. S2I	0.9.025, 0.78+160, 0.78+160	4
196. S2I	0.78+160, 0.78+160	
197. S2	0.0, 0.833, 0.0, 0.833, 0.0, 0.833	4
198. S2	0.0, 0.833, 0.0, 0.833	
199. C2L	0.4, 0.24, 0.24, 0.24, 0.24, 0.24	
200. INDC	1	
201. NSMAIN	2	
202. CTAB0	-1.0, 0.0, 0.0	3
203. CTAB0	1.0, 2.0, 3.0, 4.0, 5.0	8
204. CTAB0	0.24, 0.24, 0.24, 0.24, 0.24, 0.24, 0.24, 0.24, 0.24	

216. CTAB.2	2160., 2160., 2160., 2160.	14
217. CTAB.2	-1.E6, 1.E6	
218. CTAB.2	1., 2., 3., 4., 5.	3
219. CTAB.2	3., 4., 5., 6., 7., 8., 9., 10.	8
220. INJ.3	2160., 2160., 2160., 2160.	14
221. INJ.3	1.	
222. INJ.3	2.	
223. CTAB.3	-1.E6, 1.E6	
224. CTAB.3	1., 2., 3., 4., 5.	3
225. CTAB.3	72., 72., 72., 72., 72., 72., 72., 72., 72.	8
226. INJ.4	1.	
227. CTAB.4	-1.E6, 1.E6	
228. CTAB.4	1., 2., 3., 4., 5.	3
229. CTAB.4	72., 72., 72., 72., 72., 72., 72., 72.	8
230. CTAB.4	72., 72., 72., 72., 72., 72., 72., 72.	14
231. MASS.2	3., 4., 5., 6., 7., 8., 9., 10.	
232. MASS.2	3., 4., 5., 6., 7., 8., 9., 10.	4
233. MUS	1., 2., 3., 4., 5., 6., 7., 8., 9., 10.	
234. ES	1., 2., 3., 4., 5., 6., 7., 8., 9., 10.	4
235. ES	1., 2., 3., 4., 5., 6., 7., 8., 9., 10.	4
236. ES	1., 2., 3., 4., 5., 6., 7., 8., 9., 10.	4
237. ES	1., 2., 3., 4., 5., 6., 7., 8., 9., 10.	
238. REM	BCD 4 FLEXIBLE AIRFRAME DATA	
239. INDFLX	1.	
240. REM	BCD 3 AUTOPILOT DATA	
241. REM	BCD 3A. ENGINE DATA	
242. INDAUT	1.	
243. IN	1.	
244. ZN	5.41, 5.39, 5.39, 5.41	
245. YN	61.8, 39.7, -39.7, -61.8	
246. N	1.975, -1.975, -1.975, 1.975	
247. REM	BCD 3B. DRAG CHUTE DATA	
248. IC	1.	
249. IC	1.	
250. IC	1.	
251. IC	1.	
252. IC	1.	
253. IC	1.	
254. IC	1.	
255. IC	1.	
256. IC	1.	
257. IC	1.	
258. IC	1.	
259. IC	1.	
260. IC	1.	
261. IC	1.	
262. IC	1.	
263. IC	1.	
264. IC	1.	
265. IC	1.	
266. IC	1.	
267. IC	1.	
268. IC	1.	
269. IC	1.	
270. IC	1.	
271. IC	1.	
272. IC	1.	
273. IC	1.	
274. IC	1.	
275. IC	1.	
276. IC	1.	
277. IC	1.	
278. IC	1.	
279. IC	1.	
280. IC	1.	
281. IC	1.	
282. IC	1.	
283. IC	1.	
284. IC	1.	
285. IC	1.	
286. IC	1.	
287. IC	1.	
288. IC	1.	
289. IC	1.	

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1301 PGS          .04
1302 DELSIG       .1
1303 RPY          .1
1304 PHIG         .1
1305 RPY          BCD 4F. FLARE MANEUVER DATA
1306 XTJ          100.
1307 HTD          .5
1308 VXTD        .00.
1309 VHTD        -1.
1310 IIR          .
1311 LU           500.
1312 DA          .04
1313 TL           500.
1314 TU          10000.
1315 RPY          BCD 4G. HOLD MANEUVER DATA
1316 ALP DES      0.5890
1317 ITJ          47.70.
1318 KE           INT 1,1,1,1
1319 PM           .1
1320 RPY          BCD 5H. LANDING ROLL MANEUVER DATA
1321 ISP         .
1322 TRV         .
1323 ICH         .
1324 TBK         .
1325 ISS         .
1326 ILR         .
1327 ISS         .
1328 RPY          BCD 0I. ENGINE FAILURE STAGE DATA
1329 IC          INT 1,1,1,1
1330 XRF1         .
1331 IT1          INT 1,1,1,1
1332 XRF2         .
1333 IT2          INT 1,1,1,1
1334 H1          .
1335 IH1          INT 1,1,1,1
1336 H2          .
1337 IH2          INT 1,1,1,1
1338 HR1         .
1339 IH11         INT 1,1,1,1
1340 HR2         .
1341 IHR2         INT 1,1,1,1
1342 TR          .
1343 IT11         INT 1,1,1,1
1344 IT21         .
1345 ITR2         INT 1,1,1,1
1346 REM         BCD 5J. BRAKE COND. STAGE DATA
1347 IB         INT 1,1,1,1,1
1348 TBK1         .
1349 TBK1         INT 1,1,1,1,1
1350 TBK2         .
1351 TBK2         INT 1,1,1,1,1
1352 REM         BCD 4K. PITCH AUTOPILOT DATA
1353 ALPUL        .
1354 RFALPH       .5
1355 DELALA       .01
1356 PSH         -20.
1357 PSH         -20.
1358 RFALP2       .5
1359 DELQC        .
1360 DELQC2       .
1361 TST         5.1
1362 DELQF        .
1363 DELFD1       .
1364 DELQTO       .
1365 DELQL        -15.

```


0358. REM QU BCD 42: YAW AUTOPILOT DATA
 0357. RFB .5
 0358. DELBA .5
 0359. PPS .5
 0360. RFP SI .5
 0361. DP SIA .5
 0362. PPSI .5
 0363. DELRL -1.
 0364. DELRU -35.
 0365. REM BCD 4N. ROLL AUTOPILOT DATA
 0366. RFP HI .5
 0367. UPHIA .5
 0368. PSA -15.
 0369. DELPL -6.
 0370. DELPU .5
 0371. REM BCD 5N. THROTTLE AUTOPILOT DATA
 0372. TF INT .5, .5
 0373. NJF INT .5, .5
 0374. LR .5, .5
 0375. NB 1.05, 1.05, 1.05, 1.05
 0376. NLR -2., -2., -2., -2.
 0377. NTJ 2., 2., 2., 2.
 0378. K2 .5
 0379. K3 .5, .5, .5, .3333, .3333
 0380. K4 .5, .5, .5, .3333, .3333, .3333, .3333
 0381. K4 .25, .25, .25
 0382. REM BCD 40. BRAKE AUTOPILOT DATA
 0383. M3C .5
 0384. PU .5
 0385. DELTAN .5
 0386. OMCGU1 .5
 0387. MBL .5, .5, .5, .5, .5, .5
 0388. MBJ .5, .5, .5, .5, .5, .5
 0389. REM BCD 3P. CONTROL RESPONSE DATA
 0390. DELHS .5
 0391. DELRRD .5
 0392. DELA .5
 0393. NEU .5
 0394. REM BCD 3Q. INITIALIZATION
 0395. LAP .5
 0396. HR .5
 0397. DELQN .5
 0398. DELQDE .5
 0399. DELQD .5
 0400. DELPU .5
 0401. DELRU .5
 0402. REM BCD 4R. AUTOPILOT OUTPUT INC.
 0403. PITCHP 1
 0404. ROLLAP 1
 0405. THROAP 1
 0406. CONTRP 1
 0407. REM BCD 2STAGING DATA
 0408. REM BCD 4A. GEARS INTO PROGRAM
 0409. INJLG .5
 0410. ISTAGE .5
 0411. DECKES BCD 1HR
 0412. STSTU TRA .5
 0413. INJLG -1
 0414. REM BCD 4B. SMOOTH IMPACT STAGE
 0415. REM BCD 4DEL1, 4DEL2, 4DEL3, 4DEL4
 0416. AINCRS -1., -1., -1., -1.
 0417. STSTU TRA .5
 0418. .5
 0419. PRINT .5

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421.DELTS          .01
421.AMAXER         .001
422.PRTMIN         .
423.REM            BCU 5G. EFFICIENT AMAXER STAGE
424.AINCERS        BCD 4DELTA1DELTA2DELTA4DELTA5
425.STEST          .1,.1,.1,.1
426.              TRA
427.PRINT          .08
428.AMAXER         .04
429.DELTS          .04
430.REM            BCU 4D. SPOILER AERO STAGE
431.AINCERS        BCU 1ISS
432.STEST          .
433.              TRA
434.ATAB10         .030,.031
435.ATAB11         .1162,.1162
436.ATAB12         .
437.ATAB51         .3433,.3439
438.ATAB52         -.0327,-.0327
439.ATAB53         .
440.ATAB54         .267,.267
441.REM            BCU 3E. BOUNCE STAGE
442.ISTAGE         BCU 4DELTA1DELTA2DELTA4DELTA5
443.DECRES         BCU .00000000
444.STSTD          .
445.              TRA
446.PRINT          .02
446.DELTS          .01
447.AMAXER         .001
448.ISTAGE         .
449.AINCERS        BCU 4DELTA1DELTA2DELTA4DELTA5
450.STEST          .1,.1,.1,.1
451.              TRA
452.PRINT          .05
452.DELTS          .00
453.AMAXER         .01
454.ISTAGE         .
455.DECRES         BCU 4DELTA1DELTA2DELTA4DELTA5
456.STSTD          .00000000
457.              TRA
458.PRINT          .02
458.DELTS          .01
459.AMAXER         .001
460.ISTAGE         .
461.AINCERS        BCU 4DELTA1DELTA2DELTA4DELTA5
462.STEST          .1,.1,.1,.1
463.              TRA
464.PRINT          .05
464.DELTS          .00
465.AMAXER         .01
466.ISTAGE         .
467.DECRES         BCU 4DELTA1DELTA2DELTA4DELTA5
468.STSTD          .00000000
469.REM            BCU 4F. STIFF STRUT STAGE
470.AINCERS        BCU 1TIME
471.STEST          .
472.              TRA
473.INDLG          .2
474.AMAXER         .1
475.DELTS          .1
476.PRINT          .02
477.FTAB53         .000,.02,100,.02
478.INDSTF         .1
479.              TRA

```

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE G-MOD STAGE 1 PAGE 9

A. GEARS INTO PROGRAM

INITIAL PRINT OUT FOR VPCS

0. XCGRF AREFF D1RFF D2RFF
62.0000000E+02 30.9000000E+00 21.9000000E+01

PRINT CODES IDENTIFYING TIME HISTORY

2SDF							
TIME	YIMES	YG77F	YG77F	HGCTF	U777F	V777F	W777F
PI77R	QI77R	RI77R	AMACH	VA77F	OYNRP	YG77F1	YG77F1
ZG77F1	ALPHD	SETAD	ALPHD1	RETA01	GAM7D	SIG7D	THTPD
PSIPD	PHIPD	AX77F	AY77F	AZ77F	NTR7P	FOC	FCX
FCY	FCZ						
VPCS							
AMASS							
TFFS							
NT	NT						
SAC1							
CAVAH	CA	DN	CY	CL	CM	CNN	

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE G-MOD STAGE 1 PAGE 10

250F

0.	0.	0.	0.	12.082400E+01	21.8546595E+01	0.	25.246500E+00
11.5139087E+00	85.8959907E-01	0.	19.7138583E-02	22.000000E+01	57.3183679E+00	21.9698498E+01	0.
0.	0.	20.1439334E-01	0.	0.	-29.999843E-01	0.	35.0959949E-01
0.	0.	0.	0.	-32.1108781E+00	83.5850000E+04	0.	0.

VPCS

19.762852JE+03

TFFS

28.4356654E+04 74.5058060E-10

3.09067687E+04	-7.38268189E+03	-7.38268189E+03	3.09067687E+04
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SAC1

15.3434214E-02	20.4914606E-03	17.8486439E-01	0.	0.	-18.8936665E-03	0.
----------------	----------------	----------------	----	----	-----------------	----

AUTS

PITCH AUTOPILOT

DELQW	ALPHA	ALPHD1	ALPDD1	ALPHET	DELQDE
-14.3779512E-02	19.1993597E-03	0.	0.	19.1993597E-03	-52.7766706E-02

ROLL AUTOPILOT

PHIE	PHIET	DELPCIE
0.	0.	0.

ND1(IN) =	1.97378031E+00	-1.00000000E+00	-1.00000000E+00	1.97378031E+00
TD1(IN) =	3.08687595E+04	-7.38268189E+03	-7.38268189E+03	3.08687595E+04

THROTTLE AUTOPILOT

DELQD1	DELQD1	DELPC1	DELOD	DELRO	DELPP
-25.0000000E+00	35.0000000E+00	60.0000000E+00	72.2700000E-03	0.	0.

ND1 =	-1.25000000E-01	1.25000000E-01	1.25000000E-01	-1.25000000E-01
N	1.97500000E+00	-1.00000000E+00	-1.00000000E+00	1.97500000E+00
HT =	1.00000000E-01			
HT =	1.00000000E-01			

INTEG RTN.
INTEG RTN.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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INTEG RTN. HT = 1.0000000E-01
INTEG RTN. HT = 1.0000000E-01

2SOF

40.0000000E-02 40.0000000E-02 87.0793850E+00 35.5110277E-19 11.6223554E+01 21.8555033E+01 10.8065684E-16 25.1565558E+00
28.7513241E-19 19.7240581E-14 42.6543981E-18 19.7133741E-02 21.9998079E+01 57.3259896E+00 21.9898082E+01 34.8643999E-16
11.4854711E+00 65.6667665E-11 49.3027758E-17 11.5358498E-02 23.6016210E-16 29.9263894E-01 89.6199421E-19 35.7346721E-01
0. 0. 0. 0. 0. 0. 0.

VPCS

19.7628520E+03

TFFS

28.3060381E+04 0.

3.0786849E+04 -7.3824833E+03 -7.3824833E+03 3.0786849E+04

SAC1

15.3258007E-02 19.8841213E-03 17.9094376E-01 11.6354551E-18 64.3970611E-20 41.7857957E-03 78.4346928E-19

PITCH AUTOPILOT

AUTS
DELQ1 ALPHAE ALPHD1 ALPDD1 ALPHET DELODE
-80.1994441E-03 19.6890172E-03 11.5358498E-02 62.2227817E-03 68.7884086E-04 80.1994440E-03

ROLL AUTOPILOT

PHIE PHIE1 DELPCE
35.4289448E-18 11.8193416E-17 0.

THROTTLE AUTOPILOT
ND(IN) = 1.97022306E+00 -1.0000000E+00 -1.0000000E+00 1.97022306E+00
TD(IN) = 3.07580473E+04 -7.3824833E+03 -7.3824833E+03 3.07580473E+04
CONTROL RESPONSE

DELQD1 DELRD1 DELPC1 DELQD DELRD DELPD
25.3000000E+00 35.0000000E+00 59.0000000E+00 80.1994440E-03 0. 0.
ND1 = -1.2500000E-01 1.2500000E-01 1.2500000E-01 -1.2500000E-01
K = 1.97022306E+00 -1.0000000E+00 -1.0000000E+00 1.97022306E+00

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE G-MOD STAGE 1 PAGE 12

INTEG RTN. HT = 1.0000000E-01
INTEG RTN. HT = 1.0000000E-01
INTEG RTN. HT = 1.0000000E-01
INTEG RTN. HT = 1.0000000E-01

2SDF

80.1300000E-02 80.0000000E-02 17.5758142E+01 52.8938894E-18 11.1630324E+01 21.8566921E+01-67.7651415E-16 25.0315591E+00
43.3598410E-19-12.1197457E-34 73.3967844E-18 19.7128433E-02 21.9995532E+01 57.3315257E+00 21.9695829E+01 25.1026657E-17
11.6813221E+00 69.3338190E-01-17.7641547E-16-71.4547150E-63-41.2900642E-16-29.9156020E-01 65.4667322E-18 35.4182120E-01
J. 12.1459851E-17 19.8445920E-01 75.5579131E-17-32.1269308E+00 63.5850000E+04 0.
J. 0.

VPCS

19.7628523E+03

TFFS

28.1768928E+04 74.5058360E-10

3.06673466E+04 -7.38226577E+03 -7.38226577E+03 3.06673466E+04

SAC1

15.3062294E-02 20.6821668E-03 17.8588131E-01 41.9234051E-18-98.4620079E-20-23.8856300E-03-15.3527011E-18

PITCH AUTOPILOT

AUTS

DELON ALPHAE ALPHD1 ALFDD1 ALPHET DELODE
-98.970752E-04 13.4176623E-03-71.4547150E-03-68.4611440E-03 11.9208768E-03-24.8314544E-02

ROLL AUTOPILOT

PHIE PHIET DELPCE
12.1459851E-17 24.8519383E-17 0.

THROTTLE AUTOPILOT

ND(IN) = 1.96628536E+00 -1.0000000E+00 -1.0000000E+00 1.96628536E+00
TD(IN) = 3.06354917E+04 -7.38226577E+03 -7.38226577E+03 3.06354917E+04

CONTROL RESPONSE

DELQD1 DELRD1 DELPC1 DELQD FELRD DELPD
-25.3030000E+00 35.0000000E+00 69.0000000E+00-24.8314544E-02 0. 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSQF 2 CASE G-MOD STAGE 1 PAGE 13

ND1 = -1.25000000E-01 1.25000000E-01 -1.25000000E-01 -1.25000000E-01
N = 1.96628536E+00 -1.00000000E+00 -1.00000000E+00 1.96628536E+00

INTEG RTN. HT = 1.00000000E-01
INTEG RTN. HT = 1.00000000E-01
INTEG RTN. HT = 1.00000000E-01
INTEG RTN. HT = 1.00000000E-01

2SDF

12.00000000E-01 12.80000000E-11 26.3636097E+01 24.6241054E-17 10.7039491E+01 21.6578925E+01 -13.9211762E-15 24.9066458E+00
55.6822729E-19 -14.5205541E-04 10.3080377E-17 19.7123302E-02 21.9993380E+01 57.3380600E+00 21.9693997E+01 78.1666300E-17
11.4732316E+00 65.8870465E-11 -36.4913792E-16 -92.3742241E-03 -51.4375782E-16 -29.8948015E-01 20.3857095E-17 35.1122330E-01
E. 23.7845711E-17 19.7057893E-01 15.4598498E-16 -32.1490342E+00 63.5650000E+04 0.
G. G. 0.

VPCS

19.7628520E+03

TFFS

28.0339370E+04 74.9058060E-10

3.05350930E+04 -7.3820554E+03 -7.3820554E+03 3.05350930E+04

SAC1

15.2844713E-02 20.7085939E-03 17.8723997E-01 86.1196548E-10 -12.4719389E-19 -30.9928098E-03 -23.6704518E-10

AUTS

PITCH AUTOPILOT

DELON ALPHAE ALPH01 ALPOD1 ALPHET DELQDE

68.5056444E-03 98.4128298E-04 -92.3742241E-03 -75.4252783E-03 13.6681007E-04 68.5056444E-03

ROLL AUTOPILOT

PHIE PHJET DELPCF

23.7845711E-17 40.0181486E-17 0.

THROTTLE AUTOPILOT

ND(IN) = 1.96192765E+00 -1.00000000E+00 -1.00000000E+00 1.96192765E+00
TD(IN) = 3.04998412E+04 -7.3820554E+03 -7.3820554E+03 3.04998412E+04

CONTROL RESPONSE

DELQ01 DELRD1 DELPC1 DELQD DELRD DELPD

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE G-MOD STAGE 1 PAGE 14
25.8250000E+00 35.0000000E+30 60.0000000E+00 68.5056444E-03 0. 0.

ND1 = -1.2500000E-01 1.2500000E-01 1.2500000E-01 -1.2500000E-01
N = 1.96192765E+00 -1.0000000E+00 -1.0000000E+00 1.96192765E+00
INTEG RTN. HT * 1.0000000E-01
INTEG RTN. HT = 1.0000000E-01
INTEG RTN. HT = 1.0000000E-01
INTEG RTN. HT = 1.0000000E-01

2SOF

16.3300000E-01 16.3300000E-11 35.1513266E+01 73.4319665E-17 10.2450771E+01 21.8590897E+01 -23.0759506E-15 24.7813393E+00
61.8726712E-19 -14.0777461E-14 12.7935919E-17 19.7118170E-02 21.9991125E+01 57.3445896E+00 21.9691935E+01 17.3802908E-16
11.4694695E+00 64.6792589E-11 -60.4853446E-16 -80.9799754E-03 -65.6423813E-16 -29.8853064E-01 45.3278954E-17 34.7939498E-01
0. 37.7059693E-17 19.4896598E-01 25.6799597E-16 -32.1160969E+00 63.5150000E+04 0. 0.

VPCS

19.7628526E+03

TFFS

27.8756959E+04 74.5658060E-10

3.03887124E+04 -7.38184498E+03 -7.38184498E+03 3.03887124E+04

SAC1

15.2662817E-02 21.0853484E-03 17.8528581E-01 14.2745413E-17 -13.8586312E-19 -23.2268765E-03 -32.6654120E-18

AUTS

PITCH AUTOPILOT

DELON ALPHAE ALPHD1 ALPDO1 ALPHET DELQDE
15.6252715E-02 91.4973706E-04 -80.9099754E-03 -83.1963156E-03 10.2929072E-03 -49.6054284E-03

ROLL AUTOPILOT

PHIE PHIET DELPOE
37.7059693E-17 55.8926080E-17 0.

ND(IN) = 1.95710504E+00 -1.0000000E+00 -1.0000000E+00 1.95710504E+00
TD(IN) = 3.03497621E+04 -7.38184498E+03 -7.38184498E+03 3.03497621E+04
CONTROL RESPONSE

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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DELOD1 DELRD1 DELPC1 DELQD DELRD DELPD

-25.000000E+00 35.000000E+00 60.000000E+00 -49.615428E-03 0. 0.

ND1 = -1.2500000E-01 1.2500000E-01 1.2500000E-01 -1.2500000E-01

N = 1.9571050E+00 -1.0000000E+00 -1.0000000E+00 1.9571050E+00

INTEG RTN. HT = 1.0000000E-01

INTEG RTN. HT = 1.0000000E-01

INTEG RTN. HT = 1.0000000E-01

INTEG RTN. HT = 1.0000000E-01

2SDF

20.000000E-01 20.000000E-01 43.938937E+01 17.054054E-16 97.862791E+00 21.859411E+01 -33.730688E-15 24.701487E+00

64.253789E-19 11.051638E-04 14.898421E-17 19.710987E-02 21.998534E+01 57.349278E+00 21.968462E+01 32.081354E-16

11.494681E+00 64.471661E-01 -88.410053E-16 13.933963E-02 -74.128074E-16 -29.951838E-01 83.671060E-17 34.519811E-01

52.708585E-17 18.665162E-01 37.538951E-16 -31.829176E+00 63.585000E+04 0. 0.

0.

VPCS

19.762852E+03

TFFS

27.324801E+04 74.565886E-10

2.9879354E+04 -7.3815049E+03 -7.3815049E+03 2.9879354E+04

SAC1

15.233381E-02 22.803038E-03 17.691140E-01 20.864772E-17 -14.392347E-19 44.339309E-03 -41.634865E-18

PITCH AUTOPILOT

AUTS

DELON ALPHAE ALFHD1 ALPOD1 ALPHET DELODE

92.845412E-02 -69.283382E-02 13.933963E-02 20.000000E-02 -72.316406E-02 15.391734E+00

ROLL AUTOPILOT

PHIE PHLET DELPDE

52.708585E-17 76.580080E-17 0.

THROTTLE AUTOPILOT

ND(IN) = 1.4589927E+00 -1.0000000E+00 -1.0000000E+00 1.4589927E+00

TO(IN) = 1.4826978E+04 -7.3815049E+03 -7.3815049E+03 1.4826978E+04

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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CONTROL RESPONSE

DELQD1	DELRD1	DELPC1	DELOD	DELRO	DELPD
25.0000000E+00	35.0000000E+00	60.0000000E+00	49.9940057E-01	0.	0.
ND1 = -1.25000000E-01 N = 1.92950444E+00 1.25000000E-01 -1.00000000E+00 1.25000000E-01 -1.25000000E-01 1.92950444E+00					

INTEG RTN.	HT	HT	HT	HT	HT
INTEG RTN.	HT	HT	HT	HT	HT
INTEG RTN.	HT	HT	HT	HT	HT
INTEG RTN.	HT	HT	HT	HT	HT

2SDF

24.1016000E-01	24.0000000E-01	52.7251740E+01	33.7902083E-16	93.2201692E+00	21.8396583E+01	-51.5521465E-15	25.8950223E+00
17.2839782E-18	19.4064129E-13	34.8760821E-17	19.7053999E-02	21.9026491E+01	57.3263907E+00	21.9617164E+01	53.0542325E-16
11.6626995E+00	67.6212956E-01	-13.5245735E-15	11.7446766E-01	-18.3333530E-15	-30.3919355E-01	13.8412843E-16	37.2293504E-01
0.	72.5276027E-17	10.6684113E-01	57.4181798E-16	-32.2770711E+00	63.5650000E+04	0.	0.

VPCS

19.7628520E+03

TFFS

25.6420746E+04 74.5258066E-10

2.83227188E+04	-7.37921394E+03	-7.37921394E+03	2.83227188E+04
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SAC1

15.2030876E-02 14.0477610E-03 17.9472471E-01 31.9179910E-17-40.0694353E-19 18.1781789E-03-83.1362422E-18

AUTS

PITCH AUTOPILOT

DELQD	ALPHA	ALPHD1	ALPHD1	ALPHET	DELQDE
11.6602967E-01	-41.7870497E-02	10.7446706E-01	0.	11.9363031E-02	-12.2123095E-01

ROLL AUTOPILOT

PHIE	PHIET	DELPDE
72.5276027E-17	10.9263659E-16	0.

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE G-H00 STAGE 1 PAGE 17

THROTTLE AUTOPILOT
ND(IN) = 1.40695824E+00 -1.00000000E+00 -1.00000000E+00 1.40695824E+00
TO(IN) = 1.32063452E+04 -7.37921394E+03 -7.37921394E+03 1.32063452E+04
CONTROL RESPONSE

DELQD1	DELRD1	DELPD1	DELOD	DELRO	DELPD
-25.0000000E+00	35.0000000E+00	60.0000000E+00	87.1261661E-02	0.	0.
ND1 = -1.25000000E-01 1.25000000E-01 1.25000000E-01 -1.25000000E-01					
N = 1.87950444E+00 -1.00000000E+00 -1.00000000E+00 1.87950444E+00					
INTEG RTN.	HT	1.00000000E-01	1.00000000E-01	1.00000000E-01	1.00000000E-01
INTEG RTN.	HT	1.00000000E-01	1.00000000E-01	1.00000000E-01	1.00000000E-01
INTEG RTN.	HT	1.00000000E-01	1.00000000E-01	1.00000000E-01	1.00000000E-01
INTEG RTN.	HT	1.00000000E-01	1.00000000E-01	1.00000000E-01	1.00000000E-01

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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ATARI0 .030,.039
ATARI1 .1162,.1162
ATARI2 .1.0
ATARI51 .3439,.3439
ATARI52 -.0327,-.0327
ATARI53 0.0
ATARI54 .267,.267
REM BCD 3E. 3OUNGE STAGE
ISTAGE 1
DECREAS BCD 40DELTA10DELTA20DELTA40DELTA5
STESTD 0.0.0.0.0.
TRA

2SDF

14.213250E+00 14.213250E+00 30.011576E+02 20.052705E-13 23.268834E+00 19.132994E+01 -41.109894E-14 29.212633E+00
-18.066389E-15 -33.921271E-13 -27.713347E-17 17.337647E-02 19.354721E+01 44.490029E+00 19.354703E+01 55.078609E-14
-26.914750E-02 86.8199C4E-11 -12.316793E-14 -16.959936E-11 39.083274E-15 79.676358E-03 16.394935E-14 87.606662E-01
0.0
-0.0

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.0	30.473400E+03	37.5846010E+04	0.0	19.452318E-02	-15.096429E+03	-32.388839E+01	13.513073E+04
0.0	41.538246E+03	34.615440E+04	0.0	33.719803E-02	-10.097616E+03	-22.784964E+01	15.580644E+04
0.0	41.538246E+03	34.615440E+04	0.0	33.719803E-02	-10.097616E+03	-22.784964E+01	15.580644E+04
68.423154E-03	42.079840E+03	34.615440E+04	26.099412E+03	37.622015E-02	-30.488644E+03	-33.303747E+00	15.552937E+04
68.423194E-03	42.079840E+03	34.615440E+04	26.099412E+03	37.622015E-02	-30.488644E+03	-33.303747E+00	15.552937E+04

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDelta
53.301000E-02	19.326100E+11	0.0	0.0	-0.0	0.0	0.0	-12.827454E+C0
53.301000E-02	19.326100E+11	0.0	0.0	-0.0	0.0	0.0	-27.032000E-01
53.301000E-02	19.326100E+11	0.0	0.0	-0.0	0.0	0.0	-27.032000E-01
65.616521E-03	63.262000E-02	17.497983E+02	10.387886E-10	-28.667039E+03	33.999330E+02	0.0	68.623194E-03
65.616521E-03	63.262000E-02	17.497983E+02	10.387886E-10	-28.667039E+03	33.999330E+02	0.0	68.623194E-03

SD2	SD1	S	S2D2	S2D1	S2	ONETO1	ONET
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	28.719885E-03	0.0	0.0	0.0	37.777034E+00	-99.563556E+03
0.0	0.0	28.719885E-03	0.0	0.0	0.0	37.777034E+00	-99.563556E+03

FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYH
11.581941E+03	20.771660E-13	-52.178024E+03	74.639433E-08	-01.925245E+04	-23.288061E-08	11.581941E+03	20.771660E-10

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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FZM LH HM NM
-52.1788243E+03 74.6094339E-08-80.9252459E+04-23.2880613E-08

WPCS
19.7628520E+03

IFFS
47.3664943E+02 18.6264515E-10

4.45334947E+03 -6.40843537E+03 -6.40843537E+03 4.45334947E+03
SAC1
13.9973794E-02-82.3048755E-03 20.6511555E-01 29.0534729E-16 45.9797719E-17 10.1972271E-02-19.5568460E-17

PITCH AUTOPILOT

DELON ALPHAE ALPHD1 ALPDD1 ALPHET DELODE
13.8666987E+00 78.1275532E-03-16.9599305E-01 0. 88.9361407E-03 12.0879758E+00

ROLL AUTOPILOT

PHIE PHIET DELPCE
-11.3339811E-15-10.8719796E-15 0.

THROTTLE AUTOPILOT

ND(IN) = 1.00000000E+00 -1.00000000E+00 -1.00000000E+00 1.00000000E+00
TD(IN) = 1.62326570E+04 -6.40843537E+03 -6.40843537E+03 1.62326570E+04
CONTROL RESPONSE

DELOD1 DELRD1 DELPD1 DELQD DELRD DELPD
25.1060000E+00 35.1060000E+00 60.0620000E+00 12.0879758E+00 0. 0.
ND1 = -1.25000000E-01 1.25000000E-01 1.25000000E-01 -1.25000000E-01
N = 1.11804565E+00 -1.00000000E+00 -1.00000000E+00 1.11804565E+00

INTEG RTN. HT = 3.2000000E-02
INTEG RTN. HT = 3.26600000E-02

2SOF

14.2932500E+00 14.2932500E+00 30.1662519E+02 20.4961952E-13 23.2375688E+00 19.0799790E+01-40.2368158E-14 29.9833049E+00
-17.2342905E-16-28.1853774E-03-31.7894154E-17 17.3312833E-02 19.3141292E+01 44.3036488E+00 19.3138425E+01 55.7600411E-14

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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10.5228168E-01 89.3073098E-01-12.0828211E-14 31.7471641E-01 30.9633925E-15-31.2162185E-02 16.5415516E-14 86.1856782E-01
0. -68.8020098E-15-27.7076000E-01 12.3454787E-14-16.6597456E+00 63.6650000E+04 0.
-0. -0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FG2
0.	30.4704930E+03	37.5840000E+04	0.	11.2041276E+00-15.0622485E+03-32.3075227E+01	13.6164919E+04		
0.	41.5382400E+03	34.6154400E+04	0.	15.2438383E+00-36.8513315E+03-22.7499251E+01	15.5852725E+04		
0.	41.5382400E+03	34.6154400E+04	0.	15.2438383E+00-36.8513315E+03-22.7499251E+01	15.5852725E+04		
58.4055998E-03	42.0798400E+03	34.6154400E+04	21.5310687E+03	16.4014796E+00-30.4388796E+03-67.4352917E+00	15.5579139E+04		
58.4055998E-03	42.0798400E+03	34.6154400E+04	21.5310687E+03	16.4014796E+00-30.4388796E+03-67.4352917E+00	15.5579139E+04		

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDELTA
53.0000000E-02	19.2896331E+01	0.	0.	-0.	0.	0.	-12.6365515E+00
53.0000000E-02	19.2615377E+01	0.	0.	-0.	0.	0.	-26.6845361E-01
53.0000000E-02	19.2615377E+01	0.	0.	-0.	0.	0.	-26.6845361E-01
38.9152004E-03	37.4633752E-02	-84.2486217E+01	81.4117251E-11	-21.6492838E+03-16.4559496E+02	0.	0.	58.4055998E-03
38.9152004E-03	37.4633752E-02	-84.2486217E+01	81.4117251E-11	-21.6492838E+03-16.4559496E+02	0.	0.	58.4055998E-03

SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	20.7198857E-03	0.	0.	0.	-18.2843885E+00-98.3810889E+00	-18.2843885E+00-98.3810889E+00
0.	0.	20.7198857E-03	0.	0.	0.	-18.2843885E+00-98.3810889E+00	-18.2843885E+00-98.3810889E+00

FTRA	FTRD	FTRC	MTX	NTY	NTZ	FXM	FYM
48.2259430E+02	16.5659063E-10	-43.0621373E+03-30.6069469E-09-76.4532536E+04-59.5706964E-09	48.2259430E+02	16.5659063E-10			
FZH	LH	HM	NH				
-43.0621373E+03-30.6069469E-09-76.4532536E+04-59.5706964E-09							

VPCS

19.7628520E+03

TFFS

31.6419870E+02 18.6264515E-10

4.29873437E+03 -6.39352614E+03 -6.39352614E+03 4.29873437E+03

SAC1

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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26.7000000E-02 20.1650888E-02 10.4186423E-01 28.5154577E-16 43.9688302E-17 30.8992024E-02-18.3438462E-17

PITCH AUTOPILOT

AUTS
DELON ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
13.6666987E+00 78.1275532E-03 31.7471641E-01 0. 88.9361407E-03 12.0879758E+00

ROLL AUTOPILOT

PHIE PHLET DELPCE
-11.3339011E-15-10.8719796E-15 0.

THROTTLE AUTOPILOT

NO(IN) = 1.0000000E+00 -1.0000000E+00 -1.0000000E+00 1.0000000E+00
TD(IN) = 1.62177478E+04 -6.39352614E+03 -6.39352614E+03 1.62177478E+04
CONTROL RESPONSE

DELQD1 DELRD1 DELPD1 DELQD DELRD DELPD
25.3000000E+00 35.0000000E+00 60.0000000E+00 12.0879758E+00 11.1863587E-13 0.

NO1 = -1.2500000E-01 1.2500000E-01 1.2500000E-01 -1.2500000E-01
N = 1.10804565E+00 -1.0000000E+00 -1.0000000E+00 1.10804565E+00
INTEG RTN. HT = 6.3000000E-03
INTEG RTN. HT = 1.2000000E-02

2SDF

14.3732500E+00 14.3732500E+00 30.3205939E+02 20.9463809E-13 23.1049040E+00 19.0275531E+01-38.8922498E-14 30.6893163E+00
-17.4850094E-16-24.3467934E-13-33.3473637E-17 17.2847957E-02 19.2714099E+01 44.1172495E+00 19.2721180E+01 56.9114153E-14
22.3155596E-01 91.6228551E-01-11.7112656E-14 26.6961131E-01 53.8246167E-15-66.3408179E-02 16.9196952E-14 84.9887621E-01
0. -76.2619894E-15-22.5825575E-01 20.2191160E-14-19.1066496E+00 63.5650000E+04 0.
-0. -0.

LGEAR

DELTA P P2 FT SR SF AA FG2
0. 30.4704000E+03 37.5840000E+04 0. 10.3819777E+00-15.0648349E+03-32.3130704E+01 13.6162333E+04
0. 41.5382400E+03 34.6154400E+04 0. 12.7671577E+00-30.0590510E+03-22.7557690E+01 15.5845006E+04
0. 41.9382400E+03 34.6154400E+04 0. 12.7671577E+00-30.0590510E+03-22.7557690E+01 15.5845006E+04
10.3500468E-02 43.6219490E+03 34.6154400E+04 43.1212652E+03 13.4529483E+00-40.0507852E+03 23.2446237E+00 14.6291508E+04
11.3500468E-02 43.6219490E+03 34.6154400E+04 43.1212652E+03 13.4529483E+00-40.0507852E+03 23.2446237E+00 14.6291508E+04

MUVP VGPT FTRX FTRY FTRZ MA HB DDELTA
53.0000000E-02 19.2508784E+01 0. 0. -0. 0. 0. -12.3694625E+00

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDSF 2 CASE G-MOD STAGE 1 PAGE 136

53.000000E-02 19.2269297E+01 0. 0. -0. 0. 0. -25.3296384E-01
53.000000E-02 19.2269297E+01 0. 0. -0. 0. 0. -25.3296384E-01
11.3044622E-03 10.8473348E-02 49.3709082E+01 15.9599449E-10 -43.6738231E+03 94.3559780E+01 0. 10.0580468E-02
11.3044622E-03 10.8473348E-02 49.3709082E+01 15.9599449E-10 -43.6738231E+03 94.3559780E+01 0. 10.0580468E-02

SJ2 SD1 S S2D2 S2D1 S2 OMET01 OMET
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
48.7688237E-01 19.8677873E-01 76.8628070E-03 0. 0. 0. 10.4839976E+00 -10.0473200E+01
48.7688237E-01 19.8677873E-01 76.8628070E-03 0. 0. 0. 10.4839976E+00 -10.0473200E+01

FTRA FTRB FTRC HTX HTY HTZ FXM FYM
13.8856848E+03 32.3975353E-10 -86.2425304E+03 -69.5963915E-09 -14.4512012E+05 -11.3102906E-09 13.8856848E+03 32.3975353E-10
FZH LH RH NH

-84.9541147E+03 20.9165213E-09 -14.1966962E+05 -11.3102906E-09

VPCS

19.7528520E+03

TFFS

-12.3115435E+01 0.

3.98554296E+03 -6.37856789E+03 Y(I) -6.37856789E+03 3.98554296E+03

SAC1

26.7000000E-02 19.6453848E-02 10.6977815E-01 27.6385867E-16 44.6901526E-17 29.8169821E-02 -17.3825519E-17

PITCH AUTOPILOT

AUTS

DELON

ALPHA

ALPH01

ALPDD1

ALPHET

DELODE

13.6666987E+00 78.1275532E-03 26.6961131E-01 0.

88.9361407E-03 12.0879758E+00

ROLL AUTOPILOT

PHIE

PHIET

DELPDE

-11.3339811E-15 -10.8719796E-15 0.

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE G-MOD STAGE 1 PAGE 137

ND(IN) = 1.0000000E+00 THROTTLE AUTOPILOT
TD(IN) = 1.62027895E+04 -1.0000000E+00 -1.0000000E+00 1.0000000E+00
-6.37856789E+03 -6.37856789E+03 1.62027895E+04
CONTRCL RESPONSE

DELQ01 DELQ01 DELPC1 DELQ0 DELRD DELPD
25.000000E+00 35.000000E+00 60.000000E+00 12.0879758E+00 0. 0.
N01 = -1.2500000E-01 1.2500000E-01 1.2500000E-01 -1.2500000E-01
H = 1.09804565E+00 -1.0000000E+00 -1.0000000E+00 1.09804565E+00
INTEG RTN. HT = 1.2000000E-02
INTEG RTN. HT = 1.2000000E-02

2SDF

14.4532500E+00 14.4532500E+00 14.4746068E+02 21.4170246E-13 22.8637139E+00 18.9771848E+01 -37.2598843E-14 31.3162679E+03
-16.3488563E-16 -21.9434477E-03 -39.7623934E-17 17.2203412E-02 19.2338407E+01 43.9365307E+00 19.2310432E+01 58.2989869E-14
32.8035250E-01 93.7053518E-01 -11.2494774E-14 24.2587621E-01 63.6523556E-15 -97.7231992E-02 17.3668557E-14 83.9330205E-01
-0. -84.1037202E-15 -21.7434152E-01 23.1994427E-14 -20.4314161E+00 63.5850000E+04 0. -0.
-0. -0.

LGEAR

DELTA P P2 FT SR SF AA FC2
0. 30.4704000E+03 37.5840000E+04 0. 10.1236589E+00 -15.0656648E+03 -32.3148505E+01 13.6161503E+04
0. 41.5382400E+03 34.6154400E+04 0. 11.4270000E+00 -30.0632434E+03 -22.7589428E+01 15.5640813E+04
0. 41.5382400E+03 34.6154400E+04 0. 11.4270000E+00 -30.0632434E+03 -22.7589428E+01 15.5640813E+04
12.0064995E-02 49.1507473E+03 34.6154400E+04 54.4850474E+03 11.8017471E+00 -50.1245331E+03 33.0106416E+00 13.7381321E+04
12.0064995E-02 49.1507473E+03 34.6154400E+04 54.4850474E+03 11.8017471E+00 -50.1245331E+03 33.0106416E+00 13.7381321E+04

HUVP VGPT FTRX FTRY FTRZ HA HB ODELTA
53.0060000E-02 19.2116435E+01 0. 0. -0. 0. 0. -12.0297349E+00
53.0060000E-02 19.2116435E+01 0. 0. -0. 0. 0. -23.0934032E-01
53.0060000E-02 19.2116435E+01 0. 0. -0. 0. 0. -23.0934032E-01
13.2884811E-03 12.7218142E-02 -73.0430103E+01 18.8973791E-10 -54.9671595E+03 -13.8168232E+02 0. 12.0064995E-02
13.2884811E-03 12.7218142E-02 -73.0430103E+01 18.8973791E-10 -54.9671595E+03 -13.8168232E+02 0. 12.0064995E-02

SD2 SD1 S S202 S201 S2 OMET01 OMET
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
12.9828914E+00 25.9333334E-01 24.9333334E-02 0. 0. 0. -15.3520257E+00 -10.1154555E+01
12.9828914E+00 25.9333334E-01 24.9333334E-02 0. 0. 0. -15.3520257E+00 -10.1154555E+01

FTRA FTRB FTRC HTX HTY HTZ FXH FVH
14.6016116E+03 38.6144365E-10 -10.8970095E+04 -10.6731509E-08 -18.8805555E+05 12.3320655E-08 14.6016116E+03 38.6144305E-10

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE G-MOD STAGE 1 PAGE 138

FZM LM NM NM
-10.5540139E+04 -41.6961075E-10 -18.2025260E+05 12.3320655E-08
VPCS
19.7628520E+03
TFFS
-34.1613021E+02 0.

3.67208804E+03 -6.36402991E+03 -6.36402991E+03 3.67208804E+03

SAC1

26.7000000E-02 19.1584587E-02 10.9487494E-01 26.5487667E-16 49.5696570E-17 28.8030455E-02 16.2668938E-16

PITCH AUTOPILOT

AUTS
DELQN ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
13.8666987E+00 78.1275532E-03 24.2587621E-01 0. 88.9361407E-03 12.0879758E+00

ROLL AUTOPILOT

PHIE PHLET DELPDE
-11.3339811E-15 -10.8719796E-15 0.

ND(IIN) = 1.00000000E+00 -1.00000000E+00 -1.00000000E+00 1.00000000E+00
TD(IIN) = 1.61882515E+04 -6.36402991E+03 -6.36402991E+03 1.61882515E+04
CONTROL RESPONSE

DELQD1 DELRD1 DELPD1 DELQD DELRD DELPD
25.0000000E+00 35.0000000E+00 60.0000000E+00 12.0879758E+00 11.2798279E-13 0.
ND1 = -1.25000000E-01 1.25000000E-01 1.25000000E-01 -1.25000000E-01
H = 1.08864565E+00 -1.00000000E+00 -1.00000000E+00 1.08864565E+00
INTEG RTH. HT = 1.20000000E-02
INTEG RTH. HT = 1.20000000E-02

2SDF

14.5332500E+00 14.5332500E+00 30.6282907E+02 21.8799628E-13 22.5842838E+00 10.9286739E+01 -35.3187105E-14 31.6284374E+08

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE G-MOD STAGE 1 PAGE 140

26.7000000E-02 18.7403054E-02 11.1559547E-01 25.2298516E-16 49.128732EE-17 28.6433387E-02-13.7427888E-17

AUTS

PITCH AUTOPILOT

DELON

ALPHA

ALPHD1

ALPDD1

ALPHET

DELQDE

13.8666987E+00 78.1275532E-03 18.3432813E-01 0.

88.9361407E-03 12.0879758E+00

ROLL AUTOPILOT

PHIE

PHIET

DELPCE

-11.3339811E-15-10.8719796E-15 0.

ND(IN) = 1.0000000E+00
TD(IN) = 1.61737845E+04

THROTTLE AUTOPILOT
-1.0000000E+00 -1.0000000E+00
-6.34956285E+03 -6.34956285E+03

1.0000000E+00
1.61737845E+04

CONTROL RESPONSE

DELQD1

DELRO1

DELPD1

DELQD

DELRO

DELPD

25.0000000E+00 35.0000000E+00 60.0000000E+00 12.0879758E+00 11.3260496E-13 0.

ND1 = -1.2500000E-01
N = 1.37804565E+00

1.2500000E-01 1.2500000E-01
-1.0000000E+00 -1.0000000E+00

-1.2500000E-01
1.07804565E+00

INTEG RTN.
INTEG RTN.

HT = 1.2000000E-02
HT = 1.2000000E-02

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE G-MOD STAGE 1 PAGE 302

ND(IN) = -2.00000000E+00 -2.00000000E+00 -2.00000000E+00 -2.00000000E+00
TO(IN) = 3.10708549E+04 -2.12466332E+04 -2.12466332E+04 3.10708549E+04
THROTTLE AUTOPILOT
CONTRCL RESPONSE

DELQ01 DELQ01 DELPD1 DELQ0 DELQ0 DELPD
-25.0000000E+00 -35.0000000E+00 60.0000000E+00 79.8597584E-01 0.
ND1 = -1.25000000E-01 -1.25000000E-01 -1.25000000E-01 -1.25000000E-01
N = -1.75000000E+00 -1.75000000E+00 -1.75000000E+00 -1.75000000E+00
INTEG RTN: HT = 6.0000000E-03
INTEG RTN: HT = 6.0000000E-03

2SDF

22.3732500E+00 22.3732500E+00 43.1286759E+02 25.2918226E-11 19.0502366E+00 11.9183677E+01 -85.0441578E-12 23.6426833E-02
-58.1081798E-12 58.1081798E-12 29.7878226E-13 58.1081798E-12 11.9183677E+01 16.8724334E+00 11.9183677E+01 16.8724334E+00
94.8557848E-12 11.9183677E+01 40.8837133E-12 58.1081798E-12 24.6641550E-12 -26.3710762E-02 11.9183677E+01 16.8724334E+00
-0. -6.0620572E-12 -99.8921245E-01 40.8837133E-12 31.9280837E+00 63.5850000E+04 0. -0.
-0. -0.

LGEAR

DELTA P P2 FT SR SF AA FC2
28.8632700E+00 19.4458833E+04 38.1085360E+04 97.3336991E+03 83.7391408E-03 -95.8261293E+03 32.3363721E+00 73.4729449E+03
24.6027198E+00 18.8227848E+04 34.9486843E+04 13.9103303E+04 24.9497412E-02 -13.4890054E+04 31.8957911E+00 83.1646447E+03
24.6027198E+00 18.8227848E+04 34.9486843E+04 13.9103303E+04 24.9497412E-02 -13.4890054E+04 31.8957911E+00 83.1646447E+03
23.1035822E+00 17.0587430E+04 34.9470939E+04 12.8489197E+04 29.7156483E-02 -12.3860524E+04 31.8611438E+00 90.9160758E+03
23.1035822E+00 17.0587430E+04 34.9470939E+04 12.8489197E+04 29.7156483E-02 -12.3860524E+04 31.8611438E+00 90.9160758E+03

HUVP VGPT FTRX FTRY FTRZ MA HS DOELTA
97.1458300E-05 57.8887113E-14 94.4583815E+00 -14.8317927E-07 -97.3337855E+03 16.2754935E+01 0. 28.8632704E-02
18.7347890E-05 11.1755188E-11 -26.1733936E+03 16.1113623E-07 -13.9172166E+04 -46.0297707E+03 45.8285679E+03 24.6027198E-02
18.7347890E-05 11.1755188E-11 -26.1733936E+03 16.1113623E-07 -13.9172166E+04 -46.0297707E+03 45.8285679E+03 24.6027198E-02
18.7347890E-05 11.1755188E-11 -26.1733936E+03 16.1113623E-07 -13.9172166E+04 -46.0297707E+03 45.8285679E+03 24.6027198E-02
18.7347890E-05 11.1755188E-11 -26.1733936E+03 16.1113623E-07 -13.9172166E+04 -46.0297707E+03 45.8285679E+03 24.6027198E-02

SD2 SD1 S S2O2 S2O1 S2 OHETD1 OHET
24.6221578E-02 53.4139467E-13 37.2669628E-02 0. 0. 20.8292787E-03 30.1398027E-01 -69.2427527E+00
24.6011450E-02 36.8289422E-12 12.6553241E-01 0. 0. 20.8278317E-03 -32.3558699E-01 -36.9453322E+00
24.6011450E-02 36.8289422E-12 12.6553241E-01 0. 0. 20.8278317E-03 -32.3558699E-01 -36.9453322E+00
15.9837799E-02 47.4913794E-13 12.6553241E-01 0. 0. 20.7294346E-03 -39.6223104E-01 -36.3445224E+00
15.9837799E-02 47.4913794E-13 12.6553241E-01 0. 0. 20.7294346E-03 -39.6223104E-01 -36.3445224E+00

FTRA FTRB FTRC HTX HTY HTZ FXH FYH
-1.0802228E+04 78.5549828E-37 -63.1678698E+04 34.8302637E-06 -13.6552766E+05 -12.3468680E-06 -10.0802228E+04 78.5549828E-07

D-27

ORIGINAL PAGE 13
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE G-HOD STAGE 1 PAGE 303

FZH LM HH NH
-63.1678893E+04 35.2495356E-06-13.0733541E+05-12.3458680E-06

VPCS

19.7628520E+03

TFFS

-30.1864543E+04-74.5058060E-10

-1.71513943E+04 -1.71513943E+04 -1.71513943E+04 -1.71513943E+04

SACS

26.7000000E-02 26.7753701E-02-64.0489830E-04 96.4855640E-14 36.4081347E-14 52.1440509E-02-84.7025384E-14

PITCH AUTOPILOT

AUTS

DELQN

ALPHA

ALPH01

ALPH01

ALPHET

DELQDE

13.8666987E+00 78.1275532E-03 52.0597102E-02 0.

88.9361407E-03 79.0597584E-01

ROLL AUTOPILOT

PHIE

PHIET

DELPDE

-11.3339811E-15-10.8719796E-15 0.

THROTTLE AUTOPILOT

NO(IN) = -2.0000000E+00
TD(IN) = 3.10003692E+04

-2.0000000E+00 -2.0000000E+00
-2.11761475E+04 -2.11761475E+04

-2.0000000E+00
3.10003692E+04

CONTROL RESPONSE

DELQ01

DELQ01

DELQ01

DELQ0

DELQD

DELQD

-25.0000000E+00 35.0000000E+00 60.0000000E+00 79.0597584E-01 14.6865746E-13 0.

NO1 = -1.2500000E-01
N = -1.7750000E+00

-1.2500000E-01
-1.7750000E+00

-1.2500000E-01
-1.7750000E+00

-1.2500000E-01
-1.7750000E+00

INTEG RTN.
INTEG RTN.

HT = 6.0000000E-03
HT = 3.0000000E-03

2SDF

22.4532500E+00 22.4532500E+00 43.1237014E+02 28.3056958E-11 19.0083937E+00 11.8375627E+01-79.2039133E-12 21.7604941E-02

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE G-MOD STAGE 1 PAGE 304

-74.4846541E-14 54.2620416E-04 25.3398892E-13 10.6937682E-02 11.8375927E+01 16.6444342E+00 11.8374919E+01 39.0318145E-11
48.3715259E-02 10.5324308E-02 38.3368162E-12 72.5360093E-02 38.9523155E-12 22.4445905E-02 10.8917756E-11 11.9121814E-02
0. 70.8339062E-12 10.2597646E+00 42.7463416E-11 34.4518218E+00 63.5850000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

29.3199308E-03 19.8529620E+14 38.1085360E+04 59.3717486E+03 14.9816742E-01 97.8257106E+03 33.1614881E+00 71.8713970E+03
26.1433491E-03 20.1864061E+14 34.5486843E+04 13.6283444E+03 14.5594706E+04 32.8582127E+00 73.3626690E+03
26.1433491E-03 20.1864061E+14 34.5486843E+04 13.6283444E+03 14.5594706E+04 32.8582127E+00 73.3626690E+03
24.7979699E-03 18.7746156E+14 34.9470939E+04 14.0355696E+04 13.6021270E+04 32.8227235E+00 82.3439048E+03

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DDelta

14.2320426E-04 84.3149472E-14 14.1426183E+01 15.3593495E-07 95.3716693E+03 24.3036185E+01 0. 29.3199308E-03
17.9968871E-03 18.5619357E-11 27.7559819E+03 16.6223510E-07 15.0337122E+04 47.3542626E+03 47.2354338E+03 26.1433491E-03
17.9968871E-03 18.5619357E-11 27.7559819E+03 16.6223510E-07 15.0337122E+04 47.3542626E+03 47.2354338E+03 26.1433491E-03
18.5619357E-11 27.7559819E+03 16.6223510E-07 15.0337122E+04 47.3542626E+03 47.2354338E+03 44.4975375E+03 24.7979699E-03
18.5619357E-11 27.7559819E+03 16.6223510E-07 15.0337122E+04 47.3542626E+03 47.2354338E+03 44.4975375E+03 24.7979699E-03

SD2

SD1

S

S2D2

S2D1

S2

OMETD1

OMET

-50.2609791E-02 25.5539581E-13 97.6311847E-02 0. 0. 20.8292707E-03 45.0067010E-01 68.9536273E+00
-16.1155121E-01 29.7906158E-03 12.9330929E-01 0. 0. 20.8278917E-03 11.2031959E-01 67.8883715E+00
-16.1155121E-01 29.7906158E-03 12.9330929E-01 0. 0. 20.8278917E-03 11.2031959E-01 67.8883715E+00
-18.7668671E-01 39.0369146E-02 12.6834678E-01 0. 0. 20.7294346E-03 23.1787324E-01 66.5747831E+00
-18.7668671E-01 39.0369146E-02 12.6834678E-01 0. 0. 20.7294346E-03 23.1787324E-01 66.5747831E+00

FTRA

FTRR

FTRC

MTX

MTY

MTZ

FXH

FYH

-10.6082136E+04 83.5453141E-07 58.6646561E+04 60.8655467E-06 17.9290115E+05 16.1301907E-06 10.6082136E+04 83.5453141E-07
FZH LH MH NH

-68.1592573E+04 61.3528176E-06 18.0184898E+05 16.1301907E-06

VPCS

19.7628520E+03

TFFS

-30.3835701E+04 74.5058060E-10

-1.72633921E+04

-1.72633921E+04

-1.72633921E+04

-1.72633921E+04

SAC1

ORIGINAL PAGE 14
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE G-MOD STAGE 1 PAGE 305

26.7000000E-02 26.7698988E-02-69.9161662E-04 50.4729983E-14 31.0049055E-14 54.3845628E-02-83.3779489E-14

AUTS

DELON

ALPHA

ALPH01

ALPH01

ALPHET

DELQDE

13.8666987E+00 78.1275532E-03-72.5360098E-02 0.

88.9361407E-03 78.2597584E-01

PITCH AUTOPILOT

ROLL AUTOPILOT

PHIE

PHIET

DELPOE

-11.3339811E-15-10.8719796E-15 0.

ND(IIN) = -2.03000000E+00
TD(IIN) = 3.09279818E+04

THROTTLE AUTOPILOT
-2.00000000E+00 -2.00000000E+00 -2.00000000E+00
-2.11037602E+04 -2.11037602E+04 3.09279818E+04
CONTROL RESPONSE

DELQD1

DELQD1

DELQD1

DELQD

DELQD

DELQD

-25.0000000E+00 35.0000000E+00 60.0000000E+00 78.2597584E-01 14.8877546E-13 0.

ND1 = -1.2500000E-11
H = -1.7850000E-03

-1.2500000E-01 -1.2500000E-01 -1.2500000E-01
-1.7850000E+00 -1.7850000E+00 -1.7850000E+00

INTEG RTN.
INTEG RTN.

HT = 6.3063000E-03
HT = 6.3063000E-03

2SDF

-22.5332500E+00 22.5332500E+00 43.2180692E+02 31.5388936E-11 18.9808539E+00 11.7542196E+01-71.4715787E-12 10.3613968E-03
-54.6144017E-14 47.3542249E-04 24.8463386E-13 10.5290850E-02 11.7542197E+01 16.4108458E+00 11.7542024E+01 41.8022673E-11
28.1487453E-02 50.5364811E-04 34.8397212E-12 16.8664448E-01 47.1037495E-12 98.2144458E-03 20.3764867E-11-93.1641775E-03
-6. -6. -6. -6. -6. -6. -6. -6.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

29.2816830E-02 19.8179530E+04 38.1005300E+04 99.2308446E+03-22.5768120E-01-97.6464170E+03 33.3422943E+00 72.0164602E+03
27.5181337E-02 21.2866226E+04 34.9486843E+04 15.8329745E+04-40.5407965E-01-15.3876187E+04 33.7150168E+00 69.7836733E+03
27.2181337E-02 21.2866226E+04 34.9486843E+04 15.8329745E+04-40.5407965E-01-15.3876187E+04 33.7150168E+00 69.7836733E+03
26.8592822E-02 20.1675791E+04 34.9470939E+04 14.9366432E+04-45.7059285E-01-14.5402784E+04 33.7914053E+00 75.7682395E+03
26.1859282E-02 20.1675791E+04 34.9470939E+04 14.9366432E+04-45.7059285E-01-14.5402784E+04 33.7914053E+00 75.7682395E+03

HUVP

VGPT

FTPX

FTRY

FTRZ

HA

HB

DOELTA

ORIGINAL PAGE IS
OF POOR QUALITY

D-30

C-3

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF		2	CASE G-H00	STAGE 1	PAGE	306
26.1831339E-04	15.3987202E-03	26.9738291E+01	15.6317322E-07	99.2015933E+03	44.6450946E+04	0.29.2816830E-02
17.8295577E-03	10.5446598E-01	28.3981540E+03	16.8524688E-07	18.8378127E+04	49.3946753E+03	49.6484353E+03
17.8295577E-03	26.5446798E-01	28.3981540E+03	16.8524688E-07	15.8378127E+04	49.3946753E+03	49.6484353E+03
17.8295577E-03	12.5149771E-01	26.8025311E+03	27.1741909E-07	14.9910212E+04	46.9260513E+03	47.0839520E+03
17.8295577E-03	10.5149772E-01	26.8025311E+03	27.1741909E-07	14.9910212E+04	46.9260513E+03	47.0839520E+03
S02	S01	S	S202	S201	S2	OMETD1
-16.8934447E-01	-42.9.27418E-63	97.6024531E-02	0.	0.	20.8292787E-03	82.6761011E-01
-25.13J2934E-01	12.6687542E-02	13.1045938E-01	0.	0.	20.8278917E-03	28.1954909E-01
-25.13J2934E-01	12.6687542E-02	13.1045938E-01	0.	0.	20.8278917E-03	28.1954909E-01
-25.13J2934E-01	18.7117176E-02	12.9197103E-01	0.	0.	20.7294346E-03	17.5445270E-01
-29.5313565E-01	18.7117176E-02	12.9197103E-01	0.	0.	20.7294346E-03	17.5445270E-01
FTR4	FTR0	FTRC	MTX	MTY	MTZ	FXH
-11.1301353E+04	85.4843755E-07	71.5593239E+04	86.8398960E-06	22.9831560E+05	21.2137189E-06	11.1301350E+04
FZM	LM	NH	NH			
-71.7088120E+04	86.8484234E-06	23.1150337E+05	21.2137189E-06			
VPQS						
19.7628520E+03						
TFFS						
-30.5756552E+04	-74.5058360E-10					
	-1.73725314E+04	-1.73725314E+04	-1.73725314E+04	-1.73725314E+04		
SAC1						
26.7000000E-02	26.7034306E-02	18.6902239E-03	82.2193821E-14	22.8949664E-14	56.8998091E-02	81.4934802E-14
AUTS						
DELQX	ALPHA	ALPHO1	ALPDO1	ALPHET	DELODE	
13.8566987E+00	78.1275532E-03	16.8404448E-01	0.	88.9361407E-03	77.4597584E-01	
PHIE	PHIET	DELPDE				
-11.3339811E-15	-10.8719796E-15	0.				

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE G-MOD STAGE 1 PAGE 307

NO(IIN) = -2.00000000E+00 -2.00000000E+00 -2.00000000E+00 -2.00000000E+00
TO(IIN) = 3.085330E+04 -2.10290850E+04 -2.10290850E+04 3.085330E+04
THROTTLE AUTOPILOT
CONTROL RESPONSE

DELQD1 DELRD1 DELPC1 DELQD DELRD DELPD
-25.0000000E+90 35.0000000E+00 60.0000000E+00 77.4597584E-01 15.0996644E-13 0.
NO1 = -1.25000000E-01 -1.25000000E-01 -1.25000000E-01 -1.25000000E-01
N = -1.79500000E+00 -1.79500000E+00 -1.79500000E+00 -1.79500000E+00
INTEG RTN: HT = 1.2300000E-02
INTEG RTN: HT = 6.3000000E-03

2SDF

22.613250E+00 22.613250E+00 43.3117E26E+02 34.922552E-11 18.9781952E+00 11.6692318E+01 -63.4409163E-12 -29.4048241E-02
-29.4752071E-14 18.9391896E-14 25.1053334E-14 10.4522904E-02 11.6692318E+01 16.1744923E+00 11.6692318E+01 44.5215872E-11
-13.5623690E-02 14.3177437E-12 31.1494492E-12 18.9459982E-01 41.9127939E-12 66.5912021E-03 21.8599488E-11 -77.7861410E-03
-0.
-0.

LGEAR

DELTA P P2 FT SR SF AA FC2
20.505254E-02 19.1262535E+04 38.1305350E+04 95.7437226E+03 -16.4046254E-01 -94.2062101E+03 32.9786231E+00 74.7803365E+03
27.3395074E-02 21.4141723E+04 34.9486843E+04 19.9221698E+04 -41.1699999E-01 -15.4749561E+04 33.8556554E+00 69.1786788E+03
27.3395074E-02 21.4141723E+04 34.9486843E+04 19.9221698E+04 -41.1699999E-01 -15.4749561E+04 33.8556554E+00 69.1786788E+03
26.377994E-02 20.4174960E+04 34.9470939E+04 19.9246595E+04 -48.2905777E-01 -14.7557504E+04 33.9837862E+00 74.2654253E+03
26.377994E-02 20.4174960E+04 34.9470939E+04 19.9246595E+04 -48.2905777E-01 -14.7557504E+04 33.9837862E+00 74.2654253E+03

HUVP

VG FT FTRX FTRY FTRZ NA HD DOELTA
39.113380E-04 22.8316730E-03 37.4501464E+01 -16.0531897E-07 -95.7433124E+03 64.6689022E+01 0. 28.505254E-02
18.1067064E-04 18.9472499E-01 -28.7637088E+03 19.9221698E+04 -41.1699999E-01 -15.4749561E+04 33.8556554E+00 69.1786788E+03
18.1067064E-04 18.9472499E-01 -28.7637088E+03 19.9221698E+04 -41.1699999E-01 -15.4749561E+04 33.8556554E+00 69.1786788E+03
18.1067064E-04 18.9472499E-01 -28.7637088E+03 19.9221698E+04 -41.1699999E-01 -15.4749561E+04 33.8556554E+00 69.1786788E+03
18.1067064E-04 18.9472499E-01 -28.7637088E+03 19.9221698E+04 -41.1699999E-01 -15.4749561E+04 33.8556554E+00 69.1786788E+03

S02

SD1 S S202 S2D1 S2 OMETD1 OMET
-83.5809762E-02 -11.4805749E-02 96.9731176E-02 0. 0. 20.8292767E-03 11.9757226E+00 -67.6167310E+00
-24.3935496E-01 -79.2431134E-03 13.1233046E-01 0. 0. 20.8278917E-03 85.5919277E-01 -66.5422845E+00
-24.3935496E-01 -79.2431134E-03 13.1233046E-01 0. 0. 20.8278917E-03 85.5919277E-01 -66.5422845E+00
-30.1924196E-01 -59.8654433E-03 12.9781731E-01 0. 0. 20.7294346E-03 78.5554267E-01 -66.1778234E+00
-30.1924196E-01 -59.8654433E-03 12.9781731E-01 0. 0. 20.7294346E-03 78.5554267E-01 -66.1778234E+00

FTRA

FTRD FTRC HTX HTY HTZ FXH FYN
-11.3052464E+04 83.6141508E-07 -71.8280249E+04 99.9308973E-06 -26.3551129E+05 87.4265802E-06 -11.3052464E+04 83.6141508E-07

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE G-MOD STAGE 1 PAGE 300

F2M LM HM NM
-71.9760243E+04 10.0708435E-05-26.4975100E+05 87.4265802E-06
VPCS
19.7628520E+03
TFFS
-30.7639839E+04 0.

T(1)
-1.74795358E+04 -1.74795358E+04 -1.74795358E+04 -1.74795358E+04

SAC1

26.7000000E-02 26.7851486E-02-36.3311515E-03 73.5126058E-14 12.4463220E-14 58.6029182E-02-82.0844847E-14

PITCH AUTOPILOT

AUTS
DELON ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
13.4666987E+00 78.1275532E-03-18.9859592E-01 0. 88.9311407E-03 76.6597584E-01

ROLL AUTOPILOT

PHIE PHRET DELPDE
-11.3339811E-15-10.8719796E-15 0.

NO(IN) = -2.00000000E+00 -2.00000000E+00 -2.00000000E+00 -2.00000000E+00
TO(IN) = 3.07772101E+04 -2.09529884E+04 -2.09529884E+04 3.07772101E+04
THROTTLE / AUTOPILOT
CONTROL RESPONSE

DELQD1 DELRD1 DELPD1 DELQD DELRD DELPD
-25.0000000E+00-35.0000000E+00 60.0000000E+00 76.6597584E-01 0. 0.

NC1 = -1.25000000E-01 -1.25000000E-01 -1.25000000E-01 -1.25000000E-01
N = -1.80500000E+00 -1.80500000E+00 -1.80500000E+00 -1.80500000E+00
INTEG RTN. HT = 6.0000000E-03
INTEG RTN. HT = 6.0000000E-03

2SDF

22.6932500E+00 22.6932500E+00 43.4047800E+02 38.6586023E-11 19.0006721E+00 11.5852307E+01-57.3755531E-12-55.8154100E-02

D-33

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(II)

[illegible]

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE G-MOD STAGE 1 PAGE 310

26.7200000E-02 26.8570614E-02-51.8296019E-03 66.9663819E-14 12.9719921E-15 58.8331616E-02-85.5820727E-14

AUTS

PITCH AUTOPILOT

DELON

ALPHA E

ALPHO1

ALPOD1

ALPHET

DELODE

13.8666987E+00 78.1275532E-03-12.7739117E-01 0.

88.9361407E-03 75.8597584E-01

ROLL AUTOPILOT

PHIE

PHIET

DELPDE

-11.3339811E-15-10.8719796E-15 0.

ND(IN) = -2.0000000E+00
TD(IN) = 3.0702052E+04

THROTTLE AUTOPILOT
-2.0000000E+00 -2.0000000E+00
-2.08778308E+04 -2.08778308E+04
CONTROL RESPONSE

-2.0000000E+00
3.0702052E+04

DELQD1

DELRD1

DELPD1

DELOD

DELRD

DELPD

-25.0000000E+00 35.0000000E+00 60.0000000E+00 75.8597584E-01 15.5430307E-13 0.

ND1 = -1.2500000E-01
N = -1.8150000E+00
HT = 3.0000000E-03
HT = 3.0000000E-03

-1.2500000E-01
-1.8150000E+00

-1.2500000E-01
-1.8150000E+00

-1.2500000E-01
-1.8150000E+00

INTEG RTN.
INTEG RTN.

HT =
HT =

D-35

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APPENDIX E

AIRPLANE B RIGID BODY EXAMPLE 2


```

1..0A8-2 * 1.4.2697E-3,8.8931664E-4
INDA8 1
ATA88 1 4.18951E-2,2.00844E-2
INDA10 1
ATA810 -3.978621E-2,-3.9658349E-2
INDA11 1
ATA811 5.7454448E-2,3.7645688E-2
INDA12 1
ATA812 1.472-279E-3,1.2354312E-3
INDA15 1
ATA815 -1.725E-2,-1.45E-2
INDA16 1
ATA816 1.25E-4,0.0E-5
INDA21 1
ATA821 7.3516484E-3,1.7-27972E-3
INDA52 1
ATA852 -5.2147852E-4,1.0238928E-3
INDA53 1
ATA853 -3.1368631E-4,1.8465268E-5
INDA56 1
ATA856 8.7E-3,7.3418182E-3
INDA57 1
ATA857 2.0E-5,3.6363636E-5
REM BCD 3ENGINE THRUST DATA
INTFFF 3
INDTSO 1
ITLX 4
ITAB10 -2.,-1.5,-1.,-.5,0.,.5,1.,1.5,2.
ITAB10 .,.,1.,.2,.3
ITAB10 0.,.,0.,.,0.,.
ITAB10 0.,.,0.,.,0.,.
ITAB10 0.,.,0.,.,0.,.
ITAB10 0.,.,0.,.,0.,.
ITAB10 0.,.,0.,.,0.,.
ITAB10 0.,.,0.,.,0.,.
ITAB10 0.,.,0.,.,0.,.
ITLW 9
REM BCD 3LANDING GEAR DATA
NSTRUT 3
MASS 4.94-16.,27.19587,27.19587
RX 35-18.3,-2.83867,-2.83867
RY 0.-8.333,+8.333
RZ 1.91657,.509583,.509583
THEIAD 0.,.,0.,.
ERDEG 0.
RGR 4.47
VTIRES 2.3,3.,3.
NZERO 1.54731E7,1.13125,1.13125
N 0.55407,.864107,.864107
DELTAH .198333,.198333,.198333
RLT 1.5-+3
IFD 1
AI 1.32-4533E+5,0.8129286E+5,3.8129286E+5
BI 1.212257,1.412391,1.412391
FTAB.2 2.,.,-1.5E+4,0.
FTAB.3 6.,.,0.,.,0.7,.336,.1,.336,.4,.336,1.,.336,1.0.,.336
MOMENT 1.2,2.6,2.0
MB 0.,.,0.,.
RF 5.40333,0.8792,0.8792
VZ 0.
PZERO 3528.,4.32.,4.32.
VZERO 0.1644580,.4716435,.4716435
A .11-4166-.2673611,.2673611

```

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E-4

1.0001	1	
NSMAIN	2	
CTAB.1	4.71.0067,1.72.73.	
CTAB.1	136.701,136.701,443.92,443.92,443.92,443.92	6
CTAB.1	4.73.32	13
INDC.2	1	
CTAB.2	4.71.0067,1.72.73.	
CTAB.2	136.701,136.701,4.23E+4,4.23E+4,4.23E+4,4.23E+4	6
CTAB.2	4.23E+4,4.23E+4	12
MUS	1.71.1	
SS	1.71.1	
SS	1.71.1	
REM	BCD 4FLEXIBLE AIRFRAME DATA	
INDFLX	BCD 3AUTPILOT DATA	
REM	BCD 3A. ENGINE DATA	
INDAUT	1	
IN	2	
ZN	1.50,1.50	
YN	14.1067,14.1067	
N	4.71.1	
REM	BCD 30. DRAG CHUTE DATA	
ICS	4.71.1	
COCH	1.244	
SSH	10.73	
XCH	9.025	
YCH	4.71.1	
ZCH	1.244	
REM	BCD 50. PHASE BEGIN-TERMINATE	
ITO	4.71.1	
IF	12.25	
NF	4.71.1	
XRF	8.790	
HRF	3.	
JELTAH	3.	
NLRI	4.71.1	
TI	4.71.1	
KP	4.71.1	
VS	1.71.1	
XS	3.000	
TS	12.	
HS	4.71.1	
REM	BCD 40. HOLD MANEUVER DATA	
ALPDES	11.5	
ITD	1.71.1	
KE	INT 1.71.1	
SM	11.5	
REM	BCD 50. LANDING ROLL MANEUVER DATA	
ISP	4.71.1	
TRV	4.71.1	
ICH	7.	
TBK	4.71.1	
ISS	4.71.1	
ILR	4.71.1	
IBS	4.71.1	
REM	BCD 51. ENGINE FAILURE STAGE DATA	
IC	INT 4.71.1	
XRF1	INT 4.71.1	
IT1	INT 4.71.1	
XRF2	INT 4.71.1	
IT2	INT 4.71.1	
H1	4.71.1	
IH1	INT 4.71.1	
P	4.71.1	

```

T 2      INT  0.0
S..1     INT  0.0
IHR1     INT  0.0
IHR2     INT  0.0
ITR1     INT  0.0
ITR2     INT  0.0
REM      BCD  5J. BRAKE COND.STAGE DATA
IB        INT  0.0
IBK1     INT  0.0
IBK2     INT  0.0
IBK2     INT  0.0
REM      BCD  4K. PITCH AUTOPILOT DATA
TST      0.0
ALPOL    0.0
RFALPH   0.0
DELALA    0.0
PSH       0.0
PSH2      0.0
RFALP2    0.0
DELOF     0.0
DELOTO    0.0
DELOL     0.0
DELOL     0.0
DELOL     0.0
DELOL     0.0
REM      BCD  4L. YAW AUTOPILOT DATA
RFB       0.0
DELSA     0.0
PSR       0.0
DPSIA     0.0
RFPPI     0.0
PSPPI     0.0
DELRLL    0.0
JELRU     0.0
REM      BCD  4M. ROLL AUTOPILOT DATA
RFPPI     0.0
OPHIA     0.0
PSA       0.0
DELPPL    0.0
DELPPL    0.0
REM      BCD  5N. THROTTLE AUTOPILOT DATA
TF        INT  0.0
NDF       INT  0.0
IR        INT  0.0
NR        0.0
NLR       0.0
NTO       0.0
K2        0.0
REM      BCD  4O. BRAKE AUTOPILOT DATA
MBC       0.0
PD        0.0
JELTAW    0.0
OHECD1    0.0
MBL       0.0
MBU       0.0
REM      BCD  5P. CONTROL RESPONSE DATA
DELSHS    0.0
DELRRO    0.0
JELLA     0.0
NED1      0.0
REM      BCD  4Q. INITIALIZATION
J-P       3

```

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F
L LQD      * 4.50478
DELQOE     4.50478
DELQON     4.50478
DELPD      .
DELRD      .
MANLOG      1
PITCHP     1
REM        BCD 3DATA PLOT TAPE
IPLT       .
REM        BCD 2STAGING DATA
REM        BCD 4A.GEARS INTO PROGRAM
INJLG      .
ISTAGE     .
DECR-S     BCD 1HR
STESTD     11.1
TRA        .
INDLG      -1
REM        BCD 40.SMOOTH IMPACT STAGE
AINCRS     BCD 30DELTA1DELTA2DELTA3
STEST      -1.5,-1.5,-1.5
TRA        .
PRINT      .2
DELTS      .15
AMAXER     .0005
PRTMIN     .
AINCRS     BCD 1TIMES
STEST      .9
TRA        .
ATAB51     7.35-8484E-3,-7.27972E-3
ATAB52     -5.2147852E-4,1.258928E-3
ATAB53     -3.1388631E-4,1.8765268E-3
ATAB56     .
ATAB57     .
REM        BCD 50.EFFICIENT AMAXER STAGE
AINCRS     BCD 40DELTA1DELTA2DELTA3
STEST      .1,.1,.1
TRA        .
PRINT      .5
AMAXER     .1
DELTS      .1
REM        BCD 40.SMOOTH IMPACT STAGE
AINCRS     BCD 10DELTA1
STEST      -1.5
TRA        .
PRINT      .5
DELTS      .15
AMAXER     .0005
REM        BCD 50.EFFICIENT AMAXER STAGE
AINCRS     BCD 10DELTA1
STEST      .1
TRA        .
PRINT      .5
AMAXER     .1
DELTS      .1
INDSTF     1
TRA        .

```

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 8

2SDF

0.	0.	0.	0.	13.000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	57.7454851E-01	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	10.3393988E+00
0.	0.	0.	0.	-31.6515539E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

TFFS

0. 0.

0.

0.

T(I)

SAC1

29.7745819E-03-20.8749533E-03 64.9750569E-02 0.

0.

15.3281676E-03 0.

FLARE

AUTS

ALPOES

PHIDES

TTO

11.5000000E+00 0.

0.

PITCH AUTOPILOT

DELQN

ALPHA8

ALPH01

ALPDD1

ALPHET

DELQDE

26.8544760E-01-14.0024531E-07 0.

0.

-14.0024531E-07 26.8544760E-01

INTEG RTN.

HT = 1.0530900E-03

2SDF

0.	0.	0.	0.	13.000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	96.1422983E-02	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	10.3393988E+00
0.	0.	0.	0.	-26.3312709E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

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E-7

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 9

TFFS

0. 0.

0. 0.

T(II)

SAC1

29.7745819E-03-20.8749533E-03 60.9750569E-02 0.

0. 15.3281670E-03 0.

AUTS

FLARE

ALPOES

PHIDES

TTO

11.5000000E+00 0.

0.

PITCH AUTOPILOT

DELON

ALPHA2

ALPH01

ALPDD1

ALPHET

DELODE

27.5617208E-01-14.0124531E-07 0.

0.

-14.0024531E-07 27.5607208E-01

STAGE ON--DECR. HR

11-00

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 10

INDLG ~1
REM BCD 48. SMOOTH IMPACT STAGE
AIRCDS BCD 300. DELT10DEL20DEL3
STEST TRA -.35, -.05, -.35

2SDF

0. 0. 0. 0. 10.0001000E+00 29.0274042E+31 0. 59.0569126E+00
59.9992281E-01 11.4999986E+30 26.5337670E-02 29.6220760E+01 10.4252977E+01 29.6199990E+01 0. 10.3393988E+00
0. 0. 0. 0. -26.3302709E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2800000E+03 0. 0. 31.9713310E-01-38.9549765E+12-78.0562277E+01 0.
0. 40.3200000E+03 0. 0. 54.9319200E-01-10.7799996E+03-39.6383699E+01 0.
0. 40.3200000E+03 0. 0. 54.9319200E-01-10.7799996E+03-39.6383699E+01 0.

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DDELTA

33.6000000E-02 29.6159999E+01 0. 0. -0. 0. 1. -79.6895154E-01
33.6000000E-02 29.6159999E+01 0. 0. -0. 0. 0. -18.9046626E-01
33.6000000E-02 29.6159999E+01 0. 0. -0. 0. 0. -18.9046626E-01

SD2

SD1

S

S2D2

S2D1

S2

ONETO1

ONET

0. 0. 0. 0. 0. 0. 1. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.

FTRA

FTRB

FTRC

MTX

MTY

MTZ

FXH

FYM

0. 0. 0. 0. 0. 0. 0. 0.

FZH

LH

NH

NH

0. 0. 0. 0.

VPCS

36.7489900E+02

TFFS

0. 0.

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E-9

INDSDF 2 CASE LROLL STAGE 1 PAGE 11

C. 3.

29.7745819E-03-20.8749533E-03 6L.9750569E-02 0. 0. 15.3281670E-03 0.

TED

11.534000E+00 G. G.

DELODE

27.5339224E-01-14.0124531E-07 L. 0. -14.0024531E-07 27.5339224E-01

[illegible]

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[illegible]

51.0030000E+03	51.0030000E+03	14.8031852E+00	0.	96.9255670E-01	29.0027316E+31	0.	59.3319920E+00
62.9389922E-01	27.2368959E-04	0.	26.5170101E-02	29.6034000E+01	10.4122497E+31	29.5967086E+01	0.
6.	11.56169.2E+00	0.	12.6453882E-01	0.	12.1824188E-31	0.	10.3434483E+00
6.	0.	94.7824236E-02	0.	-26.7931133E+00	12.4671000E+04	0.	0.

FC2

```

0.8562277E+01  0
0.6383699E+01  0
0.6383699E+01  0

```

DDelta

1. -76
2. -78
3. -78

DMET

၁၂၂

FYN

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

Q.	Q.	L.	Q.	Q.	Q.	Q.
FZN	LN	NH	NH			
Q.	Q.	L.	Q.			

VPCS
38.748990GE+12
TFFS
0.

SAC1

30.0142493E-03-21.9770289E-03 62.124650JE-32 0. 0. 12.2577406E-03 0.

ALPDES PHIDES TTD

11.500J:00E+03 0. 0.

PITCH AUTOPILOT

DELON	ALPHA	ALPHD1	ALPDD1	ALPHET	DELQDE
28.303635E-01	61.6902417E-03	12.6453882E-01	0.	61.6902417E-03	28.3036950E-01

[illegible]

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INDSDF 2 CASE LROLL STAGE 1 PAGE 14

[illegible]

2SDF

11.0000000E+00	11.0000000E+00	29.5966730E+00	0.	93.7100927E+01	28.9775565E+01	0.	59.6180378E+00
48.1984450E+04	48.1984450E+04	0.	26.5001399E+02	29.5844872E+01	10.3990476E+01	29.5772046E+01	0.
11.6257361E+00	11.6257361E+00	99.5793099E+02	12.9189599E+01	0.	-12.7133604E+01	0.	19.3544050E+00
0.	0.	0.	0.	-27.2600123E+00	12.4671000E+04	0.	0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

35.284714E+53	0.	31.184714E+31	38.95497656E+32	78.8562277E+61	0.
40.322100E+53	0.	44.779816E+61	10.77999966E+33	39.6383699E+11	0.
40.322100E+53	0.	44.77991906E+61	10.77999966E+33	39.6383699E+11	0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2		CASE LROLL	STAGE 1	PAGE 15			
NUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDelta
33.6030000E-02	29.5776739E+01	L.	0.	-0.	0.	0.	-73.4934807E-01
33.6030000E-02	29.5839538E+01	L.	0.	-0.	0.	0.	-46.1091723E-02
33.6030000E-02	29.5809538E+01	L.	0.	-0.	0.	0.	-46.1091723E-02
S02	S01	S	S202	S201	S2	OHETO1	OHET
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYM
0.	0.	0.	0.	0.	0.	0.	0.
FZH	LH	MH	NH				
0.	0.	0.	0.				
VPCS							
38.7489900E+02							
TFFS							
0.	0.						
	0.	0.					
SAC1							
30.2764715E-03	23.1185661E-03	63.3346129E-02	0.	0.	90.5478627E-04	0.	
AUTS							
ALPDES	PHIDES	TYD					
11.5033000E+00	0.	0.					
DELQN	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELQDE		
29.1245546E-01	12.5736266E-02	12.9189599E-01	0.	2.5736266E-02	29.1245546E-01		

FLARE

PITCH AUTOPILOT

E-14

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSO 2 CASE LROLL STAGE 1 PAGE 52

38.2996470E-01 21.1198847E-02 77.1641871E-01 0. 21.1198847E-02 42.3746470E-01

INTEG RTN. HT = 1.000000E-03
INTEG RTN. HT = 1.000000E-03
INTEG RTN. HT = 1.000000E-03
INTEG RTN. HT = 1.000000E-03

2SDF

62.1500110E-02 62.1511000E-02 18.2926421E+01 0. 72.9166610E-01 28.8828077E+01 0. 47.5733457E+00
-16.0212887E-01 93.9333334E-01 0. 26.2199268E-02 29.2719799E+01 10.1811329E+01 29.2715415E+01 0. 96.6689606E-01
0. 0. 61.8985338E-01 0. -47.8492989E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

11.6634853E-02 35.2881160E+03 0. 1.8849378E+03 -14.8347490E+01 -38.9549765E+12 -78.8562277E+31 0. 19.5666741E+03
11.6634853E-02 27.4996217E+04 0. 53.8849378E+03 -16.2392380E+01 -52.8120637E+33 39.4498903E+00 19.5666741E+03

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DDELTA

33.6093110E-02 29.2636254E+01 0. 0. 0. 0. 0. -48.3938674E-01
40.00934359E-03 24.7382237E-02 22.3466355E+02 0. -55.0417389E+03 22.6718941E+02 0. 11.6694853E-02
40.00934359E-03 24.7382237E-02 22.3466355E+02 0. -55.0417389E+03 22.6718941E+02 0. 11.6694853E-02

S02

S01

S

S202

S201

S2

OMETD1

OMET

-85.1643783E-01 -68.1124347E-02 15.1542118E-01 0. 0. 0. 0. 29.0665309E+01 -28.8523553E+01
-85.1643783E-01 -68.1124347E-02 15.1542118E-01 0. 0. 0. 0. 29.0665309E+01 -28.8523553E+01

FTRA

FTRB

FTRC

MTX

MTY

HTZ

FXH

FYH

22.8916655E+03 0. -10.7769876E+04 0. -16.6712311E+04 0. 22.8916655E+03 0.

FZH

LH

NH

NH

-10.8232559E+04 0. -16.8025716E+04 0.

VPCS

38.7489900E+12

TFFS

0. 0.

E-15

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 53

T(I)

SAC1

32.1641259E-03-66.0010496E-04 47.2288173E-02 0. 0. 17.6446850E-03 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1 ICS = 0

IBS = 1

TI

TR

17.1500000E-02 45.0000000E-02

PITCH AUTOPILOT

DELQIN

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

30.2996471E-01 21.1198847E-02-63.7143672E-01 0. 21.1198847E-02 43.4246470E-01

INTEG RTN. HT = 1.0000000E-03
INTEG PTN. HT = 1.0000000E-03
INTEG RTH. HT = 1.0000000E-03
INTEG RTH. HT = 1.0000000E-03

2SDF

64.2533000E-02 64.1500000E-02 18.8780351E-01 0. 73.2578161E-01 28.8885384E-01 0. 46.9996324E-03
-56.7441972E-03 26.2166936E-02 29.2683670E-01 10.1786094E-01 29.2677849E-01 0. 96.0208168E-01
-18.4582715E-01 92.4466722E-01 49.4226111E-01 0. -48.9187814E-01 0. 36.1341828E-02 0.
0. 0. 0. 0. 0. 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2850000E-03 0. 0. -85.8816724E-01-38.9549765E+02-78.8562277E+01 0. 29.3150118E+03
94.8781104E-03 25.9745872E+04 0. 40.1335917E+03-85.6141224E-01-39.2203852E+03 33.5790523E+00 29.3150118E+03
94.8781104E-03 25.9745872E+04 0. 40.1335917E+03-85.6141224E-01-39.2203852E+03 33.5790523E+03 29.3150118E+03

HUVP

VGPT

FTRX

FTRY

FTRZ

MA

MB

ODELTA

33.6000000E-02 29.2595892E+01 0. 0. -0. 0. 0. -48.3354383E-01
55.5735113E-03 33.8684567E-02 22.8352421E+02 0. -41.091553E+03 23.6658053E+02 0. 94.8781104E-03
55.5735113E-03 33.8684567E-02 22.8352421E+02 0. -41.091553E+03 23.6658053E+02 0. 94.8781104E-03

SD2

SD1

S

S2D2

S*01

S2

ONETD1

ONET

E-16

INDSUF 2 CASE LROLL STAGE 1 PAGE 54

FTRA	FTRU	FTRC	HTX	HTY	HTZ	FXM	FYM
------	------	------	-----	-----	-----	-----	-----

F7H LH HH NH

VPCS

TFES

3. 1.

SAC1

32.1313174E-03-57.5249362E-04 46.1927622E-02 0. 0. 19.1075466E-03 0.

AUTS

13

TR

17.150000E-12 47.000000E-02

ISS = 1

LANDING ROLL
ILR = 1

$$ICS = 0$$

IBS = 1

PITCH AUTOPILOT

DELOU

ALPHA E

ALPHE1

ALP001

ALPHET

DELOOE

30.2996475E-11 21.1198847E-12 48.3187814E-11 0.

21.1198847E-02 44.4746470E-01

```

INTEG RTN.      HT = 1.40000000E-03
INTEG RTN.      HT = 1.40000000E-03
INTEG RTN.      HT = 1.40000000E-03
INTEG RTN.      HT = 1.40000000E-03

```

250F

66.1500000E-02 66.1500000E-02 19.4633538E+01 0.

73.6387960E-01 28.8917405E+01 0.

46.5732413E+00

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INDSO 2 CASE LROLL STAGE 1 PAGE 55

0. -56.3810266E-03 0. 26.2134227E-02 29.2647115E+01 10.1763557E+01 29.2640683E+01 0. 95.3712275E-01
-19.4021516E-01 91.5725585E-01 0. -34.7744374E-01 0. 37.9867845E-02 0. 0. 0.
0. 0. 36.7432276E-01 0. -33.2755916E+00 12.4671000E+04 0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	35.2805044E+03	0.	1.	-27.3834214E-01	-38.9549765E+02	-78.8562277E+01	0.
72.344285E-03	24.3836493E+04	0.	27.2805706E+03	-14.5194675E-01	-26.5397426E+03	28.3435693E+00	38.0122258E+03
72.3414285E-03	24.3836493E+04	0.	27.2805706E+03	-14.5194675E-01	-26.5397426E+03	28.3435693E+00	38.0122258E+03

HUVP	VGPT	FTRX	FTRY	FTRZ	MA	MB	DDelta
33.6031613E-02	29.2556964E+01	0.	0.	-0.	0.	0.	-48.3107499E-01
74.6606221E-03	45.4873368E-02	21.9156627E+02	0.	-28.0143162E+03	22.1477955E+02	0.	72.3404285E-03
74.6606221E-03	45.4873368E-02	21.9156627E+02	0.	-28.0143162E+03	22.1477955E+02	0.	72.3404285E-03

S02	S01	S	S202	S201	S2	OMETO1	OMET
0.	0.	0.	0.	0.	0.	0.	0.
-48.3768316E-01	94.7963164E-02	14.7235858E-01	0.	0.	0.	28.3946096E+01	-27.6682641E+01
-48.3768316E-01	94.7963164E-02	14.7235858E-01	0.	0.	0.	28.3946096E+01	-27.6682641E+01

FTRA	FTRB	FTRC	MTX	MTY	MTZ	FXH	FYM
13.4085088E+03	0.	-54.5611413E+03	0.	-71.1212210E+03	0.	13.4085088E+03	0.

FZH	LK	HM	NH
-54.8242713E+03	0.	-71.8681603E+03	0.

VPCS

38.7489900E+02

TFFS

0. 0.

T(1)

111
111
111
SAC1
32.0946873E-03-50.7649859E-04 45.3767937E-02 0.

0. 20.4413987E-03 0.

ISS = 1

LANDING ROLL
ILR = 1 ICS = 0

IBS = 1

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 56

AUTS

TI

TR

17.1500000E-02 49.0000000E-02

PITCH AUTOPILOT

DELQX

ALPHA

ALP401

ALPDD1

ALPHET

DELQDE

30.2996470E-01 21.1198847E-02 -34.7744374E-01 0.

21.1198847E-02 45.5246470E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SDF

68.1500000E-02 68.1500000E-02 2.0000000E+01 0. 74.0251567E-01 28.8924877E+01 0. 46.2794317E+00
0. -55.4197867E-13 0. 26.2099116E-02 29.2607878E+01 10.1733157E+01 29.2601685E+01 0.
-19.0381842E-01 91.0022914E-01 0. -22.7281121E-01 0. -27.5096971E+00 12.4671000E+04 0. 94.7301595E-01
0. 0. 25.3995726E-01 0. 0. 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2800000E+03 0. 0. 21.1173660E-01 -38.9549765E+02 -78.8562277E+01 0.
51.2003347E-03 22.8333476E+04 0. 16.6723350E+03 43.3454560E-01 -16.0115882E+03 24.2958507E+00 44.5810024E+03
51.2003347E-03 22.8333476E+04 0. 16.6723350E+03 43.3454560E-01 -16.0115882E+03 24.2958507E+00 44.5810024E+03

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DDELTA

33.6600000E-02 29.2517171E+01 0. 0. -0. 0. 0. -44.2962490E-01
10.1372763E-02 61.7571865E-02 17.4296928E+02 0. -17.1936644E+03 18.8249339E+02 0. 51.2003347E-03
10.1372763E-02 61.7571865E-02 17.4296928E+02 0. -17.1936644E+03 18.8249339E+02 0. 51.2003347E-03

SD2

SD1

S

S2D2

S2D1

S2

OHETD1

OHET

0. 0. 0. 0. 0. 0. 0.
-30.4485408E-01 -16.266821E-01 14.5256316E-01 0. 0. 0. 24.1345306E+01 -27.1318846E+01
-30.4485408E-01 -16.266821E-01 14.5256316E-01 0. 0. 0. 24.1345306E+01 -27.1318846E+01

FTRA

FTRB

FTRC

MTX

MTY

MTZ

FXH

FYH

90.9797430E+02 0. -33.3446700E+03 0. -36.8819522E+03 0. 90.9797430E+02 0.

FZH

LH

NH

NH

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 57

-33.5102850E+03 0.

-37.3520783E+03 0.

VPOS

38.7489900E+02

TFFS

0.

0.

0.

0.

T(I)

SAC1

32.0569960E-03-45.4768223E-04 44.7596670E-02 0.

0.

21.6559792E-03 0.

LANDING ROLL

ISS = 1

ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

17.1503000E-02 51.9300000E-02

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHO1

ALPDD1

ALPHET

DELQDE

30.2996470E-01 21.1198847E-02-22.7281121E-01 0.

21.1198847E-02 46.5746470E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SDF

70.1500000E-02 70.1500000E-02 20.6337583E+01 0. 74.3935200E-01 28.8911102E+01 0. 46.8925942E+00
0. -54.5139400E-03 0. 26.2966547E-02 29.2564783E+01 10.1763083E+01 29.2559456E+01 0.
-17.6551425E-01 90.6452210E-01 0. -13.5175249E-01 0. 34.5760876E-02 0. 94.1828191E-01
0. 0. 16.2516449E-01 0. -23.3645572E+00 12.4671800E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2810000E+03 0. 0. 56.7422524E-01-38.9549765E+02-78.8562277E+01 0.
33.1126455E-03 21.3892458E+04 0. 09.5115729E+02 86.5603277E-01-83.6305250E+02 21.6247831E+03 48.5423373E+03

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 58

33.1126455E-03 21.3892458E+04 1. 89.5115729E+02 86.5803277E-01-83.6305250E+02 21.6247831E+00 48.5423373E+03

HUVP	VGPI	FTRX	FTRY	FTRZ	MA	MB	ODELTA
33.6140100E-02	29.2474972E+01	0.	0.	-92.9036134E+02	0.	0.	-48.2724322E-01
14.1011891E-02	85.8913116E-02	13.995814E+02	0.	-92.9036134E+02	14.3851396E+02	0.	33.1126455E-03
14.1011891E-02	85.8913116E-02	13.995814E+02	0.	-92.9036134E+02	14.3851396E+02	0.	33.1126455E-03

SQ2	SD1	S	S2D2	S2D1	S2	OHETD1	OHET
-14.5821334E-01	10.7124833E-01	14.3153172E-01	0.	0.	0.	0.	18.4424867E+01-26.7044031E+01
-14.5821334E-01	10.7124833E-01	14.3153172E-01	0.	0.	0.	0.	18.4424867E+01-26.7044031E+01

FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYH
56.2266358E+02	0.	-17.9023146E+03	0.	-14.4461157E+03	0.	56.2266358E+02	0.

FZM	LH	NH	NH
-17.9816293E+03	0.	-14.6712641E+03	0.

VPCS
38.7489900E+02
TFFS
L. G.

SAC1
32.0236535E-03-41.3324883E-04 44.3042398E-02 0.
G. 22.7760654E-03 0.

AUTS
TI TR
17.1501000E-02 53.000000E-02
ISS = 1 LANDING ROLL ICS = 0 IBS = 1
ILR = 1

PITCH AUTOPILOT
OELON ALPHAE ALPHD1 ALPDD1 ALPHET OELQDE
30.2996470E-01 21.1198847E-02-13.5079249E-01 0. 21.1198847E-02 47.6246470E-01

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 59

INTEG RTN. HT = 1.0000000E-13
INTEG RTN. HT = 1.0000000E-13
INTEG RTN. HT = 1.0000000E-13
INTEG RTN. HT = 1.0000000E-13

2SDF

72.153000E-02 72.153000E-12 21.2188318E+01 J. 74.7265955E-01 28.8880558E+11 0. 45.9834023E+00
-15.5714373E-01 -52.3063913E-13 0. 26.2318167E-02 29.2517436E+01 10.1670069E+01 29.2513291E+01 0.
-15.5714373E-01 90.4434425E-11 0. -71.6214438E-02 0. 30.502628E-02 0. 93.4934550E-01
J. 0. 0. -20.6364372E+00 12.4671000E+04 0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FG2
0.	35.2830010E+03	0.	0.	79.5181651E-01	-38.9549765E+12	-78.8562277E+01	0.
19.1875434E-03	20.0831828E+04	0.	41.0306337E+12	11.3638999E+01	-35.5363599E+12	20.2026138E+00	49.9870374E+03
19.1875434E-03	20.0831828E+04	0.	41.0306337E+02	11.3638999E+01	-35.5363599E+12	20.2026138E+00	49.9870374E+03

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.603000E-02	29.2429451E+01	0.	0.	-42.9886484E+02	94.7971475E+01	0.	-48.2246445E-01
19.8305016E-02	12.0707251E-01	85.2443556E+01	0.	-42.9886484E+02	94.7971475E+01	0.	19.1875433E-03
19.8305016E-02	12.0707251E-01	85.2443556E+01	0.	-42.9886484E+02	94.7971475E+01	0.	19.1875433E-03

SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
0.	0.	0.	0.	0.	0.	0.	0.
-18.0102415E-02	-18.0707251E-01	14.0990592E-01	0.	0.	0.	12.1534676E+01	-26.3982494E+01
-18.0102415E-02	-18.0707251E-01	14.0990592E-01	0.	0.	0.	12.1534676E+01	-26.3982494E+01

FTRA	FTRB	FTRC	MTX	MTY	MTZ	FXM	FYM
30.7890223E+02	0.	-82.0612675E+02	0.	-29.9016680E+02	0.	30.7890223E+02	0.
30.7890223E+02	0.	-82.0612675E+02	0.	-29.9016680E+02	0.	30.7890223E+02	0.

FZH	LM	HM	NH
-82.1592283E+02	0.	-30.1797473E+02	0.
-82.1592283E+02	0.	-30.1797473E+02	0.

VPCS

38.7489900E+02

TFFS

0. 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 60

T(I)

SAC1
31.9814616E-33-37.9918838E-34 43.967967JE-32 J. 23.8223836E-33 3.

AUTS ISS = 1 LANDING ROLL ILR = 1 ICS = 0 IBS = 1

TI TR
17.1530000E-02 55.000000E-02

PITCH AUTOPILOT

DELQX ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
30.2996473E-01 21.1198847E-02-71.6214438E-02 0. 21.1198847E-02 48.6746470E-01

INTEG RTN. HT = 1.0433333E-33
INTEG RTN. HT = 1.0433333E-33
INTEG RTN. HT = 1.0433333E-33
INTEG RTN. HT = 1.0433333E-33

2SDF

74.1530330E-02 74.1500000E-02 21.8334689E-01 0. 75.5136348E-01 28.8837917E-01 0. 45.9248716E-00
0. -52.4326358E-13 L. 26.1972235E-02 24.2466129E-01 10.1634321E-01 29.2463206E-01 0.
-13.6744330E-01 96.3433349E-11 L. -32.3204996E-12 0. 25.6136204E-12 0. 92.9046934E-01
0. 52.1939216E-02 0. -19.234008E-00 12.4671000E-04 0.

LGEAR

DELTA	P	P2	FT	SX	SF	AA	FC2
35.2810000E+03	0.	0.	91.508318E-01	-38.9549765E+02	-78.8562277E+01	0.	0.
10.0368445E-03	18.9231636E+04	0.	16.2546709E+02	12.7926022E+00	-10.9525040E+02	19.6800726E+00	49.4304800E+03
10.0368445E-03	18.9231636E+04	0.	16.2546709E+02	12.7926022E+00	-10.9525040E+02	19.6800726E+00	49.4304800E+03

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.6303000E-02	29.2385000E+01	0.	0.	-0.	0.	0.	-48.1435182E-01
26.2940182E-02	16.1133227E-01	45.2561406E+01	0.	-17.2110490E+02	53.7418146E+11	0.	10.0360845E-03
26.2940182E-02	16.1133227E-01	45.2561406E+01	0.	-17.2110490E+02	53.7418146E+11	0.	10.0360845E-03

SQ2	SQ1	S	S202	S201	S2	OMETD1	OMET

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E-23

E-24

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22

3.

T(II)

SAC1

31.9506005E-03-35,15766L1E-04 43.7115696E-02 0.

0.

24.8181620E-03 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1 ICS = 0

IPS = 1

II

TR

17.1530000E-02 57.0000000E-02

PITCH AUTOPILOT

DELOH

ALPHA

ALPH01

ALPBB1

ALPHET

DELODE

3C.299647J-E-01 21.1198847L-02-32.3234096E-02 0.

21.1198847E-02 49.7246473E-01

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 144

INTEG RTN. HT = 1.0000000E+03
INTEG RTN. HT = 1.0000000E+03
INTEG RTN. HT = 1.0000000E+03
INTEG RTN. HT = 1.0000000E+03

2SOF

29.5675000E-01 20.5675000E-01 6.776061E+01 1. 69.9552454E-01 28.9899030E+01 0. 67.7620672E-01
0. -18.9920053E-02 25.9743277E-02 28.9978222E+01 99.9140191E+00 28.9978171E+01 0.
17.1763950E-02 13.3908603E-01 13.6071246E+00 0. -33.9379903E-03 0. 13.0507056E-01
0. 0. -13.7092696E-01 0. -30.8253423E+00 12.4671000E+04 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

82.603649E-03 57.751129E+03 0. 12.9768983E+03 -17.8521723E-01 -12.8344942E+03 28.8267336E+00 -69.5445122E+02
12.5156996E-02 23.5831491E+04 0. 60.7423223E+03 15.6931214E-01 -59.9171756E+03 39.7122598E+00 29.8851747E+02
12.5156996E-02 23.5831491E+04 0. 60.7423223E+03 15.6931214E-01 -59.9171756E+03 39.7122598E+00 29.8851747E+02

MUVP

VGPT

FTRX

FTRY

FTRZ

MA

MB

BDELTA

33.6030000E-02 15.2496453E+01 -43.2823799E+02 0. -12.8816627E+03 -41.7812113E+02 0. 82.603649E-03
29.9322238E-04 18.1121342E-03 18.1874856E+01 0. -60.7622265E+03 18.2983021E+01 0. 12.5156996E-02
29.9322238E-04 18.1121342E-03 18.1874856E+01 0. -60.7622265E+03 18.2983021E+01 0. 12.5156996E-02

SD2

SD1

S

S2D2

S2D1

S2

OMETD1

OMET

-51.2513826E-01 66.5311695E-01 56.8969582E-02 0. 0. 0. -17.4188339E+02 -14.1077993E+01
11.5917841E-02 -26.5801976E-02 14.6246717E-01 0. 0. 0. 23.4593616E+00 -28.7115329E+01
11.5917841E-02 -26.5801976E-02 14.6246717E-01 0. 0. 0. 23.4593616E+00 -28.7115329E+01

FTRA

FTRB

FTRC

HTX

HTY

HTZ

FXH

FYM

-90.2251954E+01 0. -13.4461543E+04 0. 97.6090453E+03 0. -90.2251954E+01 0.

FZH

LH

NH

NH

-13.4403556E+04 0. 90.5151884E+03 0.

VPCS

38.7489930E+02

TFFS

0. 0.

E-25

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 145

T(I)

0.

SAC1

32.4484639E-03 27.4792202E-03-93.7615814E-03 0. 0. 67.2563621E-04 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1 ICS = 0

IBS = 1

TI

TR

17.1500030E-02 18.8525000E-01

PITCH AUTOPILOT

DELQN

ALPHA E

ALPDD1

ALPDD1

ALPHET

DELQDE

30.2996470E-01 21.1198847E-02-16.6071245E+00 0. 21.1198847E-02 80.0000000E-01

INTEG RYN. HT = 1.0000000E-03
INTEG RYN. HT = 1.0000000E-03
INTEG RYN. HT = 1.0000000E-03
INTEG RYN. HT = 1.0000000E-03

2SDF

28.767500E-01 21.767500E-01 60.657520E+01 0. 69.9170297E+01 28.9879068E+01 0. 57.1445327E-01
0. -16.7974699E-02 0. 25.9704906E-02 28.9935388E+01 99.8845148E+00 28.9935314E+01 0.
20.6593048E-02 11.2933871E-01 0. -16.4628314E-01 -16.3652437E+00 0. -48.8259327E-03 19.8851268E-01
0. 0. -30.1634212E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

87.5317049E-03 67.7614288E+03 0. 13.9047113E+03-18.5902022E-01-13.7686293E+03 27.5469678E+00-58.4866232E+02
12.3908426E-02 23.1798200E+04 0. 99.8933443E+03 22.9391545E-01-59.0595066E+03 30.6634545E+00 27.8828085E+02
12.3936426E-02 23.1798200E+04 0. 99.8933443E+03 22.9391545E-01-59.0595066E+03 30.6634545E+00 27.8828085E+02

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

ODELTA

33.601100E-02 11.8682083E+01-46.4318353E+02 0. -13.8189986E+03-44.5924379E+02 0. 87.5317049E-03
20.4493257E-04 12.3143280E-01 12.3143280E-01 0. -59.9064822E+03 12.3404339E+01 0. 12.3908426E-02
20.4493257E-04 12.3143280E-01 12.3143280E-01 0. -59.9064822E+03 12.3404339E+01 0. 12.3908426E-02

S02

S01

S

S2D2

S2D1

S2

OMETD1

OMET

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 146

-64.8024632E-01 65.3966097E-01 76.1936113E-02 0. 0. 0. -18.5801825E+02 -17.7897412E+01
78.6176072E-02 -25.6742682E-02 14.5721938E-01 0. 0. 0. 15.8210691E+00 -28.6722012E+01
78.6176372E-02 -25.6742682E-02 14.5721938E-01 0. 0. 0. 15.8210691E+00 -28.6722012E+01

FTRA FTRB FTRC HTX HTY HTZ FXM FYH

-18.5877569E+02 0. -13.3691400E+04 0. 12.9188881E+04 0. -18.5877569E+02 0.

FZH LH MM NM

-13.3681651E+04 0. 13.3433368E+04 0.

VPCS
38.7489900E+02
TFFS
0. 0.

0. 0. T(I)

SAG1
32.4520715E-03 28.1975723E-03 -10.4797977E-02 0. 0. 70.1303410E-04 0.

AUTS ISS = 1 LANDING ROLL ILR = 1 ICS = 0 IBS = 1

TI TR
17.1500000E-02 19.1925000E-01

PITCH AUTOPILOT

DELON ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE

34.2996476E-01 21.1198847E-02 -10.3652437E+00 0. 21.1198847E-02 80.0000000E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SDF

20.9875000E-01 20.9875000E-01 61.2373452E+01 0. 69.8719246E-01 28.9851586E+01 0. 46.7573928E-01
0. -18.5549888E-02 0. 25.9663617E-02 28.9889297E+01 99.8527735E+00 28.9889188E+01 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 147

25.1659598E-02 92.4186398E-02 0. -10.1550057E+00 0. -49.7388831E-03 0. 87.4446601E-02
0. 0. -19.4536533E-01 0. -29.7994813E+00 12.4671000E+04 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
94.2813891E-13	81.6260410E+33	0.	15.1957589E+03	-24.5424104E-01	-15.0713106E+03	25.1933505E+00	-55.7346301E+02
12.313515E-12	22.81238JE+34	0.	59.472902E+33	27.3785850E-01	-58.5682102E+03	30.8535809E+00	23.2753274E+02
12.3186150E-02	22.81238JE+34	0.	59.4072902E+03	27.3785850E-01	-58.5682102E+03	30.8535809E+00	23.2753274E+02

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.631130E-12	82.9859781E+34	-5.8031559E+02	0.	-15.1199872E+03	-48.4476843E+12	0.	94.2813891E-03
11.1524635E-14	67.0967849E-04	66.2626385E+00	0.	-59.4152210E+03	66.7969433E+00	0.	12.3186150E-02
11.1524635E-04	67.0967849E-04	66.2626385E+00	0.	-59.4152210E+03	66.7969433E+00	0.	12.3186150E-02

SD2	SU1	S	S2D2	S2D1	S2	OMETD1	OMET
-94.3414351E-01	63.8335494E-01	83.258169E-12	0.	0.	0.	-20.1865351E+02	-21.5686502E+01
14.2118644E-01	23.4572834E-02	14.5228534E-01	0.	0.	0.	85.6371029E-01	-28.6479919E+01
14.2118644E-01	23.4572834E-02	14.5228534E-01	0.	0.	0.	85.6371029E-01	-28.6479919E+01

FTRA	FTRG	FTRC	MTX	MTY	MTZ	FXH	FYH
-29.0234587E+02	0.	-13.4010339E+04	0.	17.0826895E+04	0.	-29.0294587E+02	0.

FZH	LH	NH	NH
-13.3973643E+04	0.	17.2681372E+04	0.

VPCS

38.7489902E+02

TFFS

0. 0.

T(I)

SAC1		
82.4564369E-03	28.9223312E-03	-11.5485887E-02 0.
		0. 72.7100934E-04 0.

AUTS

ISS = 1

ILR = 1 LANDING ROLL

IGS = 0

IBS = 1

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 148

TI TR
17.1530000E-02 19.2525000E-01

PITCH AUTORILCT

DELQN ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
30.2996473E-01 21.1198847E-02 10.1550657E+00 0. 21.1198847E-02 80.0000000E-01
INTEG RTN. HT = 1.000000E-03
INTEG RTN. HT = 1.000000E-03
INTEG RTN. HT = 1.000000E-03

2SDF

21.9975000E-01 21.5975000E-01 61.6141805E+01 0. 69.8371474E-01 28.9829473E+01 0. 40.1149358E-01
28.3545670E-02 79.2973105E-02 0. 25.9634093E-02 28.9857233E+01 99.8306962E+00 28.9857095E+01 0.
0. 0. -21.5743958E-01 0. -29.7357206E+00 12.4671060E+04 0. 73.6932823E-02
0. 0. 0. 0. 0. 0. 0.

LGEAR

DELTA P P2 FT SR SF AA FC2
10.0079198E-02 93.8139792E+03 0. 16.3222778E+03 -31.9724318E-01 -16.2106409E+03 22.5985759E+00 -53.2685612E+02
12.2971190E-02 22.8141270E+04 0. 59.2627943E+03 28.6897074E-01 -58.4171234E+03 31.0954190E+00 19.3042667E+02
12.2971190E-02 22.8141270E+04 0. 59.2627943E+03 28.6897074E-01 -58.4171234E+03 31.0954190E+00 19.3042667E+02

HUVP VGPT FTRX FTRY FTRZ MA HB ODELTA
33.6030000E-02 58.5412251E+00 -54.6113686E+02 0. -16.2533435E+03 -51.7627032E+02 0. 10.0079198E-02
60.8743000E-02 36.6212833E-04 36.6790764E+00 0. -59.2681566E+03 36.3778043E+00 0. 12.2971190E-02
60.8743000E-02 36.6212833E-04 36.6790764E+00 0. -59.2681566E+03 36.3778043E+00 0. 12.2971190E-02

S02 S01 S S202 S201 S2 OMETD1 OMET
-12.7701060E+00 62.4546100E-01 91.2360547E-02 0. 0. 0. -21.5677930E+02 -24.2791799E+01
17.9345000E-01 -21.3627162E-02 14.4936649E-01 0. 0. 0. 46.6382106E-01 -28.6394875E+01
17.9345000E-01 -21.3627162E-02 14.4936649E-01 0. 0. 0. 46.6382106E-01 -28.6394875E+01

FTRA FTRB FTRC MTX HTY MTZ FXH FYH
-36.5492862E+02 0. -13.4847859E+04 0. 26.6493632E+04 0. -36.5492862E+02 0.

FZH LH MH NM
-13.4813415E+04 0. 21.8983668E+04 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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VPCS

38.7489900E+02

TFFS

0.

0.

0.

0.

T(I)

SAC1

32.4603187E-03 29.3984428E-03-12.2264911E-02 0.

0.

74.3099679E-04 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1500000E-02 19.3825000E-01

PITCH AUTOPILOT

DELON

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

30.2996475E-01 21.1198847E-02-10.1334587E+03 0.

21.1198847E-02 80.0000000E-01

STAGE ON--INCR. DELTA1

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 150

PRINT
AMAXER
DELTS
INOSTF
TRA

.05
.01
.01
1

2SDF

21.097500E+01 21.097500E+01 61.614183E+01 0. 69.837147E+01 28.982947E+01 0. 40.114935E+01
0. -18.384906E+01 25.963489E+02 28.985723E+01 99.830696E+00 28.985709E+01 0.
26.353567E+02 79.297313E+02 -10.033407E+00 0. -56.039392E+03 0. 73.693282E+02
0. 0. -21.574395E+01 0. -29.735726E+00 12.467100E+04 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
10.007919E+02	93.813979E+03	0.	16.322277E+03	-31.972431E+01	-16.216640E+03	22.598575E+00	-53.268561E+02
12.297199E+02	22.601412E+04	0.	59.262791E+03	28.689707E+01	-58.417123E+03	31.095419E+00	19.304266E+02
12.237199E+02	22.601412E+04	0.	59.262791E+03	28.689707E+01	-58.417123E+03	31.095419E+00	19.304266E+02

NUVP	VGPT	FTRX	FTRY	FIRZ	MA	NB	ODELTA
33.601100E+02	58.541225E+03	-54.611368E+02	0.	-16.253383E+03	-51.762703E+02	0.	10.007919E+02
60.874301E+02	36.621283E+04	36.679176E+00	0.	-59.268156E+03	36.377804E+00	0.	12.297199E+02
60.874301E+02	36.621283E+04	36.679176E+00	0.	-59.268156E+03	36.377804E+00	0.	12.297199E+02

S02	S01	S	S202	S201	S2	OHETD1	OHET
-12.773586E+00	62.405461E+01	91.236354E+02	0.	0.	0.	-21.567793E+02	-24.278179E+01
17.933582E+01	-21.362716E+02	14.493664E+01	0.	0.	0.	46.639210E+01	-28.639487E+01
17.933582E+01	-21.362716E+02	14.493664E+01	0.	0.	0.	46.639210E+01	-28.639487E+01

FTRA	FTRB	FTRC	MTX	MTY	HTZ	FXH	FYM
-36.549286E+02	0.	-13.484785E+04	0.	20.649363E+04	0.	-36.549286E+02	0.

FZH	LH	NH	NH
-13.481341E+04	0.	20.898366E+04	0.

VPCS

38.748990E+02

TFFS

0. 0.

E-31

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 151

T(I)

SAC1

32.4603187E-03 29.398428E-03-12.2264911E-02 0.

0.

74.3099679E-04 0.

AUTS

ISS = 1

ILR = 1 LANDING ROLL ICS = 0

IBS = 1

TI

TR

17.1500000E-02 19.3825000E-01

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHD1

ALPOD1

ALPHET

DELQDE

30.2996470E-01 21.1198847E-02-16.334087E+00 0.

21.1198847E-02 80.0000000E-01

INTEG RTN. HT = 8.0000000E-03
INTEG RTN. HT = 8.0000000E-03
INTEG RTN. HT = 8.0000000E-03
INTEG RTN. HT = 8.0000000E-03
INTEG RTN. HT = 8.0000000E-03

2SDF

21.5975000E-01 21.5975000E-01 63.2631559E+01 0. 69.6671216E-01 28.9742858E+01 0. 15.2774539E-01
-17.1428822E-02 L. 25.9536136E-12 28.9746885E+01 99.7547497E+00 28.9746628E+01 0.
38.6117223E-02 20.2184261E-02 L. -95.9584974E-01 0. -76.3504194E-03 0. 22.5753757E-02
0. 0. -15.3373938E-01 0. -31.6411855E+00 12.4671000E+04 0.
0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FG2

14.2748595E-02 19.6835899E+04 L. 24.9945052E+03-11.9077334E+04-25.0572254E+03-12.6964138E+00-31.8826156E+02
12.3095817E-02 22.0409122E+04 L. 59.3532927E+03 21.6826018E-01-58.4734584E+03 32.3520563E+00 43.3517893E+01
12.3095817E-02 22.0409122E+04 L. 59.3532927E+03 21.6826018E-01-58.4734584E+03 32.3520563E+00 43.3517893E+01

HUVP

VGPT

FTRX

FTRY

FTRZ

MA

NB

DELTA

57.9696255E-03 34.8649233E-02-14.4860248E+02 0. -24.9889914E+03-13.1122876E+02 0. 14.2748595E-02
25.7627953E-03 15.4966197E-04-15.2811713E+03 0. -59.3536932E+03-15.4158975E+00 0. 12.3095817E-02
25.7627953E-03 15.4966197E-04-15.2811713E+03 0. -59.3536932E+03-15.4158975E+00 0. 12.3095817E-02

S02

S01

S

S202

S201

S2

OHETD1

OHET

E-32

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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-56.7778974E+01 48.2796468E-01 12.0017484E-01 J. 0. 0. -54.6345316E+01 -31.8548379E+01
23.4656614E-01 -10.1235616E-02 14.4136351E-01 0. 0. -19.7639199E-01 -28.6388743E+01
23.4656614E-01 -10.1235616E-02 14.4136351E-01 0. 0. -19.7639199E-01 -28.6388743E+01

FTRA FTRB FTRC HTX HTY HTZ FXH FYH
-91.2990043E+01 0. -14.3701091E+04 0. 53.2808124E+04 0. -91.2990043E+01 0.

FZH LH HM NH
-14.3853940E+04 0. 54.3613697E+04 0.

VPCS
38.7489900E+02

TFFS
0. 0.

T(I)

SAC1
32.4744315E-03 31.2633643E-03 -14.7236739E-02 0. 0. 79.6697768E-04 0.

AUTS ISS = 1 LANDING ROLL ILS = 0 IBS = 1
TI TR

17.1500300E-02 19.8825000E-01

PITCH AUTOPILOT

DELQX ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
30.2996470E-01 21.1198847E-02 -95.9584973E-01 0. 21.1198847E-02 80.0000000E-01
INTEG RTN. HT = 4.0000000E-03
INTEG RTN. HT = 2.0000000E-03
INTEG RTN. HT = 2.0000000E-03 TIRE DEFLECTION EXCEEDED DELTA(1) = 1.9992265E-01

2SOF

21.8575000E-01 21.8575000E-01 63.8164365E+01 J. 69.5654273E-01 28.9697775E+01 0. 27.7881913E-02
0. -15.8695247E-02 0. 25.9492156E-02 28.9697918E+01 99.7211584E+08 28.9697657E+01 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 153

38.4155056E-02 54.9588080E-03 0. -21.5703210E-01 0. -94.2329996E-01 0. -75.9762512E-03 0. -21.0184683E-03 0.
0. 0. 0. 0. 0. 0. 0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
19.9922651E-02	32.0249699E+04	0.	36.9345486E+03	-23.4946757E+04	-36.9569574E+03	-65.6050140E-01	-12.0921624E+02
12.3653383E-02	21.9113897E+04	0.	59.3288822E+03	27.1577958E-02	-58.4436179E+03	32.5517919E+00	13.8306244E+01
12.3059383E-02	21.9113897E+04	0.	59.3288822E+03	27.1577958E-02	-58.4436179E+03	32.5517919E+00	13.8306244E+01

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
85.5803838E-03	51.4777783E-02	-31.6091797E+02	0.	-36.9352153E+03	-26.8439636E+02	0.	19.9922651E-02
10.3285636E-03	62.1332077E-05	61.2782133E-01	0.	-59.3288823E+03	61.7801197E-01	0.	12.3653383E-02
10.3285636E-03	62.1332077E-05	61.2782133E-01	0.	-59.3288823E+03	61.7801197E-01	0.	12.3059383E-02

SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
-62.2291764E+01	30.7182146E-01	13.1432799E-01	0.	0.	0.	-11.1684984E+02	-33.9866216E+01
64.9373222E-02	-57.1886366E-03	14.3939819E-01	0.	0.	0.	79.2052816E-02	-28.6406834E+01
64.9373222E-02	-57.1886366E-03	14.3939819E-01	0.	0.	0.	79.2052816E-02	-28.6406834E+01

FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYM
-32.0574011E+02	0.	-15.5591806E+04	0.	93.6880372E+04	0.	-32.0574011E+02	0.

FZN	LM	NM	NH
-15.5863898E+04	0.	94.7765666E+04	0.

VPCS

38.7489900E+02

TFFS

0. 0.

T(I)

SAC1

32.4861312E-03 32.2614879E-03 -15.9583011E-02 0. 0. 82.0270827E-04 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 154

TI TR
17.1500000E-02 20.1425000E-01

PITCH AUTOPILOT

DELQN ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
30.2996470E-01 21.1198847E-02 94.2329996E-01 0. 21.1198847E-02 80.0000000E-01

STOP

ORIGINAL PAGE IS
OF POOR QUALITY

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APPENDIX F

AIRPLANE B FLEXIBLE BODY EXAMPLE 3

STAGE	TAB	NUM
ATAB1	2	1
ATAB9	2	2
ATAB8	0	3
ATAB1	6	4
ATAB1	1	5
ATAB1	2	6
ATAB1	5	7
ATAB1	6	8
ATAB5	2	9
ATAB5	2	10
ATAB5	3	11
ATAB5	5	12
ATAB5	7	13
CTAB1	1	14
CTAB1	2	15
CTAB1	3	16
FTTAB	10	17
VTAB1	1	18
VTAB1	2	19
VTAB1	3	20
VTAB1	4	21
VTAB1	6	22

BCD 5VEHICLE PHYSICAL PROP. DATA

BCD 4AERODYNAMIC INPUT DATA

1
1005.
37.7
56.7
1
-7.9573427E-3,-5.5941985E-3

FN

ATAB12 1.4020979E-3,8.8931664E-4
 INDA12 1
 INDA83 1
 ATAB85 4.18351E-2,2.03844E-2
 INDA10 1
 ATAB10 -3.978321E-2,-3.9650349E-2
 INDA11 1
 ATAB11 5.7452448E-2,3.7645688E-2
 INDA12 1
 ATAB12 1.4720279E-3,1.2354312E-3
 INDA15 1
 ATAB15 -1.725E-2,-1.45E-2
 INDA16 1
 ATAB16 1.25E-4,5.6E-5
 INDA51 1
 ATAB51 7.3516484E-3,1.7027972E-3
 INDA52 1
 ATAB52 -5.2147852E-4,1.1238928E-3
 INDA53 1
 ATAB53 -3.1368631E-4,1.8065268E-5
 INDA56 1
 ATAB56 8.7E-3,7.3418182E-3
 INDA57 1
 ATAB57 2.0E-5,3.6363636E-5
 REM BCD 3 ENGINE THRUST DATA
 INDTFF 3
 INDTSO 1
 IT1JX 4
 TTAB13 -2.,-1.5,-1.,-.5,0.,.5,1.,1.5,2.
 TTAB10 0.,.1.,.2.,.3
 TTAB10 0.,.1.,.2.,.3
 TTAB10 0.,.1.,.2.,.3
 TTAB10 0.,.1.,.2.,.3
 TTAB10 0.,.1.,.2.,.3
 TTAB10 0.,.1.,.2.,.3
 TTAB10 0.,.1.,.2.,.3
 TTAB10 0.,.1.,.2.,.3
 TTAB10 0.,.1.,.2.,.3
 IT1CW 9
 REM BCD 3 LANDING GEAR DATA
 NSTRT 3
 MASS 4.94.,.50,27.19587,27.19587
 RX 35.,.833,-2.83867,-2.83867
 RY 0.,-.9.3333,+.8.3333
 RZ 1.91667,+.509583,.509583
 THETAD 0.,.0.,.0.
 ERDEG 0.
 RGR 4.47
 NTIRES 2.,.3.,.3.
 RZERO 1.0479167,1.13125,1.13125
 W 554107,+.634107,+.634107
 DELTAM 1.93333,+.1958333,+.1958333
 RLT 1.5E+3
 IFD 1
 AI 1.3204533E+5,3.8129286E+5,3.8129286E+5
 BI 1.2112297,1.412391,1.412391
 FTAB12 2.,.0.,.0.,.1.5E+4
 FTAB13 6.8.,.0.,.0.,.0.,.1.,.336,+.4.,.336,1.,.336,161.,.336
 MOMENT 1.2,2.6,2.6
 KE 1.2,2.6,2.6
 RF 3.48333,6.8792,6.8792
 VZ 0.
 PZERO 35280.,.40320.,.40320.
 VZERO 0.1614583,+.4716435,+.4716435
 A 0.1104166,+.2673611,+.2673611

10
 14
 060800
 0711
 09

ORIGINAL PAGE 14
 OF POOR QUALITY

41


```

NB      1.71:
NLR     1.71:
NTO     1.71:
K2      1.
REM     BCD 40. BRAKE AUTOPILOT DATA
MBC     1.71:
PO      1.71:
DELTAW  1.71:
OMEC01  1.71:
MBL     1.71:
MBU     1.71:
REM     BCD 50. CONTROL RESPONSE DATA
DELHS   1.71:
DELRRD  1.71:
DELA    1.71:
NEO1    1.71:
REM     BCD 40. INITIALIZATION
IAP     1.71:
HR      1.71:
DELQD   4.56478
DELODE  4.56478
DELON   4.56478
DELPD   1.71:
DELRO   1.71:
HANLOG  1.71:
PITCHP  1.71:
REM     BCD 2 STAGING DATA
REH     BCD 4A. GEARS INTO PROGRAM
INDLG   1.71:
ISTAGE  1.71:
DECRES  BCD 1HR
STESTD  1.71:
INDLG   -1
REM     BCD 3. SMOOTH IMPACT STAGE
AINCPS  BCD 30DEL110DEL120DEL13
STEST   -1.5,-1.5,-1.5
TRA     1.71:
PRINT   1.71:
DELTS   1.71:
AMAXER  1.71:
PRTHIN  1.71:
AINCPS  BCD 1TIMES
STEST   1.71:
TRA     1.71:
ATAB51  7.3516484E-3,1.7127972E-3
ATAB52  -5.2147852E-4,1.238928E-3
ATAB53  -3.1368631E-4,1.8665268E-5
ATAB56  1.71:
ATAB57  1.71:
REM     BCD 50. EFFICIENT AMAXER STAGE
AINCPS  BCD 4DELTA1DELTA2DELTA3
STEST   1.71:
TRA     1.71:
PRINT   1.71:
AMAXER  1.71:
DELTS   1.71:
REM     BCD 40. SMOOTH IMPACT STAGE
AINCPS  BCD 10DEL11
STEST   -1.5
TRA     1.71:
PRINT   1.71:
DELTS   1.71:
AMAXER  1.71:
REM     BCD 50. EFFICIENT AMAXER STAGE

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ORIGINAL PAGE IS
OF POOR QUALITY

AINCRS BCD 10ELTA1
STEST .1
TRA
PRINT .5
AMAXER .1
DELTS .31
INOSTF 1
TRA

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 7

A.GEARS INTO PROGRAM

INITIAL PRINT OUT FOR VPCS

8. XGGRF AREFF D1RFF D2RFF
16.0500000E+02 37.7000000E+00 56.7000000E+00

PRINT CODES IDENTIFYING TIME HISTORY

250F							
TIME	TIMES	XG77F	YG77F	HG07F	U777F	V777F	W777F
PI77R	QI77R	RI77R	AHACH	VA77F	OYNOP	XG77F1	YG77F1
ZG77F1	ALPHD	SETAD	ALPHD1	HETAD1	GAM7D	SIG7D	THTPD
PSIPD	PHIPD	AX77F	AY77F	AZ77F	WTR7P	FDC	FCX
FCY	FCZ						
VPCS							
AMASS							
TFFS							
HT	HT						
SAC1							
QAVAH	CA	CN	CY	CL	CM	CNN	

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 8

2SOF

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	57.7454851E-01	0.	0.	-11.6859853E-01	0.	10.3393988E+00
0.	0.	0.	0.	-31.6515539E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

TFFS

0.

0.

0.

T(1)

SAC1

29.7745819E-03-26.8749533E-03 60.9750569E-02 0.

0.

15.3281670E-03 0.

FLARE

AUTS

ALPD&S

PHIDES

TTD

11.5800000E+00 0.

0.

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

26.8544760E-01-14.0024531E-07 0.

0.

-14.0024531E-07 26.8544760E-01

INTEG RTN.

HT = 1.00000000E-03

2SOF

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	90.1422983E-02	0.	0.	-11.6859853E-01	0.	10.3393988E+00
0.	0.	0.	0.	-26.3302709E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM
INDSOF 2 CASE LROLL STAGE 1 PAGE 9

TFFS

0.

0.

0.

0.

T(I)

SACI

29.7745819E-03-28.8749533E-03 68.9758559E-02 0.

0.

15.3281678E-03 0.

AUTS

FLARE

ALPOES

PHIDES

TTD

11.5008000E+00 0.

0.

PITCH AUTOPILOT

DELON

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELODE

27.5607208E-01-14.8024531E-07 0.

0.

-14.8024531E-07 27.5607208E-01

STAGE ON--DECR. HR

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 10

INOLG -1
REM BCD 40. SMOOTH IMPACT STAGE
ATNCRS BCD 30DEL110DEL22COELT3
STEST TRA -.05, -.05, -.05

250F

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	90.1422983E-02	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.			-26.3302709E+00	12.4671000E+04	0.	0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0.	35.2800000E+03	0.	0.	31.9713310E-01	-38.9549765E+02	-78.6562277E+01	0.
0.	40.3200000E+03	0.	0.	54.9315280E-01	-10.7799996E+03	-39.6383699E+01	0.
0.	40.3200000E+03	0.	0.	54.9315280E-01	-10.7799996E+03	-39.6383699E+01	0.

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

ODELTA

33.6000000E-02	29.6159990E+01	0.	0.	-0.	0.	0.	-79.6895154E-01
33.6000000E-02	29.6159990E+01	0.	0.	-0.	0.	0.	-10.9046626E-01
33.6000000E-02	29.6159990E+01	0.	0.	-0.	0.	0.	-10.9046626E-01

SD2

SD1

S

S2D2

S2D1

S2

ONETD1

ONET

0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.

FTRA

FTRB

FTRC

HTX

HTY

HTZ

FXM

FYN

0.	0.	0.	0.	0.	0.	0.	0.
----	----	----	----	----	----	----	----

F2M

LH

HM

NH

0.	0.	0.	0.
----	----	----	----

VPCS

38.7489900E+02

TFFS

0.	0.
----	----

F-11

ORIGINAL PAGE IS
OF POOR QUALITY

INSDOF 2 CASE LROLL STAGE 1 PAGE 11

T E D

SAC1

29.7745819E-03-20.8749533E-03 60.9750569E-02 0.

0.

15.3281670E-03 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01	0.	90.1422650E-02	0.	0.	0.	-20.9135646E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	-55.0126135E-07
20.0000000E-01	0.	10.1746929E-01	0.	0.	0.	-20.4544200E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	-33.2846020E-07
30.0000000E-01	0.	93.2276373E-02	0.	0.	0.	-26.1584011E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	37.9673791E-07
40.0000000E-01	0.	90.1422602E-02	0.	0.	0.	-24.3726223E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	-62.9045083E-07

FLAKE

AUTS

ALPDES

PHIDES

170

11.50000000E+00 0.

Q. 4.

PITCH AUTOPILOT

DELOH

ALPHA

ALFHD1

ALF001

ALPHET

DELODE

27.5339224E-01-14.0024531E-07 0.

04

-14.0024531E-07 27.5339224E-01

[illegible]

YNDSPF 2 CASE LROLL STAGE 1 PAGE 12

[illegible]

50.0000000E-03	50.0000000E-03	14.8031852E+00	0.	96.9255670E-01	29.0027316E+01	0.	59.3319920E+00
27.2368036E-04	0.	0.	26.5170101E-02	29.6034600E+01	10.4122497E+01	29.5967086E+01	0.
62.9389921E-01	11.5616902E+00	94.7824235E-02	12.6453926E-01	0.	12.1824188E-01	0.	10.3434483E+00
0.	0.	0.	0.	-26.7931117E+00	12.4671000E+04	0.	0.

1000

35.28000000E+03 0.
40.32000000E+03 0.
40.32000000E+03 0.

000

31.6173890E-01-38.9549765E+02-78.8562277E+01 0.
49.9512117E-01-10.7799996E+03-39.6383699E+01 0.
49.9512117E-01-10.7799996E+03-39.6383699E+01 0.

HUMP

VGPT

FTRX

FTRY

FIRE

HA

ME

DDelta

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 13

33.6000000E-02 29.5969757E+01 0. 0. -0. 0. 0. -76.5404000E-01
33.6000000E-02 29.5988272E+01 0. 0. -0. 0. 0. -78.2915523E-02
33.6000000E-02 29.5988272E+01 0. 0. -0. 0. 0. -78.2915523E-02

S02 SD1 S S202 S201 S2 ONET01 ONET
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.

FTRA FTRD FTRC HTX HTY HTZ FXH FYH
0. 0. 0. 0. 0. 0. 0. 0.

FZH LH MM NM
85.1226902E-04 0. 71.0026346E-03 0.

VPCS

38.7489900E+02

TFFS

0. 0.

T(1)

SAG1

38.0142493E-03-21.9770889E-03 62.1246500E-02 0. 0. 12.2577406E-03 0.

FLEX

POINT XD1T	X02F Y01F	X02Y Y01T	Y02F Z01F	Y02Y Z01T	Z02F X00F	Z02Y Y00F	X01F Z00F
10.3800000E-01 0.	94.7507440E-02 0.	0.	0.	0.	-23.7844783E-08-28.8565931E+08 0.	0.	-56.1122672E-07
29.0027316E+01 0.	0.	-29.4250924E-08 59.2157808E+08 0.	0.	0.	23.0909337E-05-28.4894263E+08 0.	0.	0.
29.0000000E-01 0.	10.4024866E-01 0.	-69.7159365E-08 59.2364352E+08 0.	0.	0.	0.	0.	-33.9792588E-07
29.0032533E+01 0.	0.	0.	0.	0.	-16.0507200E-05-28.6560050E+00 0.	0.	0.
29.0000000E-01 0.	97.2487500E-02 0.	67.9829249E-08 59.3397243E+00 0.	0.	0.	0.	0.	33.7456793E-07
29.0028704E+01 0.	0.	0.	0.	0.	18.0097006E-06-28.2295520E+00 0.	0.	0.
40.0000000E-01 0.	94.8063785E-02 0.	-63.9733678E-08 59.4200572E+00 0.	0.	0.	0.	0.	-64.2851187E-07
29.0027316E+01 0.	0.	0.	0.	0.	0.	0.	0.

AUTS

FLARE

INDSOFF 2 CASE LROLL STAGE 1 PAGE 14

PITCH AUTOPILOT
01 ALPHET DECODE
61.6902407E-03 28.3036816E-01

[illegible]

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL SYAGE 1 PAGE 15

INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03
INTEG RTN. HT = 1.60000000E-03

2SDF

10.0000000E-02 10.0000000E-02 29.5966730E+00 0. 93.7100927E-01 28.9775565E+01 0. 59.6180378E+00
0. 48.198443E-04 0. 26.5000399E-02 28.5644872E+01 10.3990476E+01 29.5772046E+01 0.
69.6393767E-01 11.6257361E+00 0. 12.9189539E-01 0. -12.7133084E-01 0. 10.3544050E+00
0. 0. 99.5793099E-02 0. -27.2803164E+00 12.4671000E+04 0.
0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	35.2400000E+03	0.	0.	31.1780275E-01	38.9549765E+02	78.8562277E+01	0.
0.	40.3200000E+03	0.	0.	44.7121839E-01	10.7799996E+03	39.6383699E+01	0.
0.	40.3200000E+03	0.	0.	44.7121839E-01	10.7799996E+03	39.6383699E+01	0.

HUVP	VGPT	FYRX	FTRY	FTRZ	HA	HB	ODELTA
33.6000000E-02	29.5776739E+01	0.	0.	-0.	0.	0.	-73.4935144E-01
33.6000000E-02	29.5809538E+01	0.	0.	-0.	0.	0.	-46.1087834E-02
33.6000000E-02	29.5809538E+01	0.	0.	-0.	0.	0.	-46.1087834E-02

SD2	SD1	S	S2D2	S2D1	SZ	OMETD1	OMET
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.

FYRA	FYRO	FYRC	MYX	MTY	MTZ	FXH	FYM
0.	0.	0.	0.	0.	0.	0.	0.

FZH	LH	MM	NH
-11.9013294E-03	0.	-64.1789723E-03	0.

VPCS

38.7489900E+02

TFFS

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 16

0.

0.

0.

0.

T(I)

SAG1

30.2764715E-03-23.1185661E-03 53.3348129E-02 0.

0.

98.5478628E-04 0.

FLEX

POINT XD1T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01 0.	0.	99.4801697E-02 0.	0.	0.	-46.1024553E-05-28.8029586E+80 0.	0.	0.
20.9775565E+01 0.	0.	0.	-12.2028162E-07 59.4123897E+00 0.	0.	0.	0.	-57.2681676E-07
30.0000000E-01 0.	0.	10.6335725E-01 0.	0.	0.	-18.1776925E-05-28.5321778E+00 0.	0.	0.
40.9784303E+01 0.	0.	0.	-14.1871366E-07 59.4489403E+00 0.	0.	0.	0.	-34.6909363E-07
50.0000000E-01 0.	0.	10.1403913E-01 0.	0.	0.	25.2714542E-05-27.1788028E+00 0.	0.	0.
60.9778021E+01 0.	0.	0.	14.4729298E-07 59.6317212E+00 0.	0.	0.	0.	39.5466867E-07
70.0000000E-01 0.	0.	99.6543978E-02 0.	0.	0.	-41.8761248E-05-28.1272092E+00 0.	0.	0.
80.9775565E+01 0.	0.	0.	-19.0476411E-07 59.7738773E+00 0.	0.	0.	0.	-65.5620690E-07

FLARE

AUTS

ALPDES

PHIDES

TYD

11.5000000E+00 0.

0.

PITCH AUTOPILOT

DELON

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELODE

29.1245665E-01 12.5736064E-02 12.9189539E-01 0.

12.5736064E-02 29.1245665E-01

F-17

ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 60

2SDF

62.1500000E-02 62.1500000E-02 18.2926428E+01 0. 72.9115865E-01 28.8820436E+01 0. 47.5712263E+00
-18.0417604E-01 -56.3983248E-03 0. 26.2199277E-02 29.2719810E+01 10.1811336E+01 29.2715414E+01 0.
0. 0. 62.2618457E-01 0. -63.4966603E-01 0. 31.3996816E-02 0. 96.6687600E-01
0. 0. 0. 0. 0. 0. 0.

LGEAR

DELTA P P2 FT SR SF AA FC2

0. 35.2880000E+03 0. 0. -62.565752E-01 -38.9549765E+02 -78.8562277E+01 0.
11.6749011E-02 27.4933394E+04 0. 53.9082090E+03 -25.5789495E+00 -52.5644288E+03 49.4111885E+00 19.7896157E+03
11.6749011E-02 27.4933394E+04 0. 53.9082090E+03 -25.5789495E+00 -52.5644288E+03 49.4111885E+00 19.7896157E+03

HUVP VGPT FTRX FTRY FTRZ HA HB DDELTA

33.6000000E-02 29.2641532E+01 0. 0. -0. 0. 0. -43.3957621E-01
41.3030996E-03 29.5320618E-02 23.0793144E+02 0. -55.0778216E+03 23.4139873E+02 0. 11.6749011E-02
41.3030996E-03 29.5320618E-02 23.0793144E+02 0. -55.0778216E+03 23.4139873E+02 0. 11.6749011E-02

SD2 SD1 S S202 S201 S2 OMETO1 OMET

0. 0. 0. 0. 0. 0. 0. 0.
-78.4491313E-01 -68.3989232E-02 15.0536198E-01 0. 0. 0. 30.0179324E+01 -28.8540956E+01
-78.4491313E-01 -68.3989232E-02 15.0536198E-01 0. 0. 0. 30.0179324E+01 -28.8540956E+01

FTRA FTRD FTRC HTX HTY HTZ FXM FYN

23.0476008E+03 0. -10.7816418E+04 0. -16.5771147E+04 0. 23.0476008E+03 0.

FZH LH NM NH

-10.7772643E+04 0. -16.4045669E+04 0.

VPCS

38.7489900E+02

TFFS

0. 0.

0. 0.

T(I)

SAG1

32.1639271E-03 -65.9787601E-04 47.2255551E-02 0. 0. 17.6467918E-03 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE ROLL STAGE 1 PAGE 61

FLEX		XD2F		XD2T		YD2F		YD2T		ZD2F		ZD2T		XD1F	
POINT	XD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F	YD1F
10.0000000E-01	0.	0.	60.0179868E-01	0.	0.	13.0502055E+00	-33.2022863E+00	0.	-19.8321887E-05	0.	0.	0.	0.	0.	0.
28.8828447E+01	0.	0.	0.	76.9504806E-03	50.0545072E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
28.0000000E-01	0.	0.	60.4463816E-01	0.	0.	85.3002256E-01	-37.9913177E+00	0.	0.	0.	0.	0.	0.	0.	0.
28.3720344E-01	0.	0.	0.	31.4571523E-03	49.5813228E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
28.0000000E-01	0.	0.	62.2192740E-01	0.	0.	-94.4761321E-01	-57.2784095E+00	0.	0.	0.	0.	0.	0.	0.	0.
28.3798690E-01	0.	0.	0.	38.7750153E-03	47.3723550E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
28.0000000E-01	0.	0.	63.1962858E-01	0.	0.	15.4945582E+00	-33.3565560E+00	0.	0.	0.	0.	0.	0.	0.	0.
28.8828447E+01	0.	0.	0.	83.4054559E-03	45.8310878E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1500000E-02 45.0000000E-02

PITCH AUTOPILOT

DELON	ALPHA	ALFHD1	ALPOD1	ALPHET	DELQOE
30.2996071E-01	21.1198852E-02	-63.4966603E-01	0.	21.1198852E-02	43.4246071E-01
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

2SDF

64.1500000E-02	64.1500000E-02	18.8780360E+01	0.	73.2593616E-01	20.8885617E+01	0.	46.9976214E+00
0.	-56.7549533E-03	0.	26.2166853E-02	29.2683577E+01	10.1786030E+01	29.2677745E+01	0.
-18.4769952E-01	92.4026413E-01	0.	-48.6326306E-01	0.	36.1709290E-02	0.	96.0197245E-01
0.	0.	49.3486208E-01	0.	-40.1321787E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FCZ
0.	35.2000000E+03	0.	0.	33.1707709E-01	-38.9549765E+02	-74.8562277E+01	0.
94.9621857E-03	25.9692261E+04	0.	40.1882134E+03	-22.6494581E+00	-38.9053020E+03	47.1730232E+00	29.6171694E+03
94.9621857E-03	25.9692261E+04	0.	40.1882134E+03	-22.6494581E+00	-38.9053020E+03	47.1730232E+00	29.6171694E+03

HUYP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DELTA

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ORIGINAL PAGE 13
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LRLL STAGE 1 PAGE 62

33.6000000E-02 29.2595039E+01 0. 0. -0. 0. 0. -48.3382829E-01
94.9443288E-03 33.4772523E-02 22.6050053E+02 0. -41.1416534E+03 23.4252916E+02 0. 94.9621857E-03
94.9443288E-03 33.4772523E-02 22.6050053E+02 0. -41.1416534E+03 23.4252916E+02 0. 94.9621857E-03

S02	S01	S	S202	S201	S2	QHETO1	QHET
0.	0.	0.	0.	0.	0.	0.	0.
-71.9968675E-01	-83.6761310E-02	14.9017865E-01	0.	0.	0.	30.0324251E+01	28.2543044E+01
-71.9968675E-01	-83.6761310E-02	14.9017865E-01	0.	0.	0.	30.0324251E+01	28.2543044E+01
FTRA	FTRD	FTRC	HTX	HTY	HTZ	FXH	FVH
18.1827401E+03	0.	-80.3764268E+03	0.	-11.6220912E+04	0.	18.1827401E+03	0.
FZH	LH	MH	NH				
-80.0515636E+03	0.	-11.3082022E+04	0.				
VPCS							
38.7489900E+02							
TFFS							
0.	0.						

T(II)

SAC1
32.1311769E-03 -57.5046886E-04 46.1896663E-02 0. 0. 19.1094924E-03 0.

FLEX

POIAT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01	0.	47.9782349E-01	0.	0.	23.6389432E+00	-16.6184467E+00	0.
20.3885637E+01	0.	0.	-34.5907556E-04	49.4156689E+00	0.	0.	-35.0293301E-05
20.0000000E-01	0.	48.2789303E-01	0.	0.	11.8417241E+00	-26.3979406E+00	0.
28.8776845E+01	0.	0.	-44.4173586E-04	48.9843307E+00	0.	0.	-15.0294245E-05
30.0000000E-01	0.	49.4493967E-01	0.	0.	-14.2554604E+00	-54.3810831E+00	0.
28.885685E+01	0.	0.	47.4154695E-04	46.8412544E+00	0.	0.	18.6525130E-05
40.0000000E-01	0.	50.3933676E-01	0.	0.	24.8192763E+00	-15.2195315E+00	0.
28.885637E+01	0.	0.	-28.7303260E-04	45.1596735E+00	0.	0.	-35.6932337E-05

ISS = 1 LANDING RCLL ICS = 0 IBS = 1

AUTS

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 63

TI TR

17.1500000E-02 47.0000000E-02

PITCH AUTOPILOT

DELQW	ALPHA	ALPHD1	ALPCD1	ALPHET	DELQDE
30.2996071E-01	21.1198852E-02	-48.6326306E-01	0.	21.1198852E-02	44.4746071E-01
INTEG RTN.	HT =	1.00000000E-03			
INTEG RTN.	HT =	1.00000000E-03			
INTEG RTN.	HT =	1.00000000E-03			
INTEG RTN.	HT =	1.00000000E-03			

2SDF

66.1500000E-02	66.1500000E-02	19.4633549E+01	0.	73.6406298E-01	28.8917664E+01	0.	46.5715091E+00
0.	-56.3925744E-03	0.	26.2134209E-02	29.2647095E+01	10.1760543E+01	29.2640652E+01	0.
-19.4179462E-01	91.5691297E-01	0.	-34.6325791E-01	0.	38.0176299E-02	0.	95.3708913E-01
0.	0.	36.3127050E-01	0.	-33.1960969E+00	12.4671000E+04	0.	0.
0.	0.						

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	35.2800000E+03	0.	0.	23.4595310E-01	-38.9549765E+02	-78.8562277E+01	0.
72.3024238E-03	24.3786882E+04	0.	27.2734757E+03	-78.6478298E-01	-26.3603627E+03	33.5754276E+00	38.1566536E+03
72.3024238E-03	24.3786882E+04	0.	27.2734757E+03	-78.6478298E-01	-26.3603627E+03	33.5754276E+00	38.1566536E+03

MUVP	VGPT	FTRX	FTRY	FTRZ	MA	HD	ODELTA
33.6000000E-02	29.2550841E+01	0.	0.	-0.	0.	0.	-48.3130693E-01
71.8272747E-03	43.7622429E-02	20.1069908E+02	0.	-27.9935315E+03	21.2922491E+02	0.	72.3024238E-03
71.8272747E-03	43.7622429E-02	20.1069908E+02	0.	-27.9935315E+03	21.2922491E+02	0.	72.3024238E-03

SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
0.	0.	0.	0.	0.	0.	0.	0.
-60.1866426E-01	-94.9762365E-02	14.7230918E-01	0.	0.	0.	27.2977553E+01	-27.6583554E+01
-60.1866426E-01	-94.9762365E-02	14.7230918E-01	0.	0.	0.	27.2977553E+01	-27.6583554E+01

FTRA	FTRB	FTRC	HTX	HTY	MTZ	FXH	FYH
13.2420903E+03	0.	-54.5469514E+03	0.	-72.2346842E+03	0.	13.2420903E+03	0.
F2M	LM	MM	NH				
-54.5460367E+03	0.	-71.2918574E+03	0.				

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 64

VPCS

38.7489900E+02

TFFS

0.

0.

0.

0.

T(I)

SACL

32.0945165E-03-50.7480311E-04 45.3740667E-02 0.

0.

20.4428364E-03 0.

FLEX

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01	0.	35.0454299E-01	0.	0.	11.0509059E+00	-23.6054390E+00	0.
20.8917673E+01	0.	0.	-79.4741263E-03	48.8981200E+00	0.	0.	-15.6216720E-05
20.0000000E-01	0.	35.8934303E-01	0.	0.	50.5134628E-01	-29.3519110E+00	0.
20.8009582E+01	0.	0.	-36.6788638E-03	48.5132679E+00	0.	0.	-70.5386688E-05
30.0009000E-01	0.	36.5267391E-01	0.	0.	-65.2303501E-01	-39.6257333E+00	0.
20.1888922E+01	0.	0.	44.7160818E-03	46.4561453E+00	0.	0.	89.1015197E-06
40.0000000E-01	0.	37.4342545E-01	0.	0.	10.0983643E+00	-21.9946559E+00	0.
20.8917673E+01	0.	0.	-82.7820726E-03	44.6653690E+00	0.	0.	-16.0678336E-05

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IRS = 1

AUTS

TI

TR

17.1500000E-02 49.0000000E-02

PITCH AUTOPILOT

DELON	ALPHA	ALPH01	ALPH001	ALPHET	DELODE
30.2996071E-01	21.1198852E-02	-34.6325791E-01	0.	21.1198852E-02	45.5246071E-01

INTEG RTN.	HT	1.0000000E-03
INTEG RTN.	HT	1.0000000E-03
INTEG RTN.	HT	1.0000000E-03
INTEG RTN.	HT	1.0000000E-03

250F

F-22

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 65

68.1500000E-02 68.1500000E-02 20.0485980E+01 0. 74.0271440E-01 28.8925184E+01 0. 46.2783486E+00
 0. 0. 0. 26.2899235E-02 29.2608010E+01 10.1733248E+01 29.2601811E+01 0.
 -19.0476055E-01 -19.0476055E-01 0. -22.8324411E-01 0. 37.2975909E-02 0. 94.7298131E-01
 0. 0. 29.0976350E-01 0. -27.5545260E+00 12.4671000E+04 0.

LGEAR
 DELTA P P2 FT SR SF AA FC2
 0. 35.2800000E+03 0. 0. -37.8284010E-01 -38.9549765E+02 -78.8562277E+01 0.
 50.9828185E-03 22.8281447E+04 0. 16.5774467E+03 11.2645390E+00 -16.1310602E+03 16.4137616E+00 44.4533807E+03
 50.9828185E-03 22.8281447E+04 0. 16.5774467E+03 11.2645390E+00 -16.1310602E+03 16.4137616E+00 44.4533807E+03

MUVP VGPT FTRX FTRY FTRZ MA MB ODELTA
 33.6000000E-02 29.2511431E+01 0. 0. -0. -0. 0. -40.2973379E-01
 99.5736748E-03 60.6626169E-02 17.0177261E+02 0. -17.0905875E+03 18.3836910E+02 0. 50.9828185E-03
 99.5736748E-03 60.6626169E-02 17.0177261E+02 0. -17.0905875E+03 18.3836910E+02 0. 50.9828185E-03

SD2 SD1 S S2D2 S2D1 S2 OMETD1 OMET
 0. 0. 0. 0. 0. 0. 0. 0.
 -40.2973379E-01 -10.2513772E-01 14.5249216E-01 0. 0. 0. 23.5688346E+01 -27.1260558E+01
 -40.2973379E-01 -10.2513772E-01 14.5249216E-01 0. 0. 0. 23.5688346E+01 -27.1260558E+01

FTRA FTRB FTRC MTX HTY MTZ FXH FYH
 89.8275507E+02 0. -33.1548935E+03 0. -37.1156155E+03 0. 89.8275507E+02 0.

FZH LH MH NH
 -33.7230366E+03 0. -39.8335952E+03 0.

VPCS
 38.7489900E+02

TFFS
 0. 0.

0. 0.

T(I)

SAC1
 32.0568066E-03 -45.4666951E-04 44.7570711E-02 0. 0. 21.6581905E-03 0.

FLEX

F-23

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

POINT X01F	X02F Y01F	INDSDF 2 X02Y Y01T	CASE ROLL Y02F Z01F	STAGE 1 Y02T Z01T	PAGE Z02F X00F	66 Z02T Y00F	X01F Z00F
10.0000000E-01	0.	23.8730248E-01	0.	0.	-12.4285771E+00	-42.4857781E+00	0.
24.3925175E+01	0.	0.	-77.5669016E-03	48.5655884E+00	0.	0.	17.4994244E-05
20.3000000E-01	0.	25.1813304E-01	0.	0.	-58.6914904E-01	-35.4883119E+00	0.
24.3818947E+01	0.	0.	-35.5569154E-03	48.1873122E+00	0.	0.	73.1879492E-06
30.0000000E-01	0.	25.4349457E-01	0.	0.	68.9434588E-01	-20.5005720E+00	0.
24.3896945E+01	0.	0.	43.4343151E-03	46.1644473E+00	0.	0.	-88.9296312E-06
40.0000000E-01	0.	25.1815483E-01	0.	0.	-14.8111127E+00	-40.4778727E+00	0.
20.3925174E+01	0.	0.	-81.6524049E-03	44.4045966E+00	0.	0.	19.5461193E-05

ISS = 1 LANDING ROLL ICS = 0 IBS = 1
ILR = 1

AUTS
II TR
17.1500000E-02 51.0000000E-02

PITCH AUTOPILOT

DELON	ALPHA E	ALPHD1	ALPOD1	ALPHET	DELODE
30.2996071E-01	21.1198852E-02	-22.8324411E-01	0.	21.1198852E-02	46.5746071E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SDF

70.1500000E-02	70.1500000E-02	20.6337599E+01	0.	74.3955512E-01	28.8911295E+01	0.	46.8924470E+00
0.	-54.0084499E-03	0.	26.2060607E-02	29.2564350E+01	10.1703189E+01	29.2559623E+01	0.
-17.6551788E-01	90.6448775E-01	0.	-13.7416649E-01	0.	34.5760878E-02	0.	94.1024801E-01
0.	0.	16.2873324E-01	0.	-23.4251620E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	35.2800000E+03	0.	0.	-59.9779162E-01	-38.9549765E+02	-78.8562277E+01	0.
32.3207231E-03	21.3835431E+04	0.	88.3296626E+02	22.4395307E+00	-86.2315092E+02	77.1497079E-01	48.2663001E+03
32.3207231E-03	21.3835431E+04	0.	88.3296626E+02	22.4395307E+00	-86.2315092E+02	77.1497079E-01	48.2663001E+03

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDelta
33.6000000E-02	29.2474644E+01	0.	0.	-0.	0.	0.	-48.2728216E-01
14.5627181E-02	88.7088549E-02	13.3611354E+02	0.	-91.7489118E+02	14.6762623E+02	0.	32.8207231E-03

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2		CASE LROLL		STAGE 1		PAGE 67	
14.5627181E-02	88.7088549E-02	13.3611354E+02	0.	-91.7489118E+02	14.6762623E+02	0.	32.8207231E-03
SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
0.	0.	0.	0.	0.	0.	0.	0.
-15.8653088E-01	-10.6819815E-01	14.3144304E-01	0.	0.	0.	18.8157209E+01	-26.6998751E+01
-15.8653088E-01	-10.6819815E-01	14.3144304E-01	0.	0.	0.	18.8157209E+01	-26.6998751E+01
FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYH
56.3650055E+02	0.	-17.6659325E+03	0.	-13.6349513E+03	0.	56.3650055E+02	0.
FZH	LH	HH	NH				
-18.4512820E+03	0.	-18.0421941E+03	0.				
VPCS							
38.7489900E+02							
IFFS							
0.	0.						
	0.	0.		T(I)			
SAC1							
32.0204557E-03	-41.3319488E-04	44.3038154E-02	0.	0.	22.7764832E-03	0.	
FLEX							
POINT	XD2F	XD2T	YD2F	YD2T	ZD2F	ZD2T	XD1F
XD1T	YD1F	YD1T	ZD1F	ZD1T	XD0F	YD0F	ZD0F
10.0000000E-01	0.	15.0433681E-01	0.	0.	-23.9754921E+00	-50.6633250E+00	0.
28.8911276E-01	0.	-29.9972575E-05	48.3965094E+00	0.	0.	0.	32.2695842E-05
20.0000000E-01	0.	16.7326610E-01	0.	0.	-11.6220579E+00	-37.7355881E+00	0.
28.3407771E-01	0.	-26.9643437E-04	47.9845452E+00	0.	0.	0.	14.4938271E-05
30.0000000E-01	0.	16.7571040E-01	0.	0.	13.9046736E+00	-93.0490509E-01	0.
33.8863783E-01	0.	23.7563246E-04	45.9415105E+00	0.	0.	0.	-17.7601609E-05
40.0000000E-01	0.	17.2338780E-01	0.	0.	-27.1758433E+00	-40.1285168E+00	0.
28.1911275E-01	0.	0.	-28.9596092E-04	44.3432796E+00	0.	0.	37.0546554E-05

ISS = 1 LANCING RCLL ICS = 0 IBS = 1

AUTS
II TR

F-25

ORIGINAL PAGE IS
OF POOR QUALITY.

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 68

17.1500000E-02 53.0000000E-02

PITCH AUTOPILOT

DELON	ALPHA2	ALPHD1	ALPDD1	ALPHET	DELOBE
30.2996071E-01	21.1198852E-02	13.7416649E-01	0.	21.1198852E-02	47.6246071E-01
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
2SDF					
72.1500000E-02	72.1500000E-02	21.2188335E+01	0.	74.7215927E-01	28.8830577E+01
0.	-52.2970355E-03	0.	25.2018281E-02	29.2517563E+01	10.1670156E+01
-15.5630160E-01	90.4447735E-01	0.	-72.8095444E-02	0.	30.4837073E-02
0.	0.	95.8821551E-02	0.	-20.7061458E+00	12.4671000E+04
0.	0.				0.
0.	0.				0.
LGEAR					
DELTA	P	P2	FT	SR	SF
0.	35.2800000E+03	0.	0.	30.3044655E-02	38.9549765E+02
18.9969322E-03	20.0772929E+04	0.	40.4071906E+02	19.7472430E+00	36.9762315E+02
18.9969322E-03	20.0772929E+04	0.	40.4071906E+02	19.7472430E+00	36.9762315E+02
AA					
FC2					
0.					78.8562277E+01
0.					0.
0.					49.8264861E+03
0.					49.8264861E+03
MUVP					
VGPT	FTRX	FTRY	FTRZ	MA	MB
33.6000000E-02	29.2434667E+01	0.	0.	0.	0.
20.5+12540E-02	12.5103433E-01	87.0632992E+01	0.	-42.3845870E+02	96.8364216E+01
20.5+12540E-02	12.5103433E-01	87.0632992E+01	0.	-42.3845870E+02	96.8364216E+01
ODELTA					
0.					-48.2256705E-01
0.					18.9969322E-03
0.					18.9969322E-03
SD2					
SG1	S	S2D2	S2D1	S2	OMETD1
0.	0.	0.	0.	0.	0.
61.6369794E-02	10.8532535E-01	14.0980202E-01	0.	0.	12.4149258E+01
61.6369794E-02	10.8532535E-01	14.0980202E-01	0.	0.	12.4149258E+01
OMET					
0.					0.
0.					26.3970312E+01
0.					26.3970312E+01
FTRA					
FTRB	FTRC	HTX	HTY	HTZ	FXH
30.9523724E+02	0.	-80.8143812E+02	0.	-24.9773279E+02	0.
0.					30.9523724E+02
0.					0.
FYM					
FZM	LH	NH	NH	NH	NH
-84.7022430E+02	0.	-50.2946407E+02	0.		
0.					
VPCS					

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 69

38.7449900E+02

TFFS

0.

0.

0.

0.

T(I)

SAC1

31.9872647E-03-37.9998726E-04 43.9687907E-02 0.

0.

23.8220768E-03 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01	0.	83.4105302E-02	0.	0.	-12.4232633E+00	-36.9103681E+00	0.
28.8880569E+01	0.	76.8612288E-03	48.2922966E+00	0.	0.	17.5460437E-05	0.
20.0000000E-01	0.	10.2947647E-01	0.	0.	-76.4823030E-01	31.4685654E+00	0.
28.9760337E+01	0.	31.0516843E-03	47.8498977E+00	0.	0.	78.1662372E-06	0.
30.0000000E-01	0.	10.1585584E-01	0.	0.	84.8127057E-01	11.9747169E+00	0.
28.8880569E+01	0.	39.4055834E-03	45.7962338E+00	0.	0.	83.6332751E-06	0.
40.0000000E-01	0.	10.3926083E-01	0.	0.	-16.0425322E+00	33.8834252E+00	0.
28.9880567E+01	0.	76.5742512E-03	44.3697319E+00	0.	0.	19.8270153E-05	0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IIS = 1

YI

TR

17.1500000E-02 55.0000000E-02

PITCH AUTOPILOT

DELQW	ALPHA	ALPHD1	ALPCD1	ALPHET	DELQDE
30.2996071E-01	21.1198852E-02	72.8095444E-02	0.	21.1198852E-02	48.6746071E-01

INTEG RTH. HT = 1.0000000E-03
INTEG RTH. HT = 1.0000000E-03
INTEG RTH. HT = 1.0000000E-03
INTEG RTH. HT = 1.0000000E-03

2SDF

74.1500000E-02	74.1500000E-02	21.8038106E+01	0.	75.0155391E-01	28.8837879E+01	0.	45.9258849E+00
0.	-50.421110E-03	0.	25.1972344E-02	29.2456250E+01	10.1634404E+01	29.2463333E+01	0.
-13.0628238E-01	90.3453071E-01	0.	-30.9215176E-02	0.	25.509558E-02	0.	92.9043961E-01

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 70

0. 0. 52.1081790E-02 0. -19.1648584E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2808000E+03 0. 0. 11.3823576E+00 -38.9549765E+02 -78.8562277E+01 0.
10.0299980E-03 18.9177408E+04 0. 16.2426103E+02 89.8108670E-01 -95.7384714E+01 24.5138806E+00 49.5488229E+03
10.0299980E-03 18.9177408E+04 0. 16.2426103E+02 89.8108670E-01 -95.7384714E+01 24.5138806E+00 49.5488229E+03

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

ODELTA

33.2000000E-02 29.2386276E+01 0. 0. -0. 0. -48.1458424E-01
26.2279293E-02 15.9722319E-01 45.1023565E+01 0. -17.1963086E+02 50.5696643E+01 0. 10.0299980E-03
26.2279293E-02 15.9722319E-01 45.1023565E+01 0. -17.1963086E+02 50.5696643E+01 0. 10.0299980E-03

SD2

SD1

S

S202

S201

S2

OMETD1

OMET

0. 0. 0. 0. 0. 0. 0. 0.
17.4300439E-01 -10.8229708E-01 13.8808741E-01 0. 0. 0. 64.8329029E+00 -26.2131126E+01
17.4300439E-01 -10.8229708E-01 13.8808741E-01 0. 0. 0. 64.8329029E+00 -26.2131126E+01

FTRA

FTRB

FTRC

HTX

HTY

HTZ

FXH

FYH

14.4544617E+02 0. -32.4852205E+02 0. 46.3709320E+01 0. 14.4544617E+02 0.

FZM

LH

MH

NH

-29.5378760E+02 0. 17.1154349E+02 0.

VPCS

38.7489900E+02

YFFS

0. 0.

0.

0.

T(I)

SAC1

31.9584130E-03 -35.1687893E-04 43.7128778E-02 0. 0. 24.8175664E-03 0.

FLEX

POINT
XD1T

XD2F
YD1F

XD2T
YD1T

YD2F
ZD1F

YD2T
ZD1T

ZD2F
XD0F

ZD2T
YD0F

XD1F
ZD0F

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ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 71

15.8000000E-01	0.	40.4644213E-02	0.	0.	10.9379160E+00	-12.3541786E+00	0.
20.8000000E-01	0.	0.	79.8256648E-03	40.1560302E+00	0.	0.	-15.3150578E-05
20.8000000E-01	0.	61.3616641E-02	0.	0.	21.6388497E-01	-20.4002358E+00	0.
28.3741241E-01	0.	0.	34.6043338E-03	47.7294424E+00	0.	0.	-61.3842333E-06
30.8000000E-01	0.	58.1869840E-02	0.	0.	-30.4483784E-01	-22.7406676E+00	0.
28.8000000E-01	0.	0.	-42.8216279E-03	45.7399333E+00	0.	0.	00.0127787E-06
40.8000000E-01	0.	59.5217053E-02	0.	0.	61.0700538E-01	-78.5721068E-01	0.
28.8037887E+01	0.	0.	79.8441265E-03	44.3754351E+00	0.	0.	-15.4209232E-05

AUTS ISS = 1 LANDING ROLL ILR = 1 ICS = 0 IBS = 1

TI TR
17.1500000E-02 57.0000000E-02

PITCH AUTOPILOT

DELOH	ALPHA E	ALPHO1	ALPCD1	ALPHET	DELODE
30.2996071E-01	21.1198852E-02	-30.9215176E-02	0.	21.1198852E-02	49.7246071E-01
INTEG RTN.	HT	1.0000000E-03			
INT IN.	HT	1.0000000E-03			
INT IN.	HT	1.0000000E-03			

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ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 164

26.9810253E+01 0. 0. 93.8205708E+04 18.7804519E+00 0. 0. 25.5352649E+05
40.0000000E+01 0. 74.9498310E+02 0. 0. 22.3545692E+00-13.1858212E+00 0. 0.
28.9909540E+01 0. 0. -30.6885702E+03 50.0140966E+01 0. 0. -43.1604059E+05

AUTS ISS = 1 ILR = 1 LANDING RCLL ICS = 0 IBS = 1

TI TR

17.1500000E+02 18.0500000E+01

PITCH AUTOPILOT

DELOD ALPHAE ALPHD1 ALPDD1 ALPHET DELODE
30.2996071E+01 21.1194852E+02-11.6023798E+00 0. 21.1194852E+02 80.0000000E+01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SDF

19.9650000E+01 19.9650000E+01 58.3301328E+01 0. 70.0502176E+01 28.9916544E+01 0. 10.1435542E+00
0. 19.3791318E+02 0. 25.9846939E+02 29.0093940E+01 99.9937504E+00 29.0093884E+01 0.
18.0669951E+02 28.0183828E+01 0. -11.4996016E+00 0. -35.6857903E+03 0. 19.6815062E+01
0. 0. -72.1927051E+02 0. -34.2246078E+00 12.4671000E+04 0. 0.

LGEAR

DELTA P P2 FT SR SF AA FCZ
75.4320830E+03 39.5622883E+03 0. 11.6667439E+03 41.3452007E+01-11.5840520E+03 16.7392634E+00-68.6782480E+02
13.1358965E+02 24.8347918E+04 0. 65.0147987E+03-90.2920789E+01-64.1555222E+03 31.5958453E+00 20.0573305E+02
13.1358965E+02 24.8347918E+04 0. 65.0147987E+03-90.2920789E+01-64.1555222E+03 31.5958453E+00 20.0573305E+02

HUVP VGPT FTRX FTRY FTRZ MA MB DDELTA
33.6000000E+02 24.6983789E+01-38.7756799E+02 0. -11.5413809E+03-37.7087522E+02 0. 75.4320830E+03
21.3516027E+04 12.8527594E+03 13.8909147E+01 0. -65.0579488E+03 13.8894011E+01 0. 13.1358965E+02
21.3516027E+04 12.8527594E+03 13.8909147E+01 0. -65.0579488E+03 13.8894011E+01 0. 13.1358965E+02

SD2 SD1 S S202 S201 S2 OHETD1 OHET
-11.2812362E+00 70.8592770E+01 15.8277982E+02 0. 0. 0. -15.7119801E+02-42.8757497E+00
-95.8838222E+01-21.7754120E+02 14.7766754E+01 0. 0. 0. 17.8069245E+00-28.8983989E+01
-95.8838222E+01-21.7754120E+02 14.7766754E+01 0. 0. 0. 17.8069245E+00-28.8983989E+01

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSQF 2		CASE LROLL		STAGE 1		PAGE 165	
FTRA	FTRQ	FTRC	HTX	HTY	HTZ	FXH	FYM
12.6741053E+02	0.	-14.1696341E+04	0.	39.5664863E+03	0.	12.6741053E+02	0.
FZH	LH	HH	NH				
-14.1928011E+04	0.	42.5151608E+03	0.				
VPCS							
38.7489900E+02							
TFFS							
0.	0.						

T(II)

SAC1
32.4388518E-03 25.3275264E-03 58.0017738E-03 0. 0. 57.1046238E-04 0.

FLEX

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X08F	Z02T Y08F	X01F Z00F
10.0000000E-01	0.	-22.8265886E-01	0.	0.	-23.9998022E-01	38.6835220E+00	0.
28.9916539E+01	0.	0.	-10.7378381E-02	18.3046119E+00	0.	0.	27.2843866E-06
28.0000000E-01	0.	-19.2807841E-01	0.	0.	79.8787513E-01	28.0017011E+00	0.
28.9545112E+01	0.	0.	-48.7999158E-03	16.8935932E+00	0.	0.	-13.5740258E-06
30.0000000E-01	0.	-61.3599790E-02	0.	0.	-70.9534638E-01	41.2021081E+00	0.
28.3817789E+01	0.	0.	59.0075433E-03	96.5245213E-01	0.	0.	11.2489923E-06
40.0000000E-01	0.	53.7085386E-02	0.	0.	20.2445228E-01	30.8398725E+00	0.
28.9916539E+01	0.	0.	-11.5411390E-02	37.6222996E-01	0.	0.	30.6088668E-06

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

17.1500000E-02 18.2500000E-01

PITCH AUTOPILOT

DELON	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELQDE
38.2996071E-01	21.1198852E-02	-11.4996016E+00	0.	21.1198852E-02	80.0000000E-01

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 166

INTEG RTN. HT = 1.00000000E-03
INTEG RTN. HT = 1.00000000E-03
INTEG RTN. HT = 1.00000000E-03
INTEG RTN. HT = 1.00000000E-03

2SDF

20.1650000E-01 20.1650000E-01 58.9102837E+01 0. 70.0170697E-01 28.9917735E+01 0. 89.9520866E-01
0. -19.2755592E-02 0. 25.9814070E-02 29.0057248E+01 99.9684666E+00 29.0057207E+01 0.
19.4239824E-02 17.7713242E-01 0. -11.2045767E+00 0. -30.4672117E-03 0. 17.4666502E-01
0. 0. -88.4743995E-02 0. -33.0283271E+00 12.4671000E+04 0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
76.4645137E-03	44.2006890E+03	0.	11.8466726E+03	-81.9600585E-01	-11.6413819E+03	41.5568106E+00	-63.9380716E+02
12.8909443E-02	24.415942E+04	0.	63.3144407E+03	72.8176613E-01	-62.8323075E+03	17.7296484E+00	22.9836458E+02
12.3909443E-02	24.4385942E+04	0.	63.3144807E+03	72.8176613E-01	-62.8323075E+03	17.7296484E+00	22.9836458E+02

HUVP	VGPT	FTFX	FTRY	FTRZ	MA	MB	DELTA
33.6000000E-02	21.6444444E+01	-39.4194257E+02	0.	-11.7319716E+03	-38.2940872E+02	0.	76.4645137E-03
37.1530315E-04	22.321701E-03	23.3368890E+01	0.	-63.3510899E+03	23.5519397E+01	0.	12.8909443E-02
37.1530315E-04	22.321701E-03	23.3368890E+01	0.	-63.3510899E+03	23.5519397E+01	0.	12.8909443E-02

S02	S01	S	S202	S201	S2	OMETO1	OYET
12.0175383E-01	68.3702046E-01	29.7226407E-02	0.	0.	0.	-15.9558697E+02	-74.3592226E+00
-71.4763636E-01	23.2692361E-02	14.7302441E-01	0.	0.	0.	30.2460765E+00	-28.8236664E+01
-71.4763636E-01	23.2692361E-02	14.7302441E-01	0.	0.	0.	30.2460765E+00	-28.8236664E+01

FTQA	FTRB	FTRC	MTX	HTY	HTZ	FXH	FYM
74.9926436E+01	0.	-13.8475634E+04	0.	52.9876494E+03	0.	74.9926436E+01	0.

FZH	LH	MH	NH
-13.9268028E+04	0.	49.5090351E+03	0.

VPCS

38.7489900E+02

TFFS

0. 0.

0.

0.

T(I)

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 167

SAC1

32.4423232E-03 26.0409137E-03-70.3270416E-03 0. 0. 60.7604035E-04 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XDDF	ZD2T YDDF	XD1F ZD0F
10.0000007E-01 0.		-24.5094091E-01 0.	0.	0.	-25.4321325E+00 0.	60.7650911E+00 0.	0.
20.9917666E+01 0.		-49.4222890E-03 0.	17.1700314E+00 0.	0.	0.	0.	35.0023438E-05 0.
20.0000000E-01 0.		-20.7214029E-01 0.	0.	0.	-53.4235612E-01 0.	40.3369125E+00 0.	0.
20.3548261E+01 0.		0.	-32.6273683E-03 0.	15.7250835E+00 0.	0.	0.	13.2137342E-05 0.
30.0000000E-01 0.		-76.5605656E-02 0.	0.	0.	79.9952076E-01 0.	24.8944096E+00 0.	0.
20.9819243E+01 0.		0.	35.9201415E-03 0.	84.8395929E-01 0.	0.	0.	-16.7206090E-05 0.
40.0000000E-01 0.		34.1012222E-02 0.	0.	0.	-24.7940055E+00 0.	56.0758572E+00 0.	0.
20.9917662E+01 0.		0.	-63.2953153E-03 0.	26.9948898E-01 0.	0.	0.	37.9884116E-05 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1500000E-02 18.4500000E-01

PITCH AUTOPILOT

DELON

ALPHA

ALPHD1

ALPDD1

ALPHET

DELQDE

30.2996071E-01 21.1198852E-02-11.2045767E+00 0.

21.1198852E-02 80.0000000E-01

INTEG RTA. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

ZSDF

20.3650000E-01 0.	20.3650000E-01 0.	59.4903597E+01 0.	0.	69.9867748E-01 0.	20.9912032E+01 0.	0.	78.7819604E-01 0.
0.	-19.1438972E-02 0.	0.	25.9779855E-02 0.	29.0019055E+01 0.	69.9421508E+00 0.	29.0019015E+01 0.	0.
15.2488057E-02 0.	15.5655743E-01 0.	0.	-10.9101022E+00 0.	0.	-30.1252308E-03 0.	0.	15.2647209E-01 0.
0.	0.	-10.6828257E-01 0.	0.	-31.9005405E+00 0.	12.4671000E+04 0.	0.	0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

79.0289801E-03 50.1365425E+03 0.

12.3151786E+03-12.5358632E+00-12.1128786E+03 40.9514172E+00-61.9938076E+02

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ORIGINAL PAGE 19
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2		CASE LROLL		STAGE 1		PAGE 168	
12.6796384E-02	24.0160893E+04	0.	0.	61.0590155E+03	12.7463742E+00	-61.3936519E+03	17.1115565E+00
12.6796384E-02	24.0160893E+04	0.	0.	61.0590155E+03	12.7463742E+00	-61.3936519E+03	17.1115565E+00
MUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DOELTA
33.6000000E-02	18.5248393E+01	-41.0263473E+02	0.	-12.2142224E+03	-39.7499241E+02	0.	79.0289401E+03
50.3667314E-04	30.6731982E-03	31.5429947E+01	0.	-61.8893813E+03	31.6834751E+01	0.	12.6796384E-02
50.3667314E-04	30.6731982E-03	31.5429947E+01	0.	-61.8893813E+03	31.6834751E+01	0.	12.6796384E-02
SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
-37.4702025E-01	67.3226602E-01	43.3300683E-02	0.	0.	0.	-16.5624664E+02	-10.6758297E+01
-23.0465156E-01	24.8156998E-02	14.6790418E-01	0.	0.	0.	40.6198399E+00	-28.7627031E+01
-23.0465156E-01	24.8156998E-02	14.6790418E-01	0.	0.	0.	40.6198399E+00	-28.7627031E+01
FTRA	FTRB	FTRC	MTX	MTY	MTZ	FXM	FYM
15.2042255E+01	0.	-13.6033210E+04	0.	74.4712007E+03	0.	15.2042255E+01	0.
FZH	LH	HH	NH				
-13.6795562E+04	0.	71.0768408E+03	0.				
VPCS							
38.7489900E+02							
TFFS							
0.	0.						
	0.	0.					
SAC1							
32.4453849E-03	26.7541211E-03	-82.1863814E-03	0.	0.	64.1238157E-04	0.	
FLEX							
POINT	X02F	X02T	Y02F	Y02T	Z02F	Z02T	X01F
Y01T	Y01F	Y01T	Z01F	Z01T	X00F	Y00F	Z00F
10.0000000E-01	0.	-26.5416480E-01	0.	0.	-24.0834772E+00	-58.9189478E+00	0.
28.9911966E+01	0.	0.	55.4538986E-03	16.1042791E+00	0.	0.	34.2882570E-05
20.0000000E-01	0.	-22.2615572E-01	0.	0.	-10.3076658E+00	-44.6917821E+00	0.
28.9544965E+01	0.	0.	82.3961353E-04	14.6048515E+00	0.	0.	14.0252533E-05
38.0000000E-01	0.	-92.3125719E-02	0.	0.	12.3014913E+00	-19.4224719E+00	0.
28.3314481E+01	0.	0.	-15.7090954E-03	73.1888456E-01	0.	0.	-17.2638845E-05
40.0000000E-01	0.	10.1308155E-02	0.	0.	-27.1324010E+00	-56.8088188E+00	0.
28.9911966E+01	0.	0.	42.1851667E-03	17.2858749E-01	0.	0.	36.9573755E-05

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 169

ISS = 1 ILR = 1 ICS = 0 IBS = 1

AUTS

TI

TR

17.1500000E-02 18.6500000E-01

PITCH AUTOPILOT

DELQK

ALPHA E

ALPHD1

ALPCD1

ALPHET

DELODE

30.2996071E-01 21.1198852E-02 -10.9101022E+00 0. 21.1198852E-02 80.0000000E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SOF

20.5650000E-01 20.5650000E-01 60.0703576E+01 0. 69.9547834E-01 28.9899170E+01 0. 67.8998409E-01
0. -18.9938520E-02 0. 25.9743604E-02 28.9978676E+01 99.9143322E+00 28.9978625E+01 0.
17.1288422E-02 13.4172967E-01 0. -10.6202789E+00 0. -33.8441128E-03 0. 13.0788544E-01
0. 0. -13.0968132E-01 0. -30.8855599E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

82.5075408E-03 57.6468916E+03 0. 12.9594918E+03 -68.5132220E-01 -12.8106476E+03 30.1304118E+00 -60.4249137E+02
12.8212330E-02 23.5423018E+04 0. 60.7775679E+03 59.3134354E-01 -50.0220776E+03 27.7832759E+00 28.8667262E+02
12.8212333E-02 23.5423018E+04 0. 60.7775679E+03 59.3134354E-01 -50.0220776E+03 27.7832759E+00 28.8667262E+02

KUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DOELTA

33.0000000E-02 15.2901577E+01 -3.2236635E+02 0. -12.8541856E+03 -41.7285206E+02 0. 82.5075408E-03
47.8330000E-01 25.6202000E-03 29.1190209E+01 0. -60.8001541E+03 29.2948377E+01 0. 12.5212104E-02
47.8330000E-01 25.6202000E-03 29.1190209E+01 0. -60.8001541E+03 29.2948377E+01 0. 12.5212304E-02

SD2

SD1

S

S2D2

S2D1

S2

OMETD1

OMET

-88.9652835E-01 56.4553249E-01 56.7387168E-02 0. 0. 0. -17.3668836E+02 -14.0641650E+01
15.4900152E-01 -26.1233328E-02 14.6258418E-01 0. 0. 0. 37.5574778E+00 -28.7141094E+01
15.4900152E-01 -26.1233328E-02 14.6258418E-01 0. 0. 0. 37.5574778E+00 -28.7141094E+01

FTRA

FTRB

FTRC

HTX

HTY

MTZ

FXM

FYM

-66.9869629E+01 0. -13.4514828E+04 0. 98.3937677E+03 0. -66.9869629E+01 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 170

FZM LH HH NH
-13.4690287E+04 0. 98.6282348E+03 0.

VPCS
38.7489900E+02

TFFS
0. 0.

T(1)

SAC1
32.4485127E-03 27.4691120E-03-93.6175649E-03 0. 0. 67.2181673E-04 0.

FLEX

POINT XDIT	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01 0.	0.	-28.8901775E-01 0.	0.	0.	35.1939558E-02-34.2543156E+00 0.	0.	0.
28.9899171E+01 0.	0.	0.	19.5466798E-02 0.	14.9995007E+00 0.	0.	0.	-89.0134018E-07
20.0000000E-01 0.	0.	-24.2050626E-01 0.	0.	0.	-50.0643431E-01-39.0205357E+00 0.	0.	0.
28.9535110E+01 0.	0.	0.	32.3234864E-03 0.	13.4859777E+00 0.	0.	0.	10.0952709E-06
30.0000000E-01 0.	0.	-11.4589782E-01 0.	0.	0.	-4.201109E-01-21.2307657E+00 0.	0.	0.
28.9502381E+01 0.	0.	0.	-44.5151500E-03 0.	62.012211E-01 0.	0.	0.	-7.0041415E-07
40.0130001E-01 0.	0.	-17.942436E-02 0.	0.	0.	-43.139711E-01-32.3794472E+00 0.	0.	0.
28.9502381E+01 0.	0.	0.	95.349103E-03 0.	74.3933741E-02 0.	0.	0.	10.4439531E-05

ISE = 1

LANDING ROLL
ILR = 1

ICS = 0

IRS = 1

AUTS

II

TR

17.1500000E-02 10.8500000E-01

PITCH AUTOPILOT

DELON	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELQDE
30.2996071E-01	21.1198852E-02-10.6202789E+00 0.	0.	0.	21.1198852E-02 80.0000000E-01	0.

INTEG RTN. HT = 1.00000000E-03
INTEG RTN. HT = 1.00000000E-03
INTEG RTN. HT = 1.00000000E-03

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 171

INTEG RYN. HT = 1.00000000E-03

2SDF

20.7650000E-01	20.7650000E-01	60.6502726E+01	0.	25.9705208E-02	69.9173809E-01	28.9879144E+01	0.	57.2764326E-01
0.	-18.8004229E-02	0.	0.	28.9935724E+01	99.8847469E+00	28.9935651E+01	0.	0.
20.5682608E-02	11.3194445E-01	0.	-18.3600649E+00	0.	-40.6448536E-03	0.	0.	10.9129839E-01
0.	0.	-16.2337048E-01	0.	-30.1287103E+00	12.4671000E+04	0.	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
87.3114972E-03	67.6201403E+03	0.	13.8625653E+03	48.5978510E-02	-13.7619946E+03	20.3584438E+00	-58.5902762E+02
12.4101621E-02	23.1991817E+04	0.	60.0259992E+03	-29.9572718E-01	-58.9852791E+03	38.2675776E+00	28.8385239E+02
12.4101621E-02	23.1991817E+04	0.	60.0259992E+03	-29.9572718E-01	-58.9852791E+03	38.2675776E+00	28.8385239E+02

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	MB	DDelta
33.6000000E-02	11.9092227E+01	-46.2903887E+02	0.	-13.7769014E+03	-44.4667882E+02	0.	87.3114972E-03
25.6048737E-04	15.4064008E-03	15.3731194E+01	0.	-60.0398173E+03	15.4830123E+01	0.	12.4101621E-02
25.6048737E-04	15.4064008E-03	15.3731194E+01	0.	-60.0398173E+03	15.4830123E+01	0.	12.4101621E-02

SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
-11.3237413E+00	65.4445283E-01	69.9345585E-02	0.	0.	0.	-18.5278264E+02	-17.6550403E+01
31.0368622E-01	-26.1105686E-02	14.5734317E-01	0.	0.	0.	15.8500157E+00	-28.6780422E+01
31.0368622E-01	-26.1105686E-02	14.5734317E-01	0.	0.	0.	15.8500157E+00	-28.6780422E+01

FTRA	FTRB	FTRC	MTX	MTY	HTZ	FXH	FYH
-17.7141480E+02	0.	-13.3914564E+04	0.	12.7555187E+04	0.	-17.7141480E+02	0.

FZH	LM	NH	NH
-13.3523511E+04	0.	13.1222538E+04	0.

VPCS

38.7489900E+02

TFFS

0. 0.

0. 0.

SA 11

T(1)

ORIGINAL PAGE IS
OF POOR QUALITY

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SIX DIGITS OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 172

32.4521021E-03 28.1880774E-03-10.4661502E-02 0. 0. 70.0661611E-04 0.

FLEX

POINT XDIT	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01	0.	-31.5112759E-01	0.	0.	24.2689248E+00	-10.4969500E+00	0.
28.5879211E+01	0.	0.	52.2301538E-03	13.8013934E+00	0.	0.	-35.3758391E-05
220.0000000E-01	0.	-26.6192774E-01	0.	0.	23.2248886E-01	-31.6869417E+00	0.
228.3518826E+01	0.	0.	17.8565110E-03	12.3413085E+00	0.	0.	-12.3720606E-05
30.0000000E-01	0.	-14.5844704E-01	0.	0.	-53.2098637E-01	-35.1591917E+00	0.
28.5783310E+01	0.	0.	-24.4360635E-03	51.6952523E-01	0.	0.	16.1605977E-05
40.0000000E-01	0.	-49.7316068E-02	0.	0.	19.5122817E+00	-71.0233374E-01	0.
28.9879210E+01	0.	0.	44.5400503E-03	-30.6613815E-02	0.	0.	-34.8997634E-05

ISS = 1

LANDING RCLL
ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

17.1500000E-02 19.0500000E-01

PITCH AUTOPILOT

DELON	ALPHA E	ALPHD1	ALPOD1	ALPHET	DELODE
30.2996071E-01	21.1198852E-02	-10.3600649E+00	0.	21.1198852E-02	80.0000000E-01

INTEG RTN.	HT =	1.00000000E-03
INTEG RTN.	HT =	1.00000000E-03
INTEG RTN.	HT =	1.00000000E-03
INTEG RTN.	HT =	1.00000000E-03

2SOF

20.9650000E-01	20.9650000E-01	61.2300990E+01	0.	69.8719070E-01	26.9851827E+01	0.	46.8824677E-01
0.	-18.5530023E-02	0.	25.9664014E-02	28.9889740E+01	99.8530785E+00	28.9889632E+01	0.
25.0246551E-02	92.6657374E-02	0.	-10.1474090E+00	0.	-49.4599334E-03	0.	87.7196938E-02
0.	0.	-19.7530480E-01	0.	-29.7503989E+00	12.4671000E+04	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
94.0729946E-03	81.4199705E+03	0.	15.1553180E+03	45.9058508E-02	-15.0628882E+03	18.7104970E+00	-55.8924525E+02
12.3337345E-02	22.8237476E+04	0.	59.5113265E+03	-31.8477173E-01	-58.4677772E+03	38.3716099E+00	24.6329973E+02
12.3337345E-02	22.8237476E+04	0.	59.5113265E+03	-31.8477173E-01	-58.4677772E+03	38.3716099E+00	24.6329973E+02

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

MOVPT		VGPT	FTRX	FTRY	FTRZ	HA	HB	DDelta
33.6000000E-02	83.4036734E+00	-50.6671770E+02	0.	-15.0795170E+03	-48.3235679E+02	0.	94.0729.6E-03	
62.6612885E-01	37.6331142E-01	-37.2948570E-01	0.	-29.5192446E+03	-37.5900007E-01	0.	12.333377.9E-02	
62.6612885E-01	37.6991142E-05	-37.2948590E-01	0.	-59.5182446E+03	-37.5900007E-01	0.	12.33337345E-02	
S02	S01	S	S202	S201	S2	OMETD1	OMET	
-13.000.734E+00	63.9239617E+01	82.8652371E-02	0.	0.	0.	-20.1369033E+02	-21.5200891E+01	
30.1660877E-01	-24.1317294E-02	14.5243213E-01	0.	0.	0.	-48.1923085E-02	-23.6516473E+01	
30.1660877E-01	-24.1317294E-02	14.5243213E-01	0.	0.	0.	-48.1923085E-02	-23.6516473E+01	
FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYM	
-30.2034956E+02	0.	-13.4177971E+04	0.	16.7992840E+04	0.	-30.2034956E+02	0.	
FZH	LH	NH	NH					
-13.3767425E+04	0.	17.2127866E+04	0.					
VPCS								
38.7489900E+02								
TEFS								
0.	0.							
SAC1								
32.4564466E-03	28.9131995E-03	-11.5357798E-02	0.	0.	72.6884394E-04	0.		
FLEX								
POINT	XD2F	XD2T	YD2F	YD2T	ZD2F	ZD2T	XD1F	
XD1T	YD1F	YD1T	ZD1F	ZD1T	XD0F	YD0F	ZD0F	
10.0000000E-01	0.	-34.2554576E-01	0.	0.	24.6656369E+00	-10.8567416E+00	0.	
28.3851893E+01	0.	0.	-52.2783315E-03	12.5544823E+00	0.	0.	-35.8349146E-05	
20.0000000E-01	0.	-29.1825456E-01	0.	0.	28.5144458E-01	-31.7110637E+00	0.	
28.3496133E+01	0.	0.	-16.6392828E-03	11.1827179E+00	0.	0.	-12.7064017E-05	
20.0000000E-01	0.	-18.1644367E-01	0.	0.	-59.7117419E-01	-35.3551078E+00	0.	
28.3757222E+01	0.	0.	21.2081636E-03	41.8262610E-01	0.	0.	16.4644383E-05	
20.0000000E-01	0.	-84.0269789E-02	0.	0.	20.5555105E+00	-48.2081805E-01	0.	
28.9551893E+01	0.	0.	-57.6714873E-03	-13.7016259E-01	0.	0.	-35.9042189E-05	

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

I8S = 1

F-39

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 174

AUTS

TI TR

17.1500000E-02 19.2500000E-01

PITCH AUTOPILOT

DELON	ALPHA	ALPHD1	ALPDD1	ALPHET	DELODE
30.2996071E-01	21.1198852E-02	10.1474090E+00	0.	21.1198852E-02	80.0000000E-01
INTEG RTN.	HT = 1.00000000E-03				
INTEG RTN.	HT = 1.00000000E-03				
INTEG RTN.	HT = 1.00000000E-03				

2SDF

21.0950000E-01	21.0950000E-01	51.6069349E+01	0.	69.8372602E-01	28.9830128E+01	0.	40.2420695E-01
0.	-18.3076860E-02	0.	25.9635638E-02	28.9858064E+01	99.8312685E+00	28.9857926E+01	0.
28.2436196E-02	79.5484105E-02	0.	-10.0674914E+00	0.	-55.8274975E-03	0.	73.9655385E-02
0.	0.	-21.1762258E-01	0.	-29.8966100E+00	12.4671000E+04	0.	0.
0.	0.						

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
10.0098848E-02	93.5532400E+03	0.	16.3264091E+03	-18.7357226E+00	-16.1470707E+03	36.3033343E+00	-52.9202851E+02
12.2778257E-02	22.6091088E+04	0.	59.1312288E+03	19.9861663E+00	-58.7459559E+03	14.1665956E+00	16.1492012E+02
12.2778257E-02	22.6091088E+04	0.	59.1312288E+03	19.9861663E+00	-58.7459559E+03	14.1665956E+00	16.1492012E+02

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.6000000E-02	59.0575100E+00	-54.6243561E+02	0.	-16.2572488E+03	-51.7739399E+02	0.	10.0098848E-02
18.1708322E-04	10.9313797E-03	10.7457838E+01	0.	-59.1375436E+03	10.8368193E+01	0.	12.2778257E-02
18.1708322E-04	10.9313797E-03	10.7457838E+01	0.	-59.1375436E+03	10.8368193E+01	0.	12.2778257E-02

SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
-14.6037073E+00	62.2011194E-01	91.0827927E-02	0.	0.	0.	-21.5724749E+02	-24.2252718E+01
19.0144285E-01	-19.5391352E-02	14.4947362E-01	0.	0.	0.	13.8933581E+00	-23.6347969E+01
19.0144285E-01	-19.5391352E-02	14.4947362E-01	0.	0.	0.	13.8933581E+00	-23.6347969E+01

FTRA	FTRB	FTRC	MTX	HTY	HTZ	FXH	FYM
-35.1039625E+02	0.	-13.4588867E+04	0.	20.8377044E+04	0.	-35.1039625E+02	0.
FZH	LM	HH	NH				
-13.5417020E+04	0.	20.5668653E+04	0.				

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSO 2 CASE LROLL STAGE 1 PAGE 175

VPCS

38.7489900E+02

TFFS

0.

0.

0.

0.

T(I)

SAC1

32.4603099E-03 29.3889078E-03-12.2135599E-02 0.

0.

74.2802727E-04 0.

FLEX

POINT XDIT	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01	0.	-35.6607964E-01	0.	0.	-27.1273517E+00	-63.7220067E+00	0.
28.9830056E+01	0.	0.	24.6728290E-03	11.8857652E+00	0.	0.	38.9164925E-05
20.0000000E+01	0.	-29.9989824E-01	0.	0.	-15.0810211E+00	-50.5505162E+00	0.
28.3478049E+01	0.	0.	-10.4695913E-04	10.4671504E+00	0.	0.	16.9355485E-05
30.0000000E+01	0.	-19.4106629E-01	0.	0.	16.9833508E+00	-12.4847683E+00	0.
28.9736567E+01	0.	0.	-22.1334351E-04	35.0069562E-01	0.	0.	-20.4801567E-05
40.0000000E-01	0.	-10.3375440E-01	0.	0.	-33.3983104E+00	-58.2184596E+00	0.
28.3830043E+01	0.	0.	19.1476346E-03	-18.9552442E-01	0.	0.	42.9864828E-05

ISS = 1

LANDING ROLL

ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

17.1500000E-02 19.3800000E-01

PITCH AUTOPILOT

DELON

ALPHA

ALPHD1

ALPDD1

ALPHET

DELQDE

30.2995071E-01 21.1198852E-02-10.0674914E+00 0.

21.1198852E-02 80.0000000E-01

STAGE ON--INCR. DELTA1

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ORIGINAL PAGE 19
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 176

PRINT .05
ANAXER .01
OLTS .01
INDSTF 1
TRA

2SOF

21.0950000E-01	21.0950000E-01	61.6069349E+01	0.	69.8372602E-01	28.9830128E+01	0.	40.2420695E-01
0.	-18.3676860E-02	0.	25.9635638E-02	28.9858064E+01	99.8312685E+00	28.9857926E+01	0.
28.2436196E-02	79.5484105E-02	0.	-10.0674914E+00	0.	-55.8274975E-03	0.	73.9655385E-02
0.	0.	-21.1762258E-01	0.	-29.8966108E+00	12.4671000E+04	0.	0.
0.	0.						

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FG2
10.0098844E-02	93.5532400E+03	0.	16.3264091E+03	-18.7357226E+00	-16.1470707E+03	36.3033343E+00	-52.9202451E+02
12.2778257E-02	22.6091088E+04	0.	59.1312288E+03	19.9861663E+00	-58.7459559E+03	14.1665956E+00	16.1492012E+02
12.2778257E-02	22.6091088E+04	0.	59.1312288E+03	19.9861663E+00	-58.7459559E+03	14.1665956E+00	16.1492012E+02

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DOELTA
33.6000000E-02	59.0575100E+00	-54.6243861E+02	0.	-16.2572488E+03	-51.7739399E+02	0.	10.0098844E-02
19.1708322E-04	10.9313797E-03	10.7457838E+01	0.	-59.1375436E+03	10.8369193E+01	0.	12.2778257E-02
18.1708322E-04	10.9313797E-03	10.7457838E+01	0.	-59.1375436E+03	10.8369193E+01	0.	12.2778257E-02

SD2	SD1	S	S202	S201	S2	OMETD1	OMET
-14.6037073E+00	62.2011194E-01	91.0827927E-02	0.	0.	0.	-21.5724749E+02	-24.2252718E+01
19.3144285E-01	-19.5391352E-02	14.4947362E-01	0.	0.	0.	13.8933581E+00	-28.6347969E+01
19.3144285E-01	-19.5391352E-02	14.4947362E-01	0.	0.	0.	13.8933581E+00	-28.6347969E+01

FTRA	FTRD	FTRG	MTX	HTY	HTZ	FXH	FYM
-35.1039625E+02	0.	-13.4588867E+04	0.	20.8377044E+04	0.	-35.1039625E+02	0.

FZH	LH	NH	NH
-13.5417020E+04	0.	20.5868653E+04	0.

VPCS
38.7489900E+02

TFFS
0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 177

T(II)

0. 0.

SAC1

32.4683099E-03 29.3889078E-03-12.2135599E-02 0. 0. 74.2802727E-04 0.

FLEX

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01 0.		-35.6607964E-01 0.	0.	0.	-27.1273517E+00-63.7228087E+00 0.		
28.9830056E+01 0.		0.	24.6728290E-03 11.8057652E+00 0.		0.		38.9184925E-05
20.0000000E-01 0.		-29.9989824E-01 0.	0.	0.	-15.0810211E+00-50.5505162E+00 0.		
28.9478043E+01 0.		0.	-10.4695913E-04 10.4671504E+00 0.		0.		16.9355485E-05
30.0000000E-01 0.		-19.4106E29E-01 0.	0.	0.	16.9833508E+00-12.4847683E+00 0.		
28.5736567E+01 0.		0.	-22.1334351E-04 35.0059562E-01 0.		0.		-20.4801567E-05
40.0000000E-01 0.		-10.3375440E-01 0.	0.	0.	-33.3983104E+00-58.2184596E+00 0.		
28.9830043E+01 0.		0.	19.1476346E-03-18.9552442E-01 0.		0.		42.9864828E-05

ISS = 1 LANDING ROLL ICS = 0 IBS = 1

AUTS

II TR

17.1500000E-02 19.3800000E-01

PITCH AUTOPILOT

DELON	ALPHA E	ALPH D1	ALPH D1	ALPH ET	DEL ODE
30.2996071E-01	21.1198852E-02	-10.0674914E+00 0.		21.1198852E-02	80.0000000E-01

INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03

ZSOF

21.5950000E-01	21.5950000E-01	63.0559132E+01 0.	0.	69.6677134E-01	28.9743395E+01 0.	15.3994660E-01
0.	-17.1516415E-02 0.	0.	25.9536575E-02	28.9747187E+01	99.7551641E+00 28.9747231E+01	0.
38.5446397E-02	30.4516381E-02 0.	0.	-96.1839149E-01 0.	0.	-76.2189912E-03 0.	22.8296709E-02
0.	0.	-15.0373746E-01 0.	0.	-31.1259701E+00	12.4671000E+04 0.	0.
0.	0.					

LGEAR

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ORIGINAL DATA
OF FOUR QUANTITIES

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

DELTA		P	INDSDF 2	CASE LROLL	STAGE 1	PAGE	178		
			P2	FT	SR	SF	AA	FC2	
14.2530236E-02	19.5920315E+04	0.		24.9482985E+03	-30.1885493E+00	-24.9521409E+03	-77.7885192E-02	-31.8374715E+02	
12.2876369E-02	22.0449682E+04	0.		59.2037088E+03	22.3974930E+00	-38.6788961E+03	19.2975162E+00	23.4145977E+01	
12.2876369E-02	22.0449682E+04	0.		59.2037088E+03	22.3974930E+00	-38.6788961E+03	19.2975162E+00	23.4145977E+01	
HUVP	VGPT		FTRX	FTRY	FTRZ	MA	MO	DOELTA	
58.3249863E-03	35.0786305E-02	-14.5478263E+02	0.		-24.9426999E+03	-13.1714050E+02	0.	14.2530236E-02	
51.3042903E-03	30.8501245E-04	30.3743400E+00	0.		-59.2042999E+03	30.6285835E+00	0.	12.2876369E-02	
51.3042903E-03	30.8501245E-04	30.3743400E+00	0.		-59.2042999E+03	30.6285835E+00	0.	12.2876369E-02	
SD2	SD1	S	S2D2		S2D1	S2	ONEID1	OMET	
-63.1401491E+00	48.2454540E-01	11.9895003E-01	0.		0.	0.	-54.8808542E+01	-31.8469919E+01	
95.2126469E-01	-74.4000396E-03	14.4142297E-01	0.		0.	0.	39.2675429E-01	-28.6331068E+01	
95.2126469E-01	-74.4000396E-03	14.4142297E-01	0.		0.	0.	39.2675429E-01	-28.6331068E+01	
FTRA	FTRB	FTRC	NTX		HTY	HTZ	FXH	FYH	
-82.2836951E+01	0.	-14.3355716E+04	0.		53.2655257E+04	0.	-82.2836951E+01	0.	
FZH	LH	MH	NH						
-14.4164734E+04	0.	53.8760574E+04	0.						
VPCS									
38.7469900E+02									
TFFS									
0.	0.								
	0.	0.							
					T(I)				
SAC1									
32.4743717E-03	31.2638629E-03	-14.7115522E-02	0.		0.		79.6457465E-04	0.	
FLEX									
POINT	X02F	X02T	Y02F	Y02T	Z02F	Z02T	X01F		
X01T	Y01F	Y01T	Z01F	Z01T	X00F	Y00F	Z00F		
10.0000000E-01	0.	-27.4612015E-01	0.	0.	-26.2167508E+00	-73.0208785E+00	0.		
28.3743323E+01	0.	0.	-36.9274855E-03	88.2114388E-01	0.	0.	38.9102387E-05		
20.0000000E-01	0.	-13.2787401E-01	0.	0.	-18.2983190E+00	-62.3622625E+00	0.		
28.9414520E+01	0.	0.	-10.5082732E-03	75.4687034E-01	0.	0.	18.0193617E-05		
30.0000000E-01	0.	-12.3830630E-01	0.	0.	20.3211674E+00	-97.7670605E-01	0.		

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 179

28.9656030E+01 0. 0. 15.2955174E-03 10.6035893E-01 0. 0. 0. 2050140E+00 -21.9842279E-05
40.0000000E-01 0. -54.1824241E-02 0. 0. 0. 0. 0. 0. 0.
28.9743327E+01 0. 0. -30.8043280E-03 -40.3661411E-01 0. 0. 0. 39.9646651E-05

ISS = 1 LANDING ROLL ICS = 0 IBS = 1

AUTS

TI

TR

17.1500000E-02 19.8800000E-01

PITCH AUTOPILOT

DELQX ALPHAE ALPHD1 ALPG01 ALPHET DELODE

30.2996071E-01 21.1198852E-02 -96.1839149E-01 0. 21.1198852E-02 80.0000000E-01

INTEG RTN. HT = 1.00000000E-03
INTEG RTN. HT = 1.00000000E-03

TIRE DEFLECTION EXCEEDED

DELTA(1) = 1.9869599E-01

INTEG RTN. HT = 1.00000000E-03

2SDF

21.3525000E-01 21.8525000E-01 63.8019525E+01 0. 69.5671454E-01 23.9699016E+01 0. 38.1886577E-02
0. -15.9006410E-02 0. 25.9493290E-02 28.9699173E+01 99.7219286E+00 28.9698918E+01 0.
38.4637672E-02 59.7061765E-03 0. -94.3568651E-01 0. -76.0714697E-03 0. -18.3662593E-03
0. 0. -21.4311032E-01 0. -33.7755465E+00 12.4671000E+04 0. 0.

LGEAR

DELTA P P2 FT SR SF AA FC2

19.3695991E-02 32.1595919E+04 0. 37.1384926E+03 -26.3298921E+00 -37.1390942E+03 -12.1775498E-02 -13.1146395E+02
12.2825657E-02 21.9182934E+04 0. 59.1697989E+03 53.7279340E-01 -58.5657646E+03 21.1074063E+00 31.9592339E-01
12.2825657E-02 21.9182934E+04 0. 59.1697989E+03 53.7279340E-01 -58.5657646E+03 21.1074063E+00 31.9592339E-01

HUVP VGPT FTRX FTRY FTRZ MA H8 DOELTA

85.4853381E-03 51.3727757E-02 -31.7189221E+02 0. -37.1392736E+03 -26.9363656E+02 0. 19.8695991E-02
58.4920741E-03 35.4275912E-04 34.8463178E+00 0. -59.1697921E+03 35.1398782E+00 0. 12.2825657E-02
58.4920741E-03 35.4275912E-04 34.8463178E+00 0. -59.1697921E+03 35.1398782E+00 0. 12.2825657E-02

SD2 SD1 S S2D2 S2D1 S2 OMETD1 OMET

-59.6256666E+00 30.9645870E-01 13.0262602E-01 0. 0. 0. -11.2234856E+02 -33.9386571E+01
-59.6379931E-01 -86.9216643E-04 14.3955645E-01 0. 0. 0. 45.0511220E-01 -28.6342829E+01
-59.6379931E-01 -86.9216643E-04 14.3955645E-01 0. 0. 0. 45.0511220E-01 -28.6342829E+01

FTRA FTRB FTRC HTX HTY HTZ FXH FYH

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 180

-31.4661123E+02 0. -15.5477965E+04 0. 94.5231037E+04 0. -31.4661123E+02 0.
FZH LH NM
-15.6346368E+04 0. 95.3256969E+04 0.
VPCS
34.7489900E+02
TFFS
0. 0.

TIME

SAC1
32.4860544E-03 32.2420975E-03-15.9347387E-02 0. 0. 81.9844148E-04 0.

FLEX

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
4.0000000E-01 0.	-31.9617414E-01 0.	0.	0.	0.	-19.5065357E+00-80.0713732E+00 0.	23.5701340E-05	
0.0000000E-01 0.	0.	0.	0.	0.	0.	0.	
0.0000000E-01 0.	-14.1394034E-01 0.	-8.1073671E-03 70.0597800E-01 0.	-13.8503994E-01-57.2369207E+00 0.	0.	0.	0.	
0.0000000E-01 0.	0.	0.	0.	0.	0.	0.	
0.0000000E-01 0.	-17.6663599E-01 0.	-39.9129658E-03 58.4044319E-01 0.	38.9070072E-01-24.1154039E+00 0.	0.	0.	0.	
0.0000000E-01 0.	0.	0.	0.	0.	0.	0.	
0.0000000E-01 0.	-12.9820258E-01 0.	47.6987126E-03-10.1781436E-02 0.	-17.1503923E+00-30.6246760E+00 0.	0.	0.	0.	
0.0000000E-01 0.	0.	0.	0.	0.	0.	0.	
0.0000000E-01 0.	-89.6368120E-03-49.2495219E-01 0.	0.	0.	0.	0.	0.	

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IDS = 1

TI

TR

17.1508000E-02 20.1375000E-01

PITCH AUTOPILOT

DELON	ALPHA	ALPHD1	ALPDD1	ALPHET	DELODE
30.2996071E-01	21.1198852E-02-94.3568651E-01 0.	21.1198852E-02 80.0000000E-01			

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OF POOR QUALITY

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APPENDIX G

AIRPLANE B FLEXIBLE BODY EXAMPLE 4

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ORIGINAL PAGE IS
OF POOR QUALITY

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ATA952 1.4120979E-3,8.8931664E-4
INDA12 1
INDA83 1
ATAB83 4.18951E-2,2.10644E-2
INDA11 1
ATA910 -3.978321E-2,-3.965349E-2
INDA11 1
ATAB11 5.7452448E-2,3.7645688E-2
INDA12 1
ATA912 1.4720279E-3,1.2354312E-3
INDA15 1
ATAB15 -1.725E-2,-1.45E-2
INDA16 1
ATAB16 1.25E-4,5.1E-5
INDA51 1
ATAB51 7.3516484E-3,1.7127972E-3
INDA52 1
ATAB52 -5.2147852E-4,1.1238928E-3
INDA53 1
ATAB53 -3.1368631E-4,1.8365268E-5
INDA56 1
ATAB56 8.7E-3,7.3418182E-3
INDA57 1
ATAB57 3.0E-5,3.6363636E-5
REH BCD ENGINE THRUST DATA
INDIFF 3
INDTSO 4
IT13X 1
TTAB13 -2.,-1.5,-1.,-.5,0.,.5,1.,1.5,2.
TTAB10 0.,.1,.2,.3
TTAB13 0.,.1,.2,.3,0.
TTAB10 0.,.1,.2,.3,0.
TTAB10 0.,.1,.2,.3,0.
TTAB10 0.,.1,.2,.3,0.
TTAB10 0.,.1,.2,.3,0.
TTAB10 0.,.1,.2,.3,0.
IT10H 9
REH BCD LANDING GEAR DATA
NSTRUT 3
MASS 4.94100,27.19587,27.19587
RX 35.1833,-2.83867,-2.83867
RY 1.1-4.3333,8.3333
RZ 1.91667,.534583,.519583
THETAD 0.,.1,0.
ERDEG 0.
RGR 4.47
NTIRES 2.,3.,3.
PZERO 1.0479167,1.13125,1.13125
H .954167,.634167,.634167
DELTAM .195333,.195333,.195333
RLT .9E+3
IFO 1.
AI 1.32,4533E+5,3.8129286E+5,3.8129286E+5
BI 1.2112257,1.412391,1.412391
FTAB82 0.,.1,.2,.3,0.
FTAB82 0.,.1,.2,.3,0.
MOMENT 1.2,2.6,2.6
MB 0.
RF 5.48333,6.8792,6.8792
VZ 0.
PZERO 35281.,4332.,4332.
VZERO 1.1614583,.4716435,.4716435
A .1134166,.2673611,.2673611

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174600000-19
11110000000044ORIGINAL PAGE IS
OF POOR QUALITY

REM	BCD	57.5	LANDING ROLL MANEUVER DATA
YSP		0.0	
TRV		0.0	
ICH		7.0	
TBK		0.0	
ISS		0.0	
ILR		0.0	
ISS		0.0	
REM	BCD	51.	ENGINE FAILURE STAGE DATA
IC	INT	0.0	
XRF1	INT	0.0	
IT1	INT	0.0	
XRF2	INT	0.0	
IT2	INT	0.0	
H1	INT	0.0	
IH1	INT	0.0	
H2	INT	0.0	
IH2	INT	0.0	
HR1	INT	0.0	
IHR1	INT	0.0	
HR2	INT	0.0	
IHR2	INT	0.0	
TR1	INT	0.0	
ITR1	INT	0.0	
TR2	INT	0.0	
ITR2	INT	0.0	
REM	BCD	50.	BRAKE COND. STAGE DATA
IB	INT	0.0	
TBK1	INT	0.0	
IBK1	INT	0.0	
TBK2	INT	0.0	
IBK2	INT	0.0	
REM	BCD	4K.	PITCH AUTOPILOT DATA
YST		0.0	
ALPOL		0.0	
RFALPH		0.0	
DELALA		0.0	
PSH.		0.0	
PSH2		0.0	
RFALP2		0.0	
DELQF		0.0	
DELQTO		0.0	
DELQQL		0.0	
DELQV		0.0	
DELFO1		0.0	
REM	BCD	4L.	YAW AUTOPILOT DATA
RFB		0.0	
DELBA		0.0	
PSI		0.0	
OPPSIA		0.0	
RFP		0.0	
PSI		0.0	
PSPSI		0.0	
DELRL		0.0	
DELRO		0.0	
REM	BCD	4M.	ROLL AUTOPILOT DATA
RFP		0.0	
PHI		0.0	
OPHIA		0.0	
PSA		0.0	
DELPL		0.0	
DELPU		0.0	
REM	BCD	5N.	THROTTLE AUTOPILOT DATA
TF	INT	0.0	
NOF	INT	0.0	
IR	INT	0.0	

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OF POOR QUALITY.

NB 1.1.
 NLR 0.1.
 NTO 1.1.
 K2 1.
 REM BCD 40. BRAKE AUTOPILOT DATA
 HBC 0.1.1.1.
 PD .1
 DELTAH .1
 OMECD1 2.
 MBL 1.1.1.1.
 MBU 1.1.1.1.
 REM BCD 50. CONTROL RESPONSE DATA
 DELHS 3.25
 DELRPO 31.5
 DELA 1.
 NED1 .1
 REM BCD 40. INITIALIZATION
 IAP 3
 HR 1.
 DELQD 4.55478
 DELQFE 4.55478
 DELQON 4.55478
 DELPD 4.
 DELRO 4.
 MANLOG 1
 PITCHP 1
 REM BCD 2 STAGING DATA
 REM BCD 44. GEARS INTO PROGRAM
 INDLG 1
 ISTAGE 1
 DECRES BCD 1HR
 STEST 11.
 TRA 1
 INDLG 1
 REM BCD 48. SMOOTH IMPACT STAGE
 AINCPS BCD 30DELTA1DELTA2DELTA3
 STEST -1.5, -1.5, -1.5
 TRA 1
 PRINT 1.2
 DELTS 1.5
 AMAXER 1.5
 PRMIN 1.
 AINCPS BCD 1 TIMES
 STEST .9
 TRA 1
 ATAB51 7.3516484E-3, 1.727972E-3
 ATAB52 -5.2147852E-4, 1.238928E-3
 ATAB53 -3.1368631E-4, 1.8265268E-3
 ATAB54 1.
 ATAB55 1.
 ATAB56 1.
 ATAB57 1.
 REM BCD 50. EFFICIENT AMAXER STAGE
 AINCPS BCD 40DELTA1DELTA2DELTA3
 STEST 1.1, 1.1
 TRA 1
 PRINT 1.5
 AMAXER 1.1
 DELTS 1.
 REM BCD 40. SMOOTH IMPACT STAGE
 AINCPS BCD 10DELTA1
 STEST -1.5
 TRA 1
 PRINT 1.2
 DELTS 1.5
 AMAXER 1.5
 REM BCD 5E. EFFICIENT AMAXER STAGE

AINCPS	BCD	1DELTA1
STEST		1
PRINT	TRA	
AMAXER		.05
DELTS		.01
INDSTF		1
	TRA	

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 7

A. GEARS INTO PROGRAM

INITIAL PRINT OUT FOR VPCS

XGGRF AREFF D1RFF D2RFF
B. 16.0500000E+02 37.7000000E+00 56.7000000E+00

PRINT CODES IDENTIFYING TIME HISTORY

2SDF							
TIME	TINES	XG77F	YG77F	HGC7F	U777F	V777F	W777F
PI77R	QI77R	RI77R	AI77F	VA77F	DYNPP	XG77F1	YG77F1
ZG77F1	ALPHD	BETAD	ALPHD1	BETAD1	GAH7D	SIG7D	THIPD
PSIPD	PHIPD	AX77F	AY77F	AZ77F	WTR7P	FDC	FCX
FCY	FCZ						
VPCS							
AMASS							
TFFS							
NT	NT						
SAC1							
CAVAH	CA	CN	CY	CL	CH	CNN	

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 8

2SDF

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	57.7454851E-01	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.	0.	0.	-31.6515539E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

TFFS

0. 0.

0.

0.

T(1)

SAC1

29.7745819E-03-20.8749533E-03 60.9750569E-02 0.

0.

15.3281670E-03 0.

FLARE

AUTS

ALPDES

PHIDES

TTD

11.5000000E+00 0.

0.

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

26.8544760E-01-14.0024531E-07 0.

0.

-14.0024531E-07 26.8544760E-01

INTEG RTN. HT = 1.0000000E-03

2SDF

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	90.1422983E-02	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.	0.	0.	-26.3302709E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 9

TFFS

0. 0.

0. 0.

T(II)

SAC1

29.7745819E-03-20.8749533E-03 60.9750569E-02 0.

0. 15.3281670E-03 0.

FLARE

AUTS

ALPOES

PHIDES

TTO

11.5000000E+00 0.

0.

PITCH AUTOPILOT

DELQW

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

27.5607208E-01-14.0024531E-07 0.

0.

-14.0024531E-07 27.5607208E-01

STAGE ON--DECR. HR

G-10

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 10

INDLG -1
REM BCD 48. SMOOTH IMPACT STAGE
AINCRS BCD 300ELT10DEL120DEL13
STEST -1.05,-1.05,-1.05
TRA

2SDF

0.	0.	0.	0.	0.	10.000000E+00	29.0274042E+01	0.	59.0569126E+00
0.	0.	0.	0.	26.5337670E-02	29.6220750E+01	10.4252977E+01	29.6159990E+01	0.
59.9992281E-01	11.4999986E+00	0.	0.	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.	90.1422983E-02	0.	0.	-26.3302709E+00	12.4671000E+04	0.	0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FG2

0.	35.2800000E+03	0.	0.	31.9713310E-01	-38.9549765E+02	-78.8562277E+01	0.
0.	40.3200000E+03	0.	0.	54.9315250E-01	-10.7799996E+03	-39.6383699E+01	0.
0.	40.3200000E+03	0.	0.	54.9315280E-01	-10.7799996E+03	-39.6383699E+01	0.

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HO

ODELTA

33.6000000E-02	29.6159990E+01	0.	0.	-0.	0.	0.	-79.6895154E-01
33.6000000E-02	29.6159990E+01	0.	0.	-0.	0.	0.	-10.9046626E-01
33.6000000E-02	29.6159990E+01	0.	0.	-0.	0.	0.	-10.9046626E-01

SD2

SD1

S

S202

S201

S2

ONETD1

ONET

0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.

FTRA

FTRB

FTRC

HTX

HTY

HTZ

FXH

FYH

0.	0.	0.	0.	0.	0.	0.	0.
----	----	----	----	----	----	----	----

FZH

LH

NH

NH

0.	0.	0.	0.
----	----	----	----

VPCS

38.7489900E+02

TFFS

0.	0.
----	----

ORIGINAL PAGE 10
OF FOUR CONTINUED

G-11

C-4

INDSO# 2 CASE LROLL STAGE 1 PAGE 11

0 0

29.7745819E-03 26.8749533E-03 50.9750569E-02 0. 0. 15.3281678E-03 0.

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01	0.	90.1259752E-02	0.	0.	0.	-28.9135646E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	-22.8050454E-04
20.0000000E-01	0.	10.1738888E-01	0.	0.	0.	-28.4544200E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	-13.3138408E-04
30.0000000E-01	0.	93.2368094E-02	0.	0.	0.	-25.1504011E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	15.1869517E-04
40.0000000E-01	0.	90.1270639E-02	0.	0.	0.	-24.3726223E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	-25.1618033E-04

AUTS

ALPDES RHIDES TTD

11.50000000E+00 0. 0.

PITCH AUTOPILOT

DELQD	ALPHA	ALPHD1	ALPOD1	ALPHET	DELQDE
339224E-01-14.0024531E-07	0.	0.	-14.0024531E-07	27.5339224E-01	

[illegible]

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INOSDF 2 CASE LROLL STAGE 1 PAGE 12

[illegible]

50.0000000E-03	50.0000000E-03	14.8031852E+00	0.	96.9255675E-01	29.0027316E+01	0.	59.3319886E+00
	27.2363829E-04	0.	26.5170101E-02	29.6034000E+01	10.4122497E+01	29.5967086E+01	0.
62.9389619E-01	11.5616896E+00	0.	12.6451556E-01	0.	-12.1824054E-01	0.	10.3434483E+00
0.		94.7824027E-02	0.	-26.7932210E+00	12.4671000E+04	0.	0.
0.							

LGEAR		P		P2	FT	SR	SF	AA	FG2
DELTA									
0.0	35.2800000E+03	0.0	0.0	0.0	31.5281571E-01	-38.9549765E+02	-78.8562277E+01	0.0	
0.0	40.3200000E+03	0.0	0.0	0.0	50.0377500E-01	-10.7799966E+03	-39.6383699E+01	0.0	
0.0	40.3200000E+03	0.0	0.0	0.0	50.0377500E-01	-10.7799966E+03	-39.6383699E+01	0.0	
HUVV		VGPT	FIRX	FIRY	FIRZ	HA	HB	ODELTA	

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 13

33.6000000E-02 29.5969707E+01 0. 0. -0. 0. 0. -76.6535562E-01
33.6000000E-02 29.5988319E+01 0. 0. -0. 0. 0. -76.1421176E-02
33.6000000E-02 29.5988319E+01 0. 0. -0. 0. 0. -78.1421176E-02

SD2 SD1 S S202 S201 S2 OHETD1 OHET
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
FYRA FYR8 FYR8 HTX HTY HTZ FXH FYH
0. 0. 0. 0. 0. 0. 0. 0.
FZH LH MM NH
-42.4553664E-02 0. -28.2129265E-01 0.

VPCS
38.7489960E+02
TFFS
0. 0.

0. 0. T(I)

SAC1
30.0142492E-03-21.9770041E-03 62.1246449E-02 0. 0. 12.2577435E-03 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01	0.	94.7399983E-02	0.	0.	-78.7375463E-04	-28.8634615E+00	0.
29.0027310E+01	0.	0.	-18.0259180E-05	59.2155997E+00	0.	0.	-22.8358789E-04
20.0000000E-01	0.	10.4017920E-01	0.	0.	-86.4746805E-04	-28.4983500E+00	0.
29.0032533E+01	0.	0.	-25.4280067E-05	59.2361801E+00	0.	0.	-13.3584997E-04
30.0000000E-01	0.	97.2561171E-02	0.	0.	86.0882860E-04	-26.6473508E+00	0.
29.0028708E+01	0.	0.	24.5483221E-05	59.3399656E+00	0.	0.	15.2296063E-04
40.0000000E-01	0.	94.7940137E-02	0.	0.	-11.6694376E-03	-25.2413997E+00	0.
29.0027309E+01	0.	0.	-32.9847765E-05	59.4197230E+00	0.	0.	-25.2189725E-04

AUTS

FLARE

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INSDOF 2 CASE LROLL STAGE 1 PAGE 14

PITCH AUTOPILOT

DELQN	ALPHA	ALPHD1	ALPDD1	ALPHET	DELQDE
28.3042261E-01	61.6896066E-03	12.6451556E-01	0.	61.6896066E-03	28.3042261E-01

[illegible]

ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 15

INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03
INTEG RTN. HT * 1.60000000E-03

2SDF

10.0000000E-02 10.0000000E-02 29.5966729E+00 0. 93.7100961E-01 28.9775565E+01 0. 59.6100276E+00
0. 48.1970865E-04 0. 26.5000397E-02 29.5844871E+01 10.3990475E+01 29.5772045E+01 0.
65.6392934E-01 11.6257341E+00 0. 12.9187211E-01 0. -12.7132816E-01 0. 10.3544047E+00
0. 0. 99.5792456E-02 0. -27.2803983E+00 12.4671000E+04 0.
0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2800000E+03 0. 0. 31.1245471E-01-38.9549765E+02-78.8562277E+01 0.
0. 40.3200000E+03 0. 0. 44.7702803E-01-10.7799936E+03-32.6383622E+01 0.
0. 40.3200000E+03 0. 0. 44.7795803E-01-10.7799936E+03-32.6383622E+01 0.

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DDelta

33.6000000E-02 29.5776613E+01 0. 0. -0. 0. 0. -73.5068539E-01
33.6000000E-02 29.5809666E+01 0. 0. -0. 0. 0. -45.9570722E-02
33.6000000E-02 29.5809666E+01 0. 0. -0. 0. 0. -45.9570722E-02

S02

S01

S

S202

S201

S2

ONETD1

OMET

0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.

FTRA

FTRB

FTRC

MTX

MTY

MTZ

FXH

FYH

0. 0. 0. 0. 0. 0. 0. 0.

FZH

LH

HM

NH

-35.6504747E-02 0. -20.5106175E-01 0.

VPCS

38.7489900E+02

TFFS

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 16

0.

0.

T(I)

SAC1

30.2764712E-03-23.1185515E-03 63.3345971E-02 0.

0.

90.5479575E-04 8.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01	0.	99.4715497E-02	0.	0.	-11.9553940E-03	-28.8144834E+00	0.
28.9775555E+01	0.	0.	-67.3748694E-05	59.4117120E+00	0.	0.	-22.2383148E-04
20.0000000E-01	0.	10.6329964E-01	0.	0.	-55.7195737E-04	-28.5376076E+00	0.
28.9734797E+01	0.	0.	-65.7138716E-05	59.4482792E+00	0.	0.	-13.5932157E-04
30.0000000E-01	0.	10.1409948E-01	0.	0.	70.7894062E-04	-27.1720620E+00	0.
28.9778029E+01	0.	0.	68.3612632E-05	59.6323928E+00	0.	0.	15.4653598E-04
40.0000000E-01	0.	99.6443108E-02	0.	0.	-11.9452926E-03	-26.1388568E+00	0.
28.9775553E+01	0.	0.	-96.6191198E-05	59.7728985E+00	0.	0.	-25.5428502E-04

AUTS

FLARL

ALPDES

PHIDES

YTD

11.5000000E+00 0.

0.

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

29.1249392E-01 12.5734134E-02 12.9187211E-01 0.

12.5734134E-02 29.1249392E-01

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 60

.. 2SQF ..
62.1000000E-02 52.1000000E-02 18.2779110E+01 0. 72.8272249E-01 28.8806318E+01 0. 47.6357052E+08
-13.4858293E-01 56.4265994E-03 0. 26.2189114E-02 29.2708473E+01 10.1803475E+01 29.2704376E+01 0.
0. 93.6603669E-01 0. 71.2729499E-01 0. 30.3127164E-02 0. 96.6916313E-01
0. 0. 66.6362676E-01 0. -51.6734069E+00 12.4671000E+04 0.

LGEAR
DELTA P P2 FT SR SF AA FC2
0. 35.2800000E+03 0. 0. -13.7733708E+00 -38.9549765E+02 -78.8562277E+01 0.
12.7645174E-02 27.4921410E+04 0. 61.2687173E+03 -23.5429745E+00 -60.0230698E+03 45.8028190E+00 12.2436086E+03
12.7645174E-02 27.4921410E+04 0. 61.2687173E+03 -23.5429745E+00 -60.0230698E+03 45.8028190E+00 12.2436086E+03

MUVP VGPT FTRX FTRY FTRZ MA MB DDELTA
33.6000000E-02 29.2578985E+01 0. 0. -0. -0. 0. -48.3607669E-01
30.4092281E-03 18.5297585E-02 18.9982668E+02 0. -62.4753341E+03 19.0667523E+02 0. 12.7645174E-02
30.4092281E-03 18.5297585E-02 18.9982668E+02 0. -62.4753341E+03 19.0667523E+02 0. 12.7645174E-02

SD2 SD1 S S202 S201 S2 ONETD1 ONET
0. 0. 0. 0. 0. 0. 0.
-93.5709199E-01 -53.8002798E-02 15.0535070E-01 0. 0. 0. 24.4445542E+01 -29.1620405E+01
-93.5709199E-01 -53.8002798E-02 15.0535070E-01 0. 0. 0. 24.4445542E+01 -29.1620405E+01

FTRA FTRB FTRC MYX HTY MTZ FXH FYH
24.7322454E+03 0. -12.2537435E+04 0. -19.8457137E+04 0. 24.7322454E+03 0.

FZH LH MH NM
-12.2866338E+04 0. -19.8660393E+04 0.

VPCS
38.7489900E+02

TFFS
0. 0.

T(I)
SAC1
32.1718773E-03 -66.6749403E-04 47.3336211E-02 0. 0. 17.5664726E-03 0.

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 61

FLEX		X02F		X02T		Y02F		Y02T		Z02F		Z02T		X01F	
POINT	X01T	Y01F		Y01T		Z01F		Z01T		X00F		Y00F		Z00F	
10.0000000E-01	0.	0.	55.5268978E-01	0.	0.	0.	0.	0.	0.	-16.5121023E-01	0.	0.	0.	0.	0.
20.0000000E-01	0.	0.	0.	0.	-22.1861114E-02	0.	49.8213808E+00	0.	0.	0.	0.	0.	0.	0.	57.4981987E-04
30.0000000E-01	0.	0.	54.7498952E-01	0.	0.	0.	0.	0.	0.	42.0178021E-01	0.	0.	0.	0.	0.
40.0000000E-01	0.	0.	0.	0.	-27.6628803E-02	0.	49.3387077E+00	0.	0.	0.	0.	0.	0.	0.	-35.9712350E-04
50.0000000E-01	0.	0.	66.1300747E-01	0.	0.	0.	0.	0.	0.	-35.2395110E-01	0.	0.	0.	0.	0.
60.0000000E-01	0.	0.	0.	0.	27.3391948E-02	0.	47.7489206E+00	0.	0.	0.	0.	0.	0.	0.	25.2143858E-04
70.0000000E-01	0.	0.	68.0873241E-01	0.	0.	0.	0.	0.	0.	18.1657989E-01	0.	0.	0.	0.	0.
80.0000000E-01	0.	0.	0.	0.	-37.2621386E-02	0.	45.4383256E+00	0.	0.	0.	0.	0.	0.	0.	22.5461521E-04

AUTS ISS = 1 LANDING ROLL ILS = 0 IBS = 1
TI TR
17.1000000E-02 45.0000000E-02

PITCH AUTOPILOT
DELQN ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
30.2904551E-01 21.0562305E-02 71.2729499E-01 0. 21.0562305E-02 43.4154551E-01
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SDF
64.1000000E-02 64.1000000E-02 18.8632797E+01 0. 73.1720146E-01 28.8876189E+01 0. 46.9789513E+00
0. -57.1559507E-03 0. 26.2155824E-02 29.2671273E+01 10.1777498E+01 29.2665267E+01 0.
-18.7493988E-01 92.3695293E-01 0. -57.4033255E-01 0. 36.7057615E-02 0. 96.0408937E-01
0. 0. 56.6626939E-01 0. -44.4350986E+00 12.4671000E+04 0.

LGEAR
DELTA P P2 FT SR SF AA FC2
0. 35.2800000E+03 0. 0. -50.3846829E-01 -38.9549765E+02 -78.8562277E+01 0.
10.8040762E-02 26.2146127E+04 0. 48.2893088E+03 -18.7230470E+00 -47.1486008E+03 41.9441613E+00 21.8810661E+03
10.8040762E-02 26.2146127E+04 0. 48.2893088E+03 -18.7230470E+00 -47.1486008E+03 41.9441613E+00 21.8810661E+03
HUVPT VGPT FTRX FTRY FTRZ MA MB DDELTA

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 62

33.6000000E-02 29.2556581E+01 0. 0. -0. 0. 0. -48.3416436E-01
46.7196987E-03 28.4648073E-02 23.0631456E+02 0. -49.3659847E+03 23.5984237E+02 0. 10.8040762E-02
46.7196987E-03 28.4648073E-02 23.0631456E+02 0. -49.3659847E+03 23.5984237E+02 0. 18.8040762E-02

SD2 SD1 S S2D2 S2D1 S2 QMETD1 QMET
0. 0. 0. 0. 0. 0. 0. 0.
-85.0194669E-01-71.9338843E-02 14.9274246E-01 0. 0. 0. 30.2543893E+01-28.6099297E+01
-85.0194669E-01-71.9338843E-02 14.9274246E-01 0. 0. 0. 30.2543893E+01-28.6099297E+01

FTRA FTRB FTRC MTX MTY MTZ FXH FYH
21.0201992E+03 0. -96.5786176E+03 0. -14.5350145E+04 0. 21.0201992E+03 0.
FZH LH MH NM
-96.7518145E+03 0. -14.4513744E+04 0.

VPCS
38.7489900E+02

TFFS
0. 0.

0. 0. T(I)

SAC1
32.1397969E-03-57.3016907E-04 46.1739396E-02 0. 0. 19.1822984E-03 1.

FLEX
POINT X02F X02T Y02F Y02T Z02F Z02T X01F
X01T Y01F Y01T Z01F Z01T Y01F Z01F Z01F
10.0000000E-01 0. 55.5512953E-01 0. 0. -85.6221848E-02-44.5733393E+00 0. 10.3160164E-04
28.6876130E+01 0. 0. -24.7228712E-02 49.1703784E+00 0. 70.8809723E-01-36.7628925E+00 0. 0.
20.0000000E-01 0. 55.3780864E-01 0. 0. 0. 0. 0. 0.
28.6876130E+01 0. 0. -15.9799290E-02 48.0243714E+00 0. 0. 0. 0.
30.0000000E-01 0. 56.4680386E-01 0. 0. 0. 0. 0. 0.
28.8846658E+01 0. 17.5349157E-02 46.9920536E+00 0. 0. 0. 0. 0.
40.0000000E-01 0. 58.0647899E-01 0. 0. 49.7240865E-01-40.0067841E+00 0. 0.
28.6876451E+01 0. 0. -30.1855626E-02 44.8290552E+00 0. 0. 0. -45.9903966E-04

AUTS ISS = 1 ILR = 1 LANDING ROLL ICS = 0 IBS = 1

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM
INOSOF 2 CASE LROLL STAGE 1 PAGE 63

TI TR
17.1000000E-02 47.0000000E-02

PITCH AUTOPILOT

DELQN	ALPHA	ALPHD1	ALPDD1	ALPHET	DELQDE
30.2904551E-01	21.0562305E-02	57.4033255E-01	0.	21.0562305E-02	44.4654551E-01
INTEG RYN.	HT = 1.0000000E-03				
INTEG RYN.	HT = 1.0000000E-03				
INTEG RYN.	HT = 1.0000000E-03				
INTEG RYN.	HT = 1.0000000E-03				

2SDF

66.1000000E-02	56.1000000E-02	19.4485748E+01	0.	73.5668916E-01	28.8023767E+01	0.	46.4726886E+00
0.	57.0831102E-03	0.	26.2125517E-02	29.2637398E+01	10.1753821E+01	29.2630235E+01	0.
-20.4744324E-01	91.3760574E-01	0.	-41.8943859E-01	0.	40.0874906E-02	0.	98.3848003E-01
0.	0.	44.2405800E-01	0.	-36.6295715E+00	12.4671000E+04	0.	0.
0.	0.						0.

LGEAR

DELTA	P	P2	FI	SR	SF	AA	FG2
0.	35.2800000E+03	0.	0.	15.5663885E-01	38.9549765E+02	78.8562277E+01	0.
84.4716219E-03	24.7555819E+04	0.	33.9887449E+03	11.0681952E+00	33.0135471E+03	35.8583052E+00	32.3567053E+03
84.4716219E-03	24.7555819E+04	0.	33.9887449E+03	11.0681952E+00	33.0135471E+03	35.8583052E+00	32.3567053E+03
MUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDELTA
33.6000000E-02	29.2544172E+01	0.	0.	-0.	0.	0.	-48.3437452E-01
69.4045752E-03	42.2823076E-02	24.2027139E+02	0.	-34.8719287E+03	25.3348777E+02	0.	84.4716219E-03
69.4045752E-03	42.2823076E-02	24.2027139E+02	0.	-34.8719287E+03	25.3348777E+02	0.	84.4716219E-03
S02	S01	S	S202	S201	S2	OMETD1	ONET
0.	0.	0.	0.	0.	0.	0.	0.
-69.3906943E-01	-87.4605015E-02	14.7675115E-01	0.	0.	0.	32.4806124E+01	-27.9759330E+01
-69.3906943E-01	-87.4605015E-02	14.7675115E-01	0.	0.	0.	32.4806124E+01	-27.9759330E+01
FTRA	FTRB	FTRC	MTX	MTY	MTZ	FXM	FYM
16.3308719E+03	0.	-67.9774897E+03	0.	-91.1973747E+03	0.	16.3308719E+03	0.
FZM	LH	NH	NM				
-68.0518879E+03	0.	-90.0487775E+03	0.				

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 64

VPCS
38.7489900E+02
TFFS

0. 0.

0.

0.

T(I)

SAC1
32.1021752E-03-49.7145925E-04 45.2378074E-02 0. 0. 20.5973651E-03 0.

FLEX

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01 0.	0.	43.1405729E-01 0.	0.	0.	93.1216294E-03-37.5039720E+00 0.	0.	0.
28.8923997E+01 0.	0.	0.	-25.5058622E-02 48.6530979E+00 0.	0.	0.	0.	-40.2296530E-04 0.
20.0000000E-01 0.	0.	43.5428973E-01 0.	0.	0.	72.5646112E-01-30.1749146E+00 0.	0.	0.
28.8314916E+01 0.	0.	0.	-11.4629069E-03 48.4638095E+00 0.	0.	0.	0.	-97.7647354E-04 0.
30.0000000E-01 0.	0.	44.3941309E-01 0.	0.	0.	-62.2838713E-01-42.7952486E+00 0.	0.	0.
28.8894145E+01 0.	0.	0.	49.5960439E-03 46.3601645E+00 0.	0.	0.	0.	93.4888925E-04 0.
40.0000000E-01 0.	0.	45.5085783E-01 0.	0.	0.	58.1095085E-01-30.0854216E+00 0.	0.	0.
28.8924312E+01 0.	0.	0.	-18.9711787E-02 44.4372115E+00 0.	0.	0.	0.	-95.4270896E-04 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IRS = 1

TI

TR

17.1000000E-02 49.0000000E-02

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHD1

ALPOD1

ALPHET

DELQDE

30.2904551E-01 21.0562305E-02-41.8943859E-01 0. 21.0562305E-02 45.5154551E-01

INTEG RTN.	HT	1.0000000E-03
INTEG RTN.	HT	1.0000000E-03
INTEG RTN.	HT	1.0000000E-03
INTEG RTN.	HT	1.0000000E-03

2SDF

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2		CASE LROLL		STAGE 1		PAGE 65	
68.1800000E-02	68.1000000E-02	20.0338011E+01	0.	73.9806348E-01	28.8945357E+01	0.	46.1213827E+00
0.	-56.2673687E-03	0.	26.2094874E-02	29.2803147E+01	10.1729880E+01	29.2595857E+01	0.
-20.6540383E-01	90.6903218E-01	0.	-27.0104488E-01	0.	40.4439562E-02	0.	94.7347042E-01
0.	0.	31.1047128E-01	0.	-29.3802070E+00	12.4671000E+04	0.	0.
0.	0.						
LGEAR							
DELTA	P	P2	FT	SR	SF	AA	FG2
0.	35.2800000E+03	0.	0.	50.8993891E-01	-38.9549765E+02	-78.8562277E+01	0.
59.3699438E-03	23.2387705E+04	0.	20.5367965E+03	-18.3524632E-01	-19.7584608E+03	28.6196270E+00	41.8045881E+03
59.3699438E-03	23.2387705E+04	0.	20.5367965E+03	-18.3524632E-01	-19.7584608E+03	28.6196270E+00	41.8045881E+03
HUVF VGPT FTRX FTRY FTRZ HA HB DDELTA							
33.6000000E-02	29.2529022E+01	0.	0.	-0.	0.	0.	-48.3402621E-01
10.5045531E-02	63.9888709E-02	22.2614815E+02	0.	-21.1922215E+03	23.8616380E+02	0.	59.3699438E-03
10.5045531E-02	63.9888709E-02	22.2614815E+02	0.	-21.1922215E+03	23.8616380E+02	0.	59.3699438E-03
SD2 SD1 S S2D2 S2D1 S2 ONETD1 ONET							
0.	0.	0.	0.	0.	0.	0.	0.
-49.5082768E-01	-99.4126820E-02	14.5799768E-01	0.	0.	0.	30.5918436E+01	-27.3382876E+01
-49.5082768E-01	-99.4126820E-02	14.5799768E-01	0.	0.	0.	30.5918436E+01	-27.3382876E+01
FYRA FTRB FTRC HIX HTY HTZ FXH FYH							
11.3676696E+03	0.	-41.0735930E+03	0.	-44.2983869E+03	0.	11.3676696E+03	0.
FZH LH MH NM							
-41.1296618E+03	0.	-43.5717616E+03	1.				
VPCS							
38.7489500E+02							
TFFS							
0.	0.						
	0.	0.					
T(I)							
SAC1							
32.0620812E-03	-43.8576472E-04	44.5328318E-02	0.	0.	21.7765091E-03	0.	
FLEX							

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01	0.	30.1022046E-01	0.	0.	11.1609250E-01	30.6812592E+00	0.
28.8945866E+01	0.	0.	-24.2988720E-02	48.2791369E+00	0.	0.	-90.3760999E-04
20.0000000E-01	0.	31.0285774E-01	0.	0.	47.2555612E-01	-26.6482506E+00	0.
28.8838000E+01	0.	0.	11.2232404E-02	48.2876011E+00	0.	0.	-86.8377466E-04
30.0000000E-01	0.	31.6352106E-01	0.	0.	-43.4668785E-01	33.5676925E+00	0.
28.8916168E+01	0.	0.	-59.2907243E-03	45.9023595E+00	0.	0.	91.8868697E-04
40.0000000E-01	0.	32.2977225E-01	0.	0.	42.6970401E-01	-23.2827640E+00	0.
28.8945046E+01	0.	0.	-85.5451789E-03	44.2165278E+00	0.	0.	-12.2431556E-03

AUTS ISS = 1 LANDING ROLL ICS = 0 IBS = 1
TI TR

17.1000000E-02 51.0000000E-02

PITCH AUTOPILOT

DELQN	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELQDE
30.2904551E-01	21.0562305E-02	27.0104488E-01	0.	21.0562305E-02	46.5654551E-01
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

2SDF

70.1000000E-02	70.1000000E-02	20.6189565E+01	0.	74.3841292E-01	28.8941098E+01	0.	45.9077102E+00
0.	-54.8628651E-03	0.	26.2661042E-02	29.2565336E+01	10.1703471E+01	29.2558837E+01	0.
-19.5010532E-01	90.2784131E-01	0.	-14.7967032E-01	0.	30.1910347E-02	0.	94.8975132E-01
0.	0.	19.2815667E-01	0.	-23.6696851E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	35.2800000E+03	0.	0.	58.2440808E-01	-38.9549765E+02	-78.8562277E+01	0.
35.6124928E-03	21.7647084E+04	0.	98.7090159E+02	71.9457304E-01	-92.7879364E+02	21.7719805E+00	48.5702127E+03
35.6124928E-03	21.7647084E+04	0.	98.7090159E+02	71.9457304E-01	-92.7879364E+02	21.7719805E+00	48.5702127E+03
HUVP	VGPT	FTRX	FTRY	FTRZ	MA	MB	DDelta
33.6000000E-02	29.2500585E+01	0.	0.	-0.	0.	0.	-48.3164983E-01
17.0336068E-02	10.3751425E-01	17.5381094E+02	0.	-10.2961807E+03	19.2154105E+02	0.	35.6124928E-03

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LRDL STAGE 1 PAGE 67

17.8336868E-02 10.3751425E-01 17.5381094E+02 0. -10.2961807E+03 19.2154105E+02 0. 35.6124928E-03

SD2 SD1 S S202 S201 S2 OMETD1 OMET

0. 0. 0. 0. 0. 0. 0. 0.

-27.7452443E-01 -10.7155487E-01 14.3726832E-01 0. 0. 0. 24.6351417E+01 -20.7793627E+01

-27.7452443E-01 -10.7155587E-01 14.3726832E-01 0. 0. 0. 24.6351417E+01 -20.7793627E+01

FTRA FTRB FTRC HTX HTY HT2 FXH FYH

68.2714937E+02 0. -19.7418032E+03 0. -11.5154201E+03 0. 68.2714937E+02 0.

FZH LH HH NH

-19.8355667E+03 0. -11.6689320E+03 0.

VPCS

38.7489900E+02

TFFS

0. 0.

0. 0.

T(I)

SAC1

32.0224504E-03 -39.4686348E-04 44.0341199E-02 0. 0. 22.9234748E-03 0.

FLEX

POINT XD2F XD2T YD2F YD2T ZD2F ZD2T XD1F

XD1T YD1F ZD1F ZD1T XD0F YD0F ZD0F

10.0000000E-01 0. 18.2175117E-01 0. 0. 20.9102745E-01 -25.0357766E+00 0.

28.8941844E+01 0. 0. -21.0716236E-02 48.0378114E+00 0. -13.6072333E-03

28.8941844E+01 0. 19.5908952E-01 0. 0. 59.8591028E-02 -25.9195283E+00 0.

28.8941844E+01 0. 0. 16.6804512E-02 47.9992851E+00 0. -57.5484668E-04

30.0000000E-01 0. 19.9121464E-01 0. 0. -11.0259732E-01 -24.5438097E+00 0.

28.8941844E+01 0. 0. -11.5103488E-02 45.6368692E+00 0. 73.3579884E-04

40.0000000E-01 0. 20.2748362E-01 0. 0. 13.8410579E-01 -19.6657362E+00 0.

28.8941844E+01 0. 0. -28.0889446E-03 44.1057238E+00 0. -13.2825042E-03

ISS = 1 ILR = 1 LANDING RCLL XCS = 0 IBS = 1

AUTS

TI TR

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 60

17.1000000E-02 53.0000000E-02

PITCH AUTOPILOT

DELQN	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELODE
30.2904551E-01	21.0562305E-02	14.7967032E-01	0.	21.0562305E-02	47.6154551E-01
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			

2SDF

72.1000000E-02	72.1000000E-02	21.2040327E+01	0.	74.7542945E-01	28.8914125E+01	0.	45.7973422E+00
0.	-53.0863490E-03	0.	26.2021718E-02	29.2521397E+01	10.1672814E+01	29.2516230E+01	0.
-17.3868925E-01	90.0732048E-01	0.	-64.4496734E-02	0.	34.0657391E-02	0.	93.4787725E-01
0.	0.	94.8981542E-02	0.	-20.0342280E+00	12.4671000E+04	0.	0.
0.	0.						

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FG2
0.	35.2800000E+03	0.	0.	50.0121961E-01	-38.9549765E+02	-78.8562277E+01	0.
15.9190494E-03	28.4009804E+04	0.	38.9238079E+02	14.2182114E+00	-26.3525381E+02	16.8086910E+00	51.7546643E+03
15.9190494E-03	28.4009804E+04	0.	38.9238079E+02	14.2182114E+00	-26.3525381E+02	16.8086910E+00	51.7546643E+03

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DOELTA
33.6000000E-02	29.2453501E+01	0.	0.	-0.	0.	0.	-48.2685087E-01
30.9166907E-02	18.8296542E-01	10.2088510E+02	0.	-33.0205166E+02	11.3862475E+02	0.	15.9190494E-03
30.9166907E-02	18.8296542E-01	10.2088510E+02	0.	-33.0205166E+02	11.3862475E+02	0.	15.9190494E-03

SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
0.	0.	0.	0.	0.	0.	0.	0.
-71.9837553E-02	-11.0612591E-01	14.1542292E-01	0.	0.	0.	14.5977532E+01	-26.3800210E+01
-71.9837553E-02	-11.0612591E-01	14.1542292E-01	0.	0.	0.	14.5977532E+01	-26.3800210E+01

FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYM
30.8735009E+02	0.	-61.8476158E+02	0.	31.7818191E+02	0.	30.8735009E+02	0.

FZX	LH	HH	NH
-63.2892699E+02	0.	21.2847142E+02	0.

VPCS

G-26

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 69

38.7489988E+02

TFFS

0.

0.

0.

0.

T(I)

SAC1

31.9856835E-03-36.1465821E-04 43.6925211E-02 0.

0.

23.9759425E-03 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01 0.	0.	84.4159485E-02 0.	0.	0.	28.8599596E-01-21.1458176E+00 0.	0.	0.
28.8915045E+01 0.	0.	-16.0538312E-02 0.	47.9018232E+00 0.	0.	-34.2081308E-01-26.7475141E+00 0.	0.	-17.3463346E-03 0.
20.0000000E-01 0.	0.	10.1490814E-01 0.	0.	0.	0.	0.	0.
28.8812513E-01 0.	0.	13.6949432E-02 0.	47.7967359E+00 0.	0.	0.	0.	-25.8240760E-04 0.
30.0000000E-01 0.	0.	10.1610754E-01 0.	0.	0.	22.4307192E-01-17.5266277E+00 0.	0.	0.
28.8886800E+01 0.	0.	-10.2747246E-02 0.	45.5439003E+00 0.	0.	0.	0.	50.4503111E-04 0.
40.0000000E-01 0.	0.	10.4182485E-01 0.	0.	0.	-12.4058721E-01-18.2454004E+00 0.	0.	0.
28.8914655E+01 0.	0.	0.	-28.3688291E-03 44.0525165E+00 0.	0.	0.	0.	-13.7588172E-03 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1000000E-02 55.0000000E-02

PITCH AUTOPILOT

DELQN	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELQDE
30.2904551E-01	21.0562305E-02-64.4496734E-02 0.	0.	21.0562305E-02	48.6654551E-01	0.

INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03

ZSOF

74.1000000E-02	74.1000000E-02	21.7890152E+01	0.	75.0760205E-01	28.8867936E+01	0.	45.7495777E+00
0.	-51.1846291E-03	0.	26.1974188E-02	29.2468303E+01	10.1635813E+01	29.2464591E+01	0.
-14.7335364E-01	89.9949525E-01	0.	-20.2652544E-02	0.	28.8637872E-02	0.	92.8813269E-01

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 70

0.	0.	19.4616585E-02	0.	-18.4348846E+00	12.4671000E+04	0.	0.
0.	0.						
LGEAR							
DELTA	P	P2	FT	SR	SF	AA	FG2
0.	35.2800000E+03	0.	0.	42.0910053E-01	-38.9549765E+02	-78.8562277E+01	0.
22.7350573E-04	19.1824278E+04	0.	19.7117005E+01	18.0079330E+00	20.2133597E+01	14.6805586E+00	51.4780641E+03
22.7350573E-04	19.1824278E+04	0.	19.7117005E+01	18.0079330E+00	20.2133597E+01	14.6805586E+00	51.4780641E+03
HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDELTA
33.6000000E-02	29.2387335E+01	0.	0.	-0.	0.	0.	-48.1984096E-01
33.6000000E-02	39.4362741E-01	71.0134318E+00	0.	-21.1349499E+01	80.1724953E+00	0.	22.7350573E-04
33.6000000E-02	39.4362741E-01	71.0134318E+00	0.	-21.1349499E+01	80.1724953E+00	0.	22.7350573E-04
S02	S01	S	S202	S201	S2	CHET01	CHET
0.	0.	0.	0.	0.	0.	0.	0.
93.6319448E-02	-11.0316613E-01	13.9327536E-01	0.	0.	0.	10.2785250E+00	-26.2409724E+01
93.6319448E-02	-11.0316613E-01	13.9327536E-01	0.	0.	0.	10.2785250E+00	-26.2409724E+01
FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYH
20.8388145E+01	0.	-39.4234010E+01	0.	29.1390079E+01	0.	20.8388145E+01	0.
FZH	LH	NH	NH				
-55.5344764E+01	0.	-12.4452784E+02	0.				
VPCS							
38.7489900E+02							
TFFS							
0.	0.						
	0.	0.					
SAC1							
31.9534011E-03	-33.4547018E-04	43.4495910E-02	0.	0.	24.9669689E-03	0.	
FLEX							
POINT	X02F	X02T	Y02F	Y02T	Z02F	Z02T	X01F
X01T	Y01F	Y01T	Z01F	Z01T	X00F	Y00F	Z00F

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 71

18.0000000E-01	0.	90.8816942E-03	0.	0.	33.9660769E-01	19.1871411E+00	0.
28.8868956E+01	0.	0.	-97.1753056E-03	47.8362816E+00	0.	0.	-19.9405308E-03
20.0000000E-01	0.	28.1179494E-02	0.	0.	-57.5817940E-01	27.5437667E+00	0.
28.8769868E+01	0.	0.	41.3794566E-03	47.5856828E+00	0.	0.	-72.0753294E-05
10.0000000E-01	0.	25.4400544E-02	0.	0.	44.2194227E-01	13.7435706E+00	0.
28.8841668E+01	0.	0.	-33.2791408E-03	45.5710022E+00	0.	0.	36.1168418E-04
40.0000000E-01	0.	28.4786366E-02	0.	0.	-22.9601776E-01	17.6474718E+00	0.
28.8868687E+01	0.	0.	-67.0176127E-03	44.0275921E+00	0.	0.	-14.6772642E-03

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1000000E-02 57.0000000E-02

PITCH AUTOPILOT

DELQW

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

30.2904551E-01 21.0562305E-02 20.2652544E-02 0.

21.0562305E-02 49.7154551E-01

INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 168

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1000000E-02 18.6500000E-01

PITCH AUTOPILOT

DELQN

ALPHA

ALPHD1

ALPDD1

ALPHET

DELCOE

30.2904551E-01 21.0562305E-02 11.2001149E+00 0.

21.0562305E-02 80.0000000E-01

INTEG RTN. HT = 2.5000000E-04
INTEG RTN. HT = 2.5000000E-04
INTEG RTN. HT = 2.5000000E-04
INTEG RTN. HT = 1.0000000E-03

2SDF

20.5600000E-01 20.5600000E-01 60.0558263E+01 0. 69.8582643E-01 28.9898420E+01 0. 68.8864251E-01
0. -18.9545803E-02 0. 25.9737925E-02 28.9972256E+01 99.9099364E+00 28.9972169E+01 0.
22.3968586E-02 13.6125877E-01 0. -11.0690466E+00 0. -44.2537658E-03 0. 13.1700469E-01
0. 0. -13.4296059E-01 0. -33.2703044E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FG2

80.5768843E-03 57.7573627E+03 0. 12.5937250E+03 -21.8992590E-01 -12.4574103E+03 27.5940712E+00 -56.8886435E+02
13.2145748E-02 24.2445669E+04 0. 62.5906232E+03 -24.0574809E-01 -64.6553364E+03 34.0241660E+00 27.2831988E-03
13.2145748E-02 24.2445669E+04 0. 65.5906232E+03 -24.0574809E-01 -64.6553364E+03 34.0241660E+00 27.2831988E-03

HUVP

VGPT

FTRX

FTRY

FTRZ

NA

HB

ODELTA

33.6000000E-02 15.1919634E+01 -42.0016480E+02 0. -12.5004909E+03 -40.6298664E+02 0. 80.5768843E-03
66.7951319E-05 40.1944847E-04 43.8236129E+00 0. -65.6089922E+03 43.7843580E+00 0. 13.2145748E-02
66.7951319E-05 40.1944847E-04 43.8236129E+00 0. -65.6089922E+03 43.7843580E+00 0. 13.2145748E-02

SD2

SD1

S

S2D2

S2D1

S2

OHETD1

OHET

-67.6135543E-01 64.4911174E-01 56.9067789E-02 0. 0. 0. -16.9291110E+02 -14.1374776E+01
-54.7082747E-02 -80.3114502E-05 14.7069520E-01 0. 0. 0. 56.1337923E-01 -28.9106680E+01
-54.7082747E-02 -80.3114502E-05 14.7069520E-01 0. 0. 0. 56.1337923E-01 -28.9106680E+01

FTRA

FTRB

FTRC

HTX

HTY

HTZ

FYM

FYM

-80.5194431E+01 0. -14.3775031E+04 0. 57.1514116E+03 0. -80.8117431E+01 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 169

FZN LM NM NH
-14.3764578E+04 0. 58.6658510E+03 0.
VPCS
38.7489900E+02
TFFS
0. 0.

SAC1
32.457915E-03 27.4118354E-03-92.5789338E-03 0. 0. 66.9564147E-04 0.
T(12)

FLEX

POINT XD1T	X02F YD1F	X02T YD1T	Y02F ZD1F	Y02T ZD1T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01 0.	-27.8100931E-01 0.	-25.1302864E-02 14.7246336E+00 0.	73.2466986E-02-35.1866044E+00 0.	-64.9008250E-04 0.			
20.9891620E+01 0.	-23.8441773E-01 0.	-26.4528194E-02 13.2740066E+00 0.	11.6101687E-01-34.3553352E+00 0.	-42.8610081E-04 0.			
20.0000000E-01 0.	-13.1235292E-01 0.	27.2550735E-02 66.2313526E-01 0.	-16.5895315E-01-34.5713398E+00 0.	49.5494215E-04 0.			
28.9527936E+01 0.	-41.3389721E-03 0.	-37.0449874E-02 38.9551328E-02 0.	88.0249904E-02-30.3827894E+00 0.	-75.8785089E-04 0.			
30.0000000E-01 0.							
28.9792892E+01 0.							
40.0000000E-01 0.							
28.9891859E+01 0.							

AUTS

ISS = 1

LANDING ROLL
ILR = 1 ICS = 0

IRS = 2

TI TR

17.1000000E-02 18.8500000E-01

PITCH AUTOPILOT

DELQN	ALPHA	ALPHD1	ALPHD01	ALPHET	DELQDE
30.2904551E-01	21.0562305E-02	11.0698466E+00	0.	21.0562305E-02	80.0000000E-01
INTEG RTN.	HT = 1.00000000E-03				
INTEG RTN.	HT = 1.00000000E-03				
INTEG RTN.	HT = 1.00000000E-03				

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LRGLL STAGE 1 PAGE 170

INTEG RTN. HT = 1.0000000E-03

2SOF

20.7600000E-01 20.7600000E-01 60.6357278E+01 0. 69.8153584E-01 28.9871610E+01 0. 57.7521060E-01
0. -18.8131124E-02 0. 25.9699296E-02 28.9929135E+01 99.8802363E+00 28.9929061E+01 0.
20.6439997E-02 11.4137229E-01 0. -10.9094654E+00 0. -40.7963984E-03 0. 11.0057562E-01
0. 0. -15.7390292E-01 0. -32.8715348E+00 12.4671000E+04 0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
65.3360411E-03	67.3985421E+03	0.	13.4842700E+03	62.3100504E-02	-13.3532419E+03	26.5239060E+00	-54.8689690E+02
13.1761197E-02	24.1933709E+04	0.	65.3259927E+03	-45.9633301E-01	-64.3828685E+03	34.6789490E+00	16.7765392E+01
13.1761197E-02	24.1933709E+04	0.	65.3259927E+03	-45.9633301E-01	-64.3828685E+03	34.6789490E+00	16.7765392E+01

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.6000000E-02	11.8984584E+01	-45.0248757E+02	0.	-13.4002606E+03	-43.3400746E+02	0.	85.3360411E-03
11.5232725E-04	69.3338436E-04	75.2924778E+00	0.	-65.3394927E+03	75.2539885E+00	0.	13.1761197E-02
11.5232725E-04	69.3338436E-04	75.2924778E+00	0.	-65.3394927E+03	75.2539885E+00	0.	13.1761197E-02

SD2	SD1	S	S202	S201	S2	ONETD1	ONET
-50.2105806E-01	63.3359826E-01	69.6837200E-02	0.	0.	0.	-18.0583644E+02	-17.6282871E+01
-20.6544849E-01	62.9768601E-03	14.7007438E-01	0.	0.	0.	96.4794725E-01	28.8963624E+01
-20.6544849E-01	62.9768601E-03	14.7007438E-01	0.	0.	0.	96.4794725E-01	28.8963624E+01

FTRA	FTRB	FTRC	MTX	MTY	MTZ	FXH	FYM
-15.8369952E+02	0.	-14.4136255E+04	0.	85.3734572E+03	0.	-15.8369952E+02	0.

FZH	LH	HH	NH
-14.4072155E+04	0.	87.2904808E+03	0.

VPCS

38.7489900E+02

TFFS

0. 0.

0. 0.

SAC1

T(1)

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 171

32.4623042E-03 28.1646597E-03-10.4164804E-02 0. 0. 69.9576766E-04 0.

FLEX

POINT XD1T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01 0.	-29.9912126E-01 0.	0.	0.	14.8415603E-01-34.8490321E+00 0.	-11.3079475E-03 0.		
28.9873737E+01 0.	-22.8072991E-02 13.5740718E+00 0.	0.	0.	42.4099548E-01-31.5447702E+00 0.	-91.1066712E-04 0.		
20.0000000E-01 0.	-25.8268568E-01 0.	0.	0.	0.	0.		
28.9512738E+01 0.	-20.7745407E-02 12.1677258E+00 0.	0.	0.	41.0533432E-01-36.7645967E+00 0.	99.0841672E-04 0.		
30.0000000E-01 0.	-15.1183179E-01 0.	0.	0.	0.	0.		
28.9773877E+01 0.	21.4069933E-02 54.5523835E-01 0.	0.	0.	40.4297015E-01-26.2052852E+00 0.	-14.5846683E-03 0.		
40.0000000E-01 0.	-31.0750644E-02 0.	0.	0.	0.	0.		
28.9874353E+01 0.	0.	-31.8800895E-02-62.6490357E-02 0.	0.	0.	0.		

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1000000E-02 19.0500000E-01

PITCH AUTOPILOT

DELQN	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELODE
30.2904551E-01	21.0562305E-02-10.9094654E+00 0.	0.	0.	21.0562305E-02 80.0000000E-01	0.

INTEG RTN.	HT = 1.0000000E-03
INTEG RTN.	HT = 1.0000000E-03
INTEG RTN.	HT = 1.0000000E-03
INTEG RTN.	HT = 1.0000000E-03

2SDF

20.9600000E-01 0.	20.9600000E-01 61.2155413E+01 0.	0.	69.7750789E-01 28.9846382E+01 0.	46.8069213E-01 0.
0.	-18.6223648E-02 0.	25.9659019E-02 28.9884173E+01 0.	99.8492722E+00 28.9884106E+01 0.	0.
19.8096676E-02 0.	92.5161794E-02 0.	-10.6964896E+00 0.	-39.1535494E-03 0.	88.6027865E-02 0.
0.	0.	-18.0076757E-01 0.	-32.3472055E+00 12.4671000E+04 0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
92.3189464E-03 0.	80.6403649E+03 0.	0.	14.8144553E+03 19.2100755E-01-14.6920229E+03 24.7834947E+00-53.1558888E+02	0.	0.	0.	0.
13.0631892E-02 0.	24.0503275E+04 0.	0.	64.5392323E+03-54.6726326E-01-63.6030389E+03 34.3946861E+00 57.8276817E+01	0.	0.	0.	0.
13.0631892E-02 0.	24.0503275E+04 0.	0.	64.5392323E+03-54.6726326E-01-63.6030389E+03 34.3946861E+00 57.8276817E+01	0.	0.	0.	0.

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2		CASE LROLL		STAGE 1	PAGE	172		
HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DELTA	
33.6000000E-02	84.2040648E+00	-49.5251720E+02	0.	-14.7396345E+03	-47.3261431E+02	0.	92.3109464E-03	
29.8840476E-04	17.9786570E-03	19.2901328E+01	0.	-64.5499333E+03	19.3020562E+01	0.	13.8631892E-02	
29.8840476E-04	17.9786570E-03	19.2901328E+01	0.	-64.5499333E+03	19.3020562E+01	0.	13.8631892E-02	
S02	S01	S	S202	S201	S2	OMETDI		OMET
-54.6525076E-01	62.3394221E-01	82.2526807E-02	0.	0.	0.	-19.7192263E+02		-21.3960995E+01
-32.4273026E-01	-11.6922396E-02	14.6832580E-01	0.	0.	0.	24.7462259E+00		-28.8614233E+01
-32.4273026E-01	-11.6922396E-02	14.6832580E-01	0.	0.	0.	24.7462259E+00		-28.8614233E+01
FTRA	FTRB	FTRC	HTX	NTY	HTZ	FXH		FYH
-23.4190824E+02	0.	-14.3892920E+04	0.	13.2102839E+04	0.	-23.4190824E+02		0.
FZH	LH	NH	NH					
-14.3822027E+04	0.	13.4466675E+04	0.					
VPCS								
38.7489900E+02								
TFFS								
0.	0.							
0.	0.							
T(I)								
SAG1								
32.4563981E-03	28.9276047E-03	-11.5433597E-02	0.	0.	72.7244510E-04	0.		
FLEX								
POINT	XD2F	XD2I	YD2F	YD2I	ZD2F	ZD2I	XD1F	
XD1I	YD1F	YD1I	ZD1F	ZD1I	XD0F	YD0F	ZD0F	
10.0000000E-01	0.	-32.1093557E-01	0.	0.	21.9722225E-01	-34.9114062E+00	0.	
28.9849273E+01	0.	0.	-19.1209170E-02	12.4350315E+00	0.	0.	-15.5248707E-03	
20.0000000E-01	0.	-27.6678548E-01	0.	0.	60.7885252E-01	-38.2490948E+00	0.	
28.9491737E+01	0.	0.	-10.1763998E-02	11.1122683E+00	0.	0.	-12.2679171E-03	
30.0000000E-01	0.	-15.8663246E-01	0.	0.	-55.9463843E-01	-37.6374850E+00	0.	
28.9749019E+01	0.	0.	11.4683733E-02	42.6674837E-01	0.	0.	13.2463200E-03	
40.0000000E-01	0.	-50.2424231E-02	0.	0.	63.2080283E-01	-22.4094949E+00	0.	
28.9850102E+01	0.	0.	-21.2864052E-02	-15.5339702E-01	0.	0.	-19.9783512E-03	
ISS = 1 ILR = 1 LANDING ROLL ICS = 0 IBS = 1								

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 173

AUTS

TI

TR

17.1000000E-02 19.2500000E-01

PITCH AUTOPILOT

DELQD	ALPHA	ALPHD1	ALPDD1	ALPHET	DELQDE
30.2904551E-01	21.0562305E-02	-10.6964896E+00	0.	21.0562305E-02	00.0000000E-01
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

2SDF

21.1225000E-01	21.1225000E-01	61.6865721E+01	0.	69.7428317E-01	28.9820790E+01	0.	38.8997490E-01
0.	-18.4135362E-02	0.	25.9624672E-02	28.9845832E+01	99.8228702E+00	28.9845762E+01	0.
20.0298634E-02	75.3165115E-02	0.	-10.4671402E+00	0.	-39.5934277E-03	0.	71.3578731E-02
0.	0.	-20.3138247E-01	0.	-31.7834531E+00	12.4671000E+04	0.	0.
0.	0.						

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
10.0110762E-02	95.6647080E+03	0.	16.3263697E+03	13.2461524E-01	-16.2171679E+03	22.1056180E+00	-51.2816563E+02
12.8999996E-02	23.8626118E+04	0.	63.4056455E+03	-48.5601011E-01	-62.4837480E+03	33.8984384E+00	12.0940879E+02
12.0999996E-02	23.8626118E+04	0.	63.4056455E+03	-48.5601011E-01	-62.4837480E+03	33.8984384E+00	12.0940879E+02

MUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDELTA
33.6000000E-02	54.1337201E+00	-54.6322310E+02	0.	-16.2595926E+03	-51.7807530E+02	0.	10.0110762E-02
42.9115000E-04	25.8138133E-03	27.2118782E+01	0.	-63.4139524E+03	27.2731050E+01	0.	12.8999996E-02
42.9115000E-04	25.8138133E-03	27.2118782E+01	0.	-63.4139524E+03	27.2731050E+01	0.	12.8999996E-02

SD2	SD1	S	S202	S201	S2	OMETD1	OHET
-87.4127159E-01	61.2305463E-01	92.2998990E-02	0.	0.	0.	-21.5753137E+02	-24.7441046E+01
-31.2907655E-01	-16.9089398E-02	14.6599933E-01	0.	0.	0.	34.9655192E+00	-28.8125009E+01
-31.2907655E-01	-16.9089398E-02	14.6599933E-01	0.	0.	0.	34.9655192E+00	-28.8125009E+01

FTRA	FTRB	FTRC	MTX	HTY	HTZ	FXH	FYM
-31.3661573E+02	0.	-14.3137661E+04	0.	18.6781461E+04	0.	-31.3661573E+02	0.
FZH	LH	NH	NH				

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 174

-14.3074474E+04 0.

10.9752814E+04 0.

VPQS

38.7489900E+02

TFFS

0.

0.

0.

0.

T(I)

SAC1

32.4703842E-03 29.5525780E-03-12.4313683E-02 0.

0.

74.7971731E-04 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.0000000E-01 0.	0.	-34.2507323E-01 0.	0.	0.	27.3302231E-01-35.3269603E+00 0.	0.	0.
26.9824163E+01 0.	0.	0.	-15.1122214E-02 0.	11.5153010E+00 0.	0.	0.	-18.3181017E-03 0.
20.0000000E-01 0.	0.	-29.4069340E-01 0.	0.	0.	61.6251319E-01-30.8468917E+00 0.	0.	0.
28.9470275E+02 0.	0.	0.	-51.8039650E-05 0.	10.2695324E+00 0.	0.	0.	-13.1007953E-03 0.
30.0000000E-01 0.	0.	-18.6614672E-01 0.	0.	0.	-56.4438719E-01-37.0275326E+00 0.	0.	0.
26.3724314E+01 0.	0.	0.	21.9581767E-03 0.	33.0923355E-01 0.	0.	0.	14.3576024E-03 0.
40.0000000E-01 0.	0.	-90.0224965E-02 0.	0.	0.	69.0878087E-01-20.1182484E+00 0.	0.	0.
26.9824945E+01 0.	0.	0.	-10.3698942E-02-22.4742796E-01 0.	0.	0.	0.	-22.5633879E-03 0.

AUTS

ISS = 1

LANDING ROLL
ILR = 1

IGS = 0

IBS = 1

TI

TR

17.1000000E-02 19.4125000E-01

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

30.2904551E-01 21.0562305E-02-10.4671402E+00 0.

21.0562305E-02 80.0000000E-01

STAGE ON--INCR. DELTA1

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 175

PRINT .05
ANAXER .01
DELTS .01
INDSTF 1

TRA

2SDF

21.1225000E-01 21.1225000E-01 61.6865721E+01 0. 59.7428317E-01 28.9820790E+01 0. 38.0997490E-01
0. -18.4135362E-02 0. 25.9624672E-02 28.9845832E+01 99.8228702E+00 28.9845762E+01 0.
20.0298634E-02 75.3165115E-02 0. -10.4671402E+00 0. -39.5934277E-03 0. 71.3570731E-02
0. 0. -20.3136247E-01 0. -31.7634531E+00 12.4671000E+04 0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
10.0118762E-02	95.6647080E+03	0.	16.3263697E+03	13.2461524E-01	-16.2171679E+03	22.1056180E+00	-51.2816563E+02
12.8999999E-02	23.8626118E+04	0.	63.4056495E+03	-48.5601011E-01	-62.4837480E+03	33.8984384E+00	12.0940879E+02
12.8999999E-02	23.8626118E+04	0.	63.4056495E+03	-48.5601011E-01	-62.4837480E+03	33.8984384E+00	12.0940879E+02

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.6000000E-02	54.1337201E+00	-54.6322310E+02	0.	-16.2595926E+03	-51.7807530E+02	0.	10.0110762E-02
42.9115000E-04	25.8138133E-03	27.2118782E+01	0.	-63.4139924E+03	27.2731050E+01	0.	12.8999999E-02
42.9115000E-04	25.8138133E-03	27.2118782E+01	0.	-63.4139924E+03	27.2731050E+01	0.	12.8999999E-02

SD2	SD1	S	S2D2	S2D1	S2	ONETD1	ONET
-47.4127159E-01	61.2305463E-01	92.2998990E-02	0.	0.	0.	-21.5753137E+02	-24.7441846E+01
-31.2907655E-01	16.9089338E-02	14.6599933E-01	0.	0.	0.	34.9655132E+00	-28.8126009E+01
-31.2907655E-01	16.9089338E-02	14.6599933E-01	0.	0.	0.	34.9655132E+00	-28.8126009E+01

FTRA	FTRB	FTRC	NTX	NTY	NTZ	FXH	FYH
-31.3661573E+02	0.	-14.3137661E+04	0.	18.6781461E+04	0.	-31.3661573E+02	0.

FZH	LH	MH	NH
-14.3074474E+04	0.	18.9752814E+04	0.

VPCS

38.7489900E+02

TFFS

0. 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 176

0. 0. T(1)

SAC1
32.4703842E-03 29.5525780E-03-12.4313683E-02 0. 0. 74.7971731E-04 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.8000000E-01	0.	-34.2507323E-01	0.	0.	27.3302231E-01	-35.3269603E+00	0.
22.9824163E+01	0.	0.	-15.1122214E-02	11.5151010E+00	0.	0.	-18.3181017E-03
20.0000000E-01	0.	-29.4069340E-01	0.	0.	61.6251319E-01	-30.8468917E+00	0.
28.9470275E+01	0.	0.	-51.0639650E-05	10.2695324E+00	0.	0.	-13.1007953E-03
30.0000000E-01	0.	-18.6614672E-01	0.	0.	-56.4438719E-01	-37.0275326E+00	0.
28.972431E+01	0.	0.	21.9581767E-03	33.0923355E-01	0.	0.	14.3576024E-03
40.0000000E-01	0.	-90.0224965E-02	0.	0.	69.0878087E-01	-20.1182484E+00	0.
28.3824942E+01	0.	0.	-10.3698942E-02	-22.4742796E-01	0.	0.	-22.5633879E-03

AUTS ISS = 1 LANDING ROLL ILR = 1 ICS = 0 IOS = 1

TI TR
17.1000000E-02 19.4125000E-01

PITCH AUTOPILOT

DELQN	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELQDE
30.2904551E-01	21.0562305E-02	-10.4671402E+00	0.	21.0562305E-02	80.0000000E-01
INTEG RTN.	HT = 4.0000000E-03				
INTEG RTN.	HT = 2.0000000E-03				
INTEG RTN.	HT = 2.0000000E-03				
INTEG RTN.	HT = 4.0000000E-03				
INTEG RTN.	HT = 2.0000000E-03				

2SDF

21.6225000E-01	21.6225000E-01	63.1355141E+01	0.	69.6309417E-01	26.9742110E+01	0.	12.7161591E-01
0.	-17.1755978E-02	0.	25.9534255E-02	28.9744901E+01	99.7533936E+00	28.9744788E+01	0.
25.5905159E-02	25.1457261E-02	0.	-95.8483130E-01	0.	-50.6038955E-03	0.	20.0853135E-02
0.	0.	-14.4452442E-01	0.	-30.8862039E+00	12.4671000E+04	0.	0.
0.	0.						

LGEAR

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

DELTA		P	INDSOF	2	CASE	LRLL	STAGE	1	PAGE	177	AA	FC2
			P2	FT	SR	SF	HA	HB	ODELTA			
14.6814006E-02	20.3337994E+04	0.	25.6883556E+03	-11.8427474E+00	-25.7483637E+03	-12.1473877E+00	-31.4896887E+02					
12.2365438E-02	22.9620854E+04	0.	58.8556558E+03	10.7801140E-01	-58.0360320E+03	30.1378031E+00	33.0985029E+02					
12.2365438E-02	22.9620854E+04	0.	58.8556558E+03	10.7801140E-01	-58.0360320E+03	30.1378031E+00	33.0985029E+02					
HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA					
60.9390613E-03	36.6507299E-02	-15.6509955E+02	0.	-25.6883556E+03	-14.1156750E+02	0.	14.6014006E-02					
42.7635998E-04	25.7225288E-03	25.1693291E+01	0.	-58.8556558E+03	25.3929475E+01	0.	12.2365438E-02					
42.7635998E-04	25.7225288E-03	25.1693291E+01	0.	-58.8556558E+03	25.3929475E+01	0.	12.2365438E-02					
SD2	SD1	S	S2D2	S2D1	S2	OMETO1	OMET					
-56.1639374E+00	47.9812150E-01	12.0855563E-01	0.	0.	0.	-58.8153125E+01	-31.9680913E+01					
-95.7987792E-02	27.9726745E-02	14.5430963E-01	0.	0.	0.	-32.5550610E+00	-28.6205421E+01					
-95.7987792E-02	27.9726745E-02	14.5430963E-01	0.	0.	0.	-32.5550610E+00	-28.6205421E+01					
FTRA	FTRB	FTRC	MTX	HTY	HTZ	FXH	FYH					
-55.9022944E+01	0.	-14.3399667E+04	0.	56.2508115E+04	0.	-55.9022944E+01	0.					
FZH	LH	MH	NH									
-14.3661408E+04	0.	57.2392094E+04	0.									
VPCS												
38.7489900E+02												
TFFS												
0.	0.											
SAC1												
32.4793797E-03	31.4672880E-03	-14.9780982E-02	0.	0.	80.1784893E-04	0.						
FLEX												
POINT	XD2F	XD2T	YD2F	YD2T	ZD2F	ZD2T	XD1F					
XD1T	YD1F	YD1T	ZD1F	ZD1T	XD0F	YD0F	ZD0F					
10.0000000E-01	0.	-27.1999248E-01	0.	0.	42.2145578E-01	-43.2499766E+00	0.					
28.9745862E+01	0.	0.	24.1751114E-03	86.2405180E-01	0.	0.	-21.8437785E-03					
20.0000000E-01	0.	-18.0211719E-01	0.	0.	56.4091431E-02	-44.0160941E+00	0.					
28.9414152E+01	0.	0.	18.8819091E-02	74.8620150E-01	0.	0.	-72.2893881E-04					
30.0000000E-01	0.	-11.0123624E-01	0.	0.	-12.9864936E-01	-31.0964496E+00	0.					

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ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 178

28.9652899E+01 0. 0. -16.7814201E-02 61.6243171E-02 0. 0. 98.2168362E-04
40.0000000E-01 0. -55.5159561E-02 0. 0. 29.6758905E-01-15.3501442E+00 0.
28.9745585E+01 0. 0. 16.4788776E-02-41.1713287E-01 0. 0. -20.2315289E-03

ISS = 1 LANDING ROLL ICS = 0 IHS = 1

AUTS

TI

TR

17.1000000E-02 19.9125000E-01

PITCH AUTOPILOT

DELQH ALPHAE ALPHD1 ALPDD1 ALPHET DELQOE
30.2904551E-01 21.0562305E-02-95.8483190E-01 0. 21.0562305E-02 00.0000000E-01
INTEG RTN. HT = 4.0000000E-03
INTEG RTN. HT = 4.0000000E-03
INTEG RTN. HT = 4.0000000E-03
TIRE DEFLECTION EXCEEDED DELTA(1) = 2.0053015E-01

2SDF

21.8625000E-01 21.8625000E-01 63.8308523E+01 0. 69.5670893E-01 28.9781378E+01 0. 12.8493429E-02
0. -15.9598999E-02 0. 25.9495290E-02 28.9701406E+01 99.7234660E+00 28.9701285E+01 0.
25.8558518E-02 25.4128260E-03 0. -92.8086251E-01 0. -53.1131020E-03 0. -27.7014395E-03
0. 0. -21.1186955E-01 0. -32.6798737E+00 12.4671000E+04 0.

LGEAR

DELTA P P2 FT SR SF AA FC2
28.0530148E-02 32.1110133E+04 0. 37.0625599E+03-25.2453298E+00-37.0989053E+03-73.5738284E-01-13.2045782E+02
12.0249744E-02 22.4845351E+04 0. 57.4247866E+03 24.5240969E-01-56.6156044E+03 29.7538634E+00 34.8732586E+02
12.0249744E-02 22.4845351E+04 0. 57.4247866E+03 24.5240969E-01-56.6156044E+03 29.7538634E+00 34.8732586E+02

MUVP VGPT FTRX FTRY FTRZ HA HB ODELTA
86.7051117E-03 52.1541791E-02-32.1360363E+02 0. -37.0636006E+03-27.2316450E+02 0. 20.0530148E-02
24.0771911E-04 14.4839644E-03 13.8262656E+01 0. -57.4247449E+03 13.9783580E+01 0. 12.0249744E-02
24.0771911E-04 14.4839644E-03 13.8262656E+01 0. -57.4247449E+03 13.9783580E+01 0. 12.0249744E-02

SD2 SD1 S S2D2 S201 S2 OMETD1 OMET
-64.7767109E+00 31.0705813E-01 13.0479289E-01 0. 0. 0. -11.3465187E+02-34.0099382E+01
32.2747838E-03-28.7128354E-02 14.4744319E-01 0. 0. 0. 17.5209719E+00-28.5605215E+01
32.2747838E-03-28.7128354E-02 14.4744319E-01 0. 0. 0. 17.5209719E+00-28.5605215E+01

FTRA FTRB FTRC HTX HTY HTZ FXH FYH

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 179

-38.1052515E+02 0. -15.1911654E+04 0. 95.3566575E+04 0. -30.1052515E+02 0.
FZH LM HM NM
-15.2281879E+04 0. 96.4205719E+04 0.
VPCS
38.7489900E+02
TFFS
0. 0.

T(1)

SAC1

32.4672233E-03 32.3831856E-03-16.1048668E-02 0. 0. 62.2923339E-04 0.

FLEX

POINT XD1T	X02F YD1F	X02T YD1T	Y02F ZD1F	Y02T Z01T	Z02F XD0F	Z02T YD0F	X01F Z00F
10.0000000E-01 0.		-32.5240597E-01 0.	0.	0.	41.1800958E-01-55.6486512E+00 0.		0.
28.9704573E+01 0.		0.	12.8530724E-02 70.6658675E-01 0.	0.	0.	0.	-20.0210801E-03
20.0000000E-01 0.		-18.4303439E-01 0.	0.	0.	-27.6453393E-01-57.7657241E+00 0.		0.
28.9359333E+01 0.		0.	16.4512752E-02 58.9226573E-01 0.	0.	0.	0.	-28.4621124E-04
30.0000000E-01 0.		-16.5886682E-01 0.	0.	0.	15.4501461E-01-29.3457206E+00 0.		0.
28.9619143E+01 0.		0.	-16.7881872E-02-49.2437333E-02 0.	0.	0.	0.	56.7421359E-04
40.0000000E-01 0.		-13.6399346E-01 0.	0.	0.	17.1453016E-02-11.9817521E+00 0.		0.
28.9703879E+01 0.		0.	20.6029964E-02-48.2583891E-01 0.	0.	0.	0.	-15.6702759E-03

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

17.1800000E-02 20.1525000E-01

PITCH AUTOPILOT

DELQW	ALPHA E	ALPHD1	ALPDD1	ALPHET	DELQDE
38.2904551E-01	21.0562305E-02-92.8086251E-01 0.			21.0562305E-02 80.0000000E-01	

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OF FOUR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 180

STOP

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APPENDIX H

AIRPLANE B FLEXIBLE BODY EXAMPLE 5

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ORIGINAL PAGE IS
OF POOR QUALITY

STCASE	TAB	
1	AB01	2
ATAB02		NNNN
ATAB03		NNNN
ATAB11		NNNN
ATAB12		NNNN
ATAB15		NNNN
ATAB16		NNNN
ATAB51		NNNN
ATAB52		NNNN
ATAB53		NNNN
ATAB56		NNNN
ATAB57		NNNN
CTAB01		113
CTAB02		113
FTAB02		113
FTAB03		113
TTAB10		113
VTAB11		113
VTAB12		113
VTAB03		113
VTAB04		113
VTAB06		113
TRA		
REH	BCD	3SDF2-PLANPLANE
NCASE	BCD	1LROLL
REH	BCD	4INTEGRATION INFORMATION
IVARBH		4
TMAX		40.
AMINER		.00005
PRTHIN		.0
AMAXER		.001
DELTS		.001
PRINT		.5
REH	BCD	3REQD FOR SDF-2
AMASS		3874.899
HGC7F		10.0
GAM7D		-1.1606E
VG77F		296.22076
THTBD		10.3394
RWHGR		.0
INDAPC		1
INDADD		1
INDFPA		1
INDPLA		1
INDACH		2
INDGRT		1
INDWGT		1
REH	BCD	5VEHICLE PHYSICAL PROP. DATA
INDVPC		1
XCGRF		.0
VTAB01		2,0.,0.,5000.,1.
VTAB02		2,0.,1.59702E+6,5000.,1.59702E+6
VTAB03		2,0.,1.59702E+6,5000.,1.59702E+6
VTAB04		2,0.,1.59702E+6,5000.,1.59702E+6
INDXZS		1
VTAB06		2,0.,1.0E+5,5000.,1.0E+5
REH	BCD	4AERODYNAMIC INPUT DATA
INDAER		1
AREFF		1605.
D1RFF		37.7
D2RFF		56.7
INDA01		1
ATAB01		-7.9573427E-3,-5.5941985E-3

ATAB02	1.4020979E-3,8.8931664E-4
INDA02	1
ATAB80	1
INDA80	4.18951E-2,2.00844E-2
ATAB10	1
INDA10	-3.978321E-2,-3.9650349E-2
ATAB11	1
INDA11	5.7452448E-2,3.7645688E-2
ATAB12	1
INDA12	1.4720279E-3,1.2354312E-3
ATAB15	1
INDA15	-1.725E-2,-1.45E-2
ATAB16	1
INDA16	1.25E-4,5.0E-5
ATAB51	1
INDA51	7.3516484E-3,1.7027972E-3
ATAB52	1
INDA52	-5.2147852E-4,1.0238928E-3
ATAB53	1
INDA53	-3.1368631E-4,1.8065268E-5
ATAB56	1
INDA56	8.7E-3,7.3418182E-3
ATAB57	1
INDA57	2.0E-5,3.6363636E-5
REH	BCD 3 ENGINE THRUST DATA
INDIFF	3
INDISO	1
IT10X	4
ITAB10	-2.,-1.5,-1.,-.5,0.,.5,1.,1.5,2.
ITAB10	0.,.5,1.,2.,3
ITAB10	0.,.5,0.,0.,0.,0.
ITAB10	0.,.5,0.,0.,0.,0.
ITAB10	0.,.5,0.,0.,0.,0.
ITAB10	0.,.5,0.,0.,0.,0.
ITAB10	0.,.5,0.,0.,0.,0.
ITAB10	0.,.5,0.,0.,0.,0.
ITAB10	0.,.5,0.,0.,0.,0.
ITAB10	0.,.5,0.,0.,0.,0.
IT10H	9
REH	BCD 3 LANDING GEAR DATA
NSTRUT	3
MASS	4.940000,27.19587,27.19587
RX	35.0833,-2.83867,-2.83867
RY	0.,-8.3333,+8.3333
RZ	1.91667,.509583,.509583
THETAD	0.,0.,0.
ERDEG	0.
RGR	4.47
NTIRES	2.,3.,3.
RZERO	1.0479167,1.13125,1.13125
W	.554167,.604167,.604167
DELTAM	.198333,.1958333,.1958333
RLT	1.5E+3
IFD	1
AI	1.324533E+5,3.8129286E+5,3.8129286E+5
BI	1.2112257,1.412391,1.412391
FTAB02	2,0.,0.,1.5E+4,0.
FTAB03	6,0.,0.,.007,.336,.1,.336,.4,.336,1.,.336,100.,.336
MOMENT	1.2,2.6,2.6
HB	0.,0.,0.
RF	5.48333,6.8792,6.8792
VZ	0.
PZERO	35280.,40320.,40320.
VZERO	0.1614583,.4716435,.4716435
A	.1104266,.2673611,.2673611

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T1		1	
1 JCQ1		1	
NSMAIN		2	
CTAB01		0.	1.6667,1.,2.,3.
CTAB01		136.781,136.781,	443.92,443.92,443.92,443.92
CTAB01		443.92	
INDCC2		1	
CTAB02		0.	1.6667,1.,2.,3.
CTAB02		136.781,136.781,	4.23E+4,4.23E+4,4.23E+4,4.23E+4
CTAB02		4.23E+4,4.23E+4	
MUS		1.	1.,1.
ES		.0001333,	.00016667,.00016667
SB		1.333,1.6667,1.6667	
REM	BCD	4	FLEXIBLE AIRFRAME DATA
INDFLX		1	
NMODE		8	
GMASS1		66.6617,79.4557,71.8341,	12.1131
GMASS1		29.0656,96.7316,70.4027,	31.6212
GFREQ		13.138,16.512,31.059,	43.398
GFREQ		48.198,61.123,74.123,	87.198
SZMOD		.08,-.16,-.16,-.02,-.042,-.0942	
SZMOD		-.153,-.1393,-.1393,-.065,-.0112,-.0112	
SZMOD		.04,-.0687,-.0687,-.189,-.12,-.12	
SZMOD		-.01,-.105,-.105,-.05,-.01,-.01	
ARMODE		0.,0.,-.1144,-.4239,-4.,0.	
ARMODE		0.,0.,-.2414,-3.6431,-4.,0.	
ARMODE		0.,0.,-.0435,-6.8331,-4.,0.	
ARMODE		0.,0.,-.6644,-3.2341,-5.,0.	
ARMODE		0.,0.,-.0342,-5.6531,-5.,0.	
ARMODE		0.,0.,-.6054,-1.3511,-1.,0.	
ARMODE		0.,0.,-.1258,-3.7161,-4.,0.	
ARMODE		0.,0.,-.0323,-9.6021,-4.,0.	
NPTS		4	
OUTMOD		0.	3.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.
OUTMOD		0.	197,-.1385,-.1385,-.0035,-.0254,-.3026,-.1673,-.1157
OUTMOD		0.	3.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.
OUTMOD		0.	.08,-.02,-.153,-.065,-.64,-.165,-.01,-.05,-.0.,0.,0.,0.,0.,0.,0.,0.
OUTMOD		0.	3.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.
OUTMOD		0.	1,-.0642,-.1393,-.0112,-.0087,-.12,-.105,-.01
OUTMOD		0.	0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0.
OUTMOD		0.	203,-.244,-.1072,-.125,-.1998,-.4409,-.0165,-.2167
ROIS		42.6667,0.,0.,35.0833,	6.,1.91667
ROIS		-2.83867,8.3333,	.509583,-32.3333,0.,0.
REM	BCD	3	PLOT TAPE DATA
IPLT		1	
ISDF		1	
ISTPL2		1	
IFLX	INT	1	0,1,1
REM	BCD	3	AUTOPILOT DATA
REM	BCD	3	A. ENGINE DATA
INDAUT		1	
IN		2	
ZN		-.55,-.55	
YN		-14.1667,14.1667	
N		0.	J.
REM	BCD	3	B. DRAG CHUTE DATA
ICS		0	
COCH		.244	
SSH		1605.	
XCH		-9.625	
YCH		0.	
ZCH		-2.41667	
REM	BCD	5	C. PHASE BEGIN-TERMINATE
ITO		0	
HF		12.25	

6
136
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H-5

NE	0.	
HRF	83.796	
DELTAH	0.	
NLRI	0.	
TI	0.	
KP	0.	
VS	10.	
XS	3000.	
TS	12.	
HS	0.	
REM	BCD 46.	HOLD MANEUVER DATA
ALPDES	11.5	
TTD	0.	
KE	INT 1.1	
PH	11.5	
REM	BCD 5H.	LANDING ROLL MANEUVER DATA
TSP	0.	
TRV	0.	
TCH	7.	
TBK	0.	
ISS	0.	
ILR	0.	
IBS	0.	
REM	BCD 5I.	ENGINE FAILURE STAGE DATA
IC	INT 0.0	
XRF1	INT 0.0	
IT1	INT 0.0	
XRF2	INT 0.0	
IT2	INT 0.0	
H1	INT 0.0	
IH1	INT 0.0	
H2	INT 0.0	
IH2	INT 0.0	
HR1	INT 0.0	
IHR1	INT 0.0	
HR2	INT 0.0	
IHR2	INT 0.0	
TR1	INT 0.0	
ITR1	INT 0.0	
TR2	INT 0.0	
ITR2	INT 0.0	
REM	BCD 5J.	BRAKE COND.STAGE DATA
IB	INT 0.0,0	
TBK1	1.	
IBK1	INT 0.0,0	
TBK2	1.	
IBK2	INT 0.0,0	
REM	BCD 4K.	PITCH AUTOPILOT DATA
TST	.2	
ALPDL	.2	
RFALPH	.61	
DELALA	0.	
PSH	0.	
PSH2	0.	
RFALP2	0.	
DELQF	0.	
DELQTO	0.	
DELQGL	-10.	
DELQUL	+25.	
DELFO1	5.25	
REM	BCD 4L.	YAW AUTOPILOT DATA
RFB	.5	
DELBA	.05	
PSR	10.	

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POSTA	.05
PSI	.05
PSPSI	.05
DELRL	-20.
DELRO	+20.
REM	BCD 4M. ROLL AUTOPILOT DATA
REFPHI	.5
OPHIA	.05
PSA	-10.
DELPL	-12.
DELPD	+12.
REM	BCD 5N. THROTTLE AUTOPILOT DATA
TF	INT 0.0
NDF	INT 0.0
IR	INT 0.0
NR	1.0
NLR	0.0
NTO	0.0
K2	1.
REM	BCD 40. BRAKE AUTOPILOT DATA
MBC	0.0
PO	.1
DELTAN	.001
OMECDI	20.
MBL	0.0
MBU	0.0
REM	BCD 5P. CONTROL RESPONSE DATA
DELHS	5.25
DELRRD	31.5
DELA	10.
NED1	.1
REM	BCD 40. INITIALIZATION
IAP	3
HR	10.
DELQD	4.56478
DELQDE	4.56478
DELQN	4.56478
DELPD	0.
DELRO	0.
MANLOG	1
PITCHP	1
REM	BCD 2STAGING DATA
REM	BCD 4A. GEARS INTO PROGRAM
INDLG	0
ISTAGE	0
DECRES	BCD 1HR
STESTD	11.0
TRA	
INDLG	-1
REM	BCD 48. SMOOTH IMPACT STAGE
AINCRS	BCD 30DEL110DEL120DEL13
STEST	-.05, -.05, -.05
TRA	
PRINT	.02
DELTS	.005
AMAXER	.0005
PRTHIN	0.
AINCRS	BCD 1TIMES
STEST	.9
TRA	
ATAB51	7.3516484E-3, 1.7027972E-3
ATAB52	-5.2147852E-4, 1.0238928E-3
ATAB53	-3.1368631E-4, 1.8065268E-5
ATAB56	0.0
ATAB57	0.0

```

BFH BCD 50 EFFICIENT AMAXER STAGE
/ NCRS BCD 40 DELTA1 DELTA2 DELTA3
STEST TRA .1, .1, .1

PRINT .05
AMAXER .01
DELTS .01
REM BCD 40 SMOOTH IMPACT STAGE
AINCRS BCD 10 DELT1
STEST -.05
TRA

PRINT .02
DELTS .005
AMAXER .0005
REM BCD 50 EFFICIENT AMAXER STAGE
AINCRS BCD 10 DELTA1
STEST .1
TRA

PRINT .05
AMAXER .01
DELTS .01
INDSTF 1
TRA

```

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 8

A. GEARS INTO PROGRAM

INITIAL PRINT OUT FOR VP3S

XCGRF AREFF 01RFF D2RFF
0. 16.4500000E+02 37.7000000E+04 56.7000000E+04

PRINT CODES IDENTIFYING TIME HISTORY

2SDF

TIME
PI77R
ZG77F1
PSIPD
FCY

TIMES
QI77R
ALPHD
PHIPO
FCZ

XG77F
RI77R
BETAD
AX77F

YG77F
AHACH
ALPHD1
AV77F

HGC7F
VA77F
BETAD1
AZ77F

U777F
DYNBP
GAN7D
WTR7P

V777F
XG77F1
SIG7D
FDG

W777F
YG77F1
THIPD
FCX

VPCS

AHASS

TFFS

HT

NT

SAG1

CAVAH

CA

CN

CY

CL

CH

CNN

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSUF 2 CASE LROLL STAGE 1 PAGE 9

2SDF

0.	0.	0.	0.	10.000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337676E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	57.7454851E-01	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.	0.	0.	-31.6515539E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

YFFS

0. 0.

T(I)

SAC1

29.7745619E-03-26.8749533E-03 60.9750539E-02 0. 0. 15.3281670E-03 0.

FLARE

AUTS

ALPDES

PHIDES

TTD

11.5000000E+00 0. 0.

PITCH AUTOPILOT

DELQN

ALPHA

ALPHD1

ALPDD1

ALPHET

DELQDE

26.8544760E-01-14.0024531E-07 0. 0. -14.0024531E-07 26.8544760E-01

INTEG RTN. HT = 1.0000000E-03

2SDF

0.	0.	0.	0.	10.000000E+00	29.0274042E+01	0.	59.0569126E+00
59.9992281E-01	11.4999986E+00	0.	26.5337676E-02	29.6221760E+01	10.4252977E+01	29.6159990E+01	0.
0.	0.	90.1422933E-02	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.	0.	0.	-26.3302709E+00	12.4671000E+04	0.	0.

VPCS

38.7489900E+02

6-H

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 10

TFFS

0.

0.

0.

0.

T(I)

SAC1

29.7745019E-03-20.8749533E-03 60.9750569E-02 0.

0.

15.3281670E-03 0.

FLARE

AUTS

ALPDES

PHIDES

TTO

11.5000000E+00 0.

0.

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELQDE

27.5607208E-01-14.0024531E-07 0.

0.

-14.0024531E-07 27.5607208E-01

STAGE-ON--DECR. HR

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 11

INDLG -1
REK BCD 40. SMOOTH IMPACT STAGE
AINCRS BCD 300 DELT100 DELT200 DELT3
STEST TRA -.05, -.05, -.05

ZSDF

0. 0. 0. 0. 10.000000E+00 29.0274042E+01 0. 59.0569126E+00
59.9992251E-01 11.4999986E+00 0. 26.5337670E-02 29.6223760E+01 10.4252977E+01 29.6159990E+01 0.
0. 0. 0. 0. 0. -11.6059853E-01 0. 10.3393988E+00
0. 0. 90.1422943E-02 0. -26.3342709E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FI

SR

SF

AA

FC2

0. 35.2814400E+13 0. 0. 31.9713310E-01 -38.9549765E+02 -78.8562277E+01 0.
0. 40.3204400E+13 0. 0. 54.9315280E-01 -10.7799996E+03 -39.6363699E+01 0.
0. 46.3204400E+13 0. 0. 54.9315280E-01 -10.7799996E+03 -39.6363699E+01 0.

HUVP

VGPT

FTRX

FTRY

FTRZ

MA

MD

ODELTA

33.6001440E-02 29.6159996E+11 0. 0. -6. 0. 0. -79.6095154E-01
33.6001440E-02 29.6159996E+11 0. 0. -6. 0. 0. -10.9646626E-01
33.6001440E-02 29.6159996E+11 0. 0. -6. 0. 0. -10.9646626E-01

S02

S01

S

S2D2

S2D1

S2

OMETD1

ONET

0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.

FTRA

FTRB

FTRC

MTX

HTY

MTZ

FXH

FYM

0. 0. 0. 0. 0. 0. 0. 0.

FZH

LH

KH

NH

0. 0. 0. 0. 0. 0. 0. 0.

VPCS

38.7489900E+02

TFPS

0. 0. 0. 0. 0. 0. 0. 0.

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INDSDF 2 CASE LROLL STAGE 1 PAGE 12

T (I)

5.

3.

SAC1

29.7745819E-03-20,8749533E-03 60,9750569E-02 0.

6.

15.3281670E-03 0.

FLEX

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
14.6627430E-01	0.	90.1295544E-02	0.	0.	0.	-28.9135646E+00	0.
19.662827430E-01	0.	1.1739412E-01	0.	59.0563126E+00	0.	-21.0484329E-04	0.
29.662927430E-01	0.	9.2374457E-02	0.	59.0563126E+00	0.	-4.4544208E+00	-1.04482040E-04
39.663027430E-01	0.	90.1254011E-02	0.	59.0563126E+00	0.	-1.584011E+00	1.62379040E-04
49.663127430E-01	0.		0.	59.0563126E+00	0.	-4.3726223E+00	-27.7776622E-04

FLARE

AUTS

ALPOES

PHILES

TYP

11.50000000E+00 0.

Le

PITCH AUTOPILOT

DELOH

ALPHA

ALPHAB1

ALPDD1

ALPHET

VELQDE

27.5339224E-01-14.0024531E-07 b.

0.

-14.0624531E-07 27.5339224E-01

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 13

[illegible]

250F

51.6410000E-03	54.0000000E-03	14.8031852E+00	0.	96.9255678E-01	29.0027316E+01	0.	59.3319476E+00
27.2363745E-04	2.72363745E-04	0.	26.5170101E-02	29.6333999E+01	10.4122497E+01	29.5967086E+01	0.
62.9388516E-01	11.5616894E+00	0.	12.6451639E-01	0.	-12.1824054E-01	0.	19.3434483E+00
0.	0.	94.7823961E-02	0.	-26.7932175E+00	12.4671000E+04	0.	0.

LGEAR

DELTA

500

35.280 JCL DE +03
40.32J.6C DE +03
40.320 JCL DE +03

4
5
6

44

FT

44

SK

31.53.72.9E-01
50.034775E-01
50.034775E-01

SF

```
-38.9549765E+J2
-10.7799996E+J3
-10.7799996E+U3
```

AA

```
-78.8562277E+01
-39.6383699E+01
-39.6383699E+01
```

FC 2

20

MVP

VGPT

FIRX

FTRY

FIRZ

NA

NB

DELTA

H-1-3

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 14

33.603000E-02 29.5969717E+11 0. 0. -0. 0. 0. -76.6526922E-01
33.603000E-02 29.5988332E+01 0. 0. -0. 0. 0. -78.1315998E-02
33.603000E-02 29.5988332E+01 0. 0. -0. 0. 0. -78.1315998E-02

S02 SD1 S S2D2 S2D1 S2 ONETD1 ONET

0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.

FTRA FTRB FTRC HTX HCY HTZ FXH FYH

0. 0. 0. 0. 0. 0. 0. 0.

FZH LH MH NH

-40.9444643E-02 0. -27.3064447E-01 0.

VPCS

38.7489900E+02

TFFS

0. 0.

T(I)

SAC1

30.0142492E-03-21.9770026E-03 62.1246433E-02 0. 0. 12.2577445E-03 0.

FLEX

POINT X02F X02T Y02F Y02T Z02F Z02T X01F
X01T Y01F Y01F Z01F Z01T X00F Y00F Z00F

10.000000E-01 0. 94.7404930E-02 0. 0. -60.3753620E-04-28.8624243E+00 0.
29.0027310E+01 0. 0. -12.0030225E-05 59.2156589E+00 0. 0. 0. -21.0662029E-04
28.660000E-01 0. 10.4018379E-01 0. 0. 0. 0. 0. 0.
29.0032533E+01 0. 0. -19.9376245E-05 59.2362340E+00 0. 0. 0. -12.4003461E-04
29.003000E-01 0. 97.2566636E-02 0. 0. 0. 0. 0. 0.
29.0028700E+01 0. 0. 31.6901258E-05 59.3404360E+00 0. 0. 0. 16.2990389E-04
40.000000E-01 0. 94.7926221E-02 0. 0. -13.3526523E-03-23.2430775E+00 0.
29.0027309E+01 0. 0. -51.3689637E-05 59.4195381E+00 0. 0. 0. -27.8760104E-04

FLARE

AUTS

H-14

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 15

ALPDES PHIDES TTO

11.50000000E+00 y.

PITCH AUTOPILOT

DELQD	ALPHA	ALPHD1	ALPD01	ALPHET	DELQDE
042994E-01	61.689458E-03	12.6451639E-01	0.	61.6894058E-03	28.3342090E-01

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OF POOR QUALITY

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 16

INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03
INTG RTN. HT 1.6000000E+03

2SDF

10.000000E-02 10.000000E-02 29.5966729E+00 0. 93.7103967E-01 28.9775565E+01 0. 59.6103275E+00
4. 48.197070E+04 L. 26.600397E-02 29.5044871E+01 10.3993475E+01 29.5772045E+01 0.
65.639292E-01 11.6257341E+03 L. 12.9187672E-01 0. -12.7132816E-01 0. 13.3544047E+00
0. 0. 99.5792447E-02 0. -27.2804053E+00 12.4671000E+04 0. 0.

LGEAR

DELTA P P2 FT SR SF AA FG2

0. 35.2800000E+03 0. 0. 31.1198337E-01-38.9549765E+02-78.8562277E+01 0.
0. 40.3200000E+03 L. 0. 44.7848901E-01-10.7799996E+03-39.6383699E+01 0.
0. 40.3200000E+03 L. 0. 44.7848901E-01-10.7799996E+03-39.6383699E+01 0.

HJVP VGPT FTRX FTRY FTRZ HA HB DDELTA

33.6000000E-02 29.5775613E+01 L. 0. -0. 0. 0. -73.5659757E-01
33.6000000E-02 29.5804669E+01 L. 0. -L. 0. 0. -45.9463710E-02
33.6000000E-02 29.5849669E+01 L. 0. -L. 0. 0. -45.9463710E-02

SQ2 S01 S S202 S201 S2 OMETD1 OMET

0. 0. L. 0. 0. 0. 0. 0.
0. 0. L. 0. 0. 0. 0. 0.
0. 0. L. 0. 0. 0. 0. 0.

FTRA FTRD FTRS HTX HTY HTZ FXH FYH

0. 0. L. 0. L. 0. 0. 0. 0.

FZM LH MH NH

-30.3471767E-02 0. -22.1607473E-01 0.

VPCS

30.7089900E+02

IFFS

H-16

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 17

1.

0.

0.

0.

T(I)

SAG1

30.2764712E-03-23.1165513E-03 53.3345960E-02 0.

0.

90.5479600E-04 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.000000E-01 0.		99.4718957E-02 0.	0.	0.	-13.9610624E-03-28.8165118E+00 0.		
28.9775555E+01 0.		0.	-67.9468564E-05 59.4117070E+00 0.	0.	0.		-21.2477124E-04 0.
20.000000E-01 0.		11.6330259E-01 0.	0.	0.	-60.2887769E-04-28.5386679E+00 0.		0.
28.9784797E+01 0.		0.	-66.0806585E-05 59.4482754E+00 0.	0.	0.		-12.6999361E-04 0.
30.000000E-01 0.		10.1410344E-01 0.	0.	0.	76.3307855E-04-27.1715151E+00 0.		0.
28.9778029E+01 0.		0.	69.8157902E-05 59.6324072E+00 0.	0.	0.		16.5537344E-04 0.
40.000000E-01 0.		99.6433153E-02 0.	0.	0.	-97.0273673E-04-26.1366245E+00 0.		0.
28.9775555E+01 0.		0.	-99.1530823E-05 59.7728730E+00 0.	0.	0.		-28.2621749E-04 0.

FLARE

AUTS

ALPD&S

PHIDES

TTD

11.5000000E+00 0.

L.

PITCH AUTOPILOT

DELQN

ALPHA&

ALPH01

ALPD01

ALPH&T

DELQ&E

29.1243699E-01 12.5734103E-02 12.9187072E-01 0.

12.5734103E-02 29.1249699E-01

H-17

ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE ROLL STAGE 1 PAGE 61

2SDF

62.1000000E-02 52.1000000E-02 18.2779011E+01 0. 72.8278655E-01 28.8804969E+01 0. 47.6178875E+00
0. 56.8839321E-02 25.2185272E-02 29.2704183E+01 10.1801491E+01 29.2699998E+01 0.
-15.6534059E-01 93.6264033E-01 69.4071438E-01 0. -73.5941148E-01 0. 36.8411629E-02 0.
0. 0. 0. 0. -52.7622423E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2801010E+03 0. 0. -27.3884855E+00 -38.9549765E+12 -78.8562277E+01 0.
13.1488509E-02 27.5133352E+04 0. 63.8888882E+03 -42.3215235E+00 -62.1944685E+03 62.3443314E+00 10.0750751E+03
13.1488589E-02 27.5133352E+04 0. 63.8888882E+03 -42.3215235E+00 -62.1944685E+03 62.3443314E+00 10.0750751E+03

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DDELTA

33.6013000E-02 19.2564946E+01 0. 0. -0. 0. 0. -48.3248881E-01
30.543491E-03 18.6144325E-02 19.9022912E+02 0. -65.1486407E+03 19.8975418E+02 0. 13.1488589E-02
30.543491E-03 18.6144325E-02 19.9022912E+02 0. -65.1486407E+03 19.8975418E+02 0. 13.1488589E-02

SD2

SD1

S

S2D2

S2D1

S2

ONETD1

ONET

0. 0. 0. 0. 0. 0. 0. 0.
-11.734163E+00 -48.8338364E-02 15.3555000E-01 0. 0. 0. 29.5096689E+01 -29.2734080E+01
-11.7341630E+00 -48.8338364E-02 15.3555000E-01 0. 0. 0. 29.5096689E+01 -29.2734080E+01

FTRA

FTRB

FTRC

NTX

MTY

HTZ

FXH

FYM

25.8082436E+03 0. -12.7777776E+04 0. -28.6730913E+04 0. 25.8082436E+03 0.

FZH

LH

MH

NH

-12.7227571E+04 0. -21.6757725E+04 0.

VPCS

38.7483900E+02

TFFS

0. 0.

0.

0.

T(II)

SAC1

32.1718824E-03 -66.4893942E-04 47.3079602E-02 0. 0. 17.5817250E-03 0.

H-18

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 62

FLEX

POINT X01F	X02F Y01F	X02I Y01I	Y02F Z01F	Y02I Z01I	Z02F X00F	Z02I Y03F	X01F Z00F
10.433000E-01	0.	68.466688E-01	0.	0.	-10.6213103E+00	-60.7731074E+00	0.
28.8834377E+01	0.	-38.1223422E-02	49.6509167E+00	0.	0.	0.	94.0271317E-04
20.1500000E-01	0.	57.4778087E-01	0.	0.	-84.7969118E-01	-59.1051493E+00	0.
28.8696456E+01	0.	-33.1877891E-02	49.2711607E+00	0.	0.	0.	-14.0727492E-06
30.1000000E-01	0.	68.8317726E-01	0.	0.	-21.0819668E+00	-74.0437875E+00	0.
28.8775697E+01	0.	30.7482825E-02	47.7647472E+00	0.	0.	0.	66.8809979E-04
40.1000000E-01	0.	70.694473E-01	0.	0.	35.4803416E+00	-19.2952814E+00	0.
28.8835337E+01	0.	-21.8599444E-02	45.5697519E+00	0.	0.	0.	-75.5986953E-04

AUTS

TI

TR

17.1000000E-02 45.0000000E-02

ISS = 1

LANDING ROLL
ILR = 1

IGS = 0

IRS = 1

PITCH AUTOPILOT

DELON	ALPHA	ALPHA01	ALPHA03	ALPHA05	DELQ0E
30.2304646E+01	21.0562187E-02	-73.59411+8E-01	0.	21.0562187E-02	43.4154646E-01
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			

2SDF

64.1000000E-02	64.1000000E-02	18.8632650E+01	0.	73.1777552E-01	28.8881821E+01	0.	46.9475045E+00
0.	-57.3493224E-03	0.	0.	29.2671787E+01	10.1777856E+01	29.2665585E+01	0.
-19.0531149E-01	92.3309947E-01	59.7925932E-01	0.	-57.5024101E-01	0.	37.3800049E-02	95.0369922E-01
0.	0.	0.	0.	-44.3912009E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	39.283300E+03	0.	0.	-64.3249163E-01	-38.9549765E+02	-78.8562277E+01	0.
10.8317855E-02	26.2846182E+34	0.	48.3677210E+03	-25.6507326E+00	-47.1053210E+03	46.4188123E+00	22.0469100E+03
10.8317855E-02	26.2806182E+34	0.	48.3677210E+03	-25.6507326E+00	-47.1053210E+03	46.4188123E+00	22.0469100E+03
HUVP	VGPT	FTRK	FTRY	FTRZ	HA	HB	DELTA

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 63

33.603354E-02 29.252124E-01 28.940538E-02 0. -0. -49.544301E+03 29.664206E+02 0. -40.340338E-01
58.412747E-03 35.584476E-02 28.940538E-02 0. -49.544301E+03 29.664206E+02 0. 13.831785E-02
58.412747E-03 35.584476E-02 28.940538E-02 0. -49.544301E+03 29.664206E+02 0. 10.831785E-02

SJ2 SD1 S S202 S201 S2 OHETD1 OHET
0. 0. 0. 0. 0. 0. 0. 0.
-10.955110E+01 -72.194428E-02 14.934233E-01 0. 0. 0. 37.954111E+01 -29.620390E+01
-10.955110E+01 -72.194428E-02 14.934233E-01 0. 0. 0. 37.954111E+01 -29.620390E+01

FTRA FTRB FTRC HTX HTY HTZ FXH FYH
22.238379E+03 0. -96.735442E+03 0. -13.738367E+04 0. 22.238379E+03 0.

FZH LH MH NH
-96.655866E+03 0. -13.606371E+04 0.

VPCS

38.748990E+02

TFFS

0. 0.

G. J. T(I)

SAC1
32.139382E-03 -56.970407E-04 46.126573E-02 0. 0. 19.130656E-03 0.

FLEX

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
16.603354E-02 0.		58.983849E-01 0.	-44.726727E-02 0.	48.945436E+00 0.	31.367856E-01 -40.766867E+00 0.		65.087258E-05 0.
58.412747E-03 0.		58.848535E-01 0.	-37.197490E-02 0.	48.586130E+00 0.	58.363449E-01 -38.161257E+00 0.		75.402915E-04 0.
58.412747E-03 0.		59.922462E-01 0.	-83.623496E-03 0.	46.701198E+00 0.	-12.932497E+00 -57.357809E+00 0.		86.451788E-04 0.
28.888217E-01 0.		60.544726E-01 0.	27.090925E-02 0.	45.365414E+00 0.	85.087347E-01 -36.251935E+00 0.		-61.122216E-04 0.

ISS = 1 ILR = 1 LANDING ROLL ICS = 0 IBS = 1

AUTS

H-20

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 64

TI TR
17.1333000E-02 47.0000000E-02

PITCH AUTOPILOT

DELQN	ALPHA	ALPH01	ALPD01	ALPHET	DELQDE
30.2904646E-01	21.1562187E-02	57.5024111E-01	0.	21.0562187E-02	44.4654646E-01
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

2SDF

66.1000000E-02	66.1100000E-02	19.4485662E+01	0.	73.5777460E-01	28.8931806E+01	0.	46.4549595E+00
20.6413184E-01	91.3394418E-01	43.1718725E-01	0.	29.2642532E+01	10.1757389E+01	29.2635252E+01	0.
0.	0.	0.	0.	0.	0.	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FG2
0.	35.2810000E+03	0.	0.	13.5609060E+00	38.9549765E+02	78.8562277E+01	0.
79.7485395E-03	24.7787484E+04	0.	31.2633690E+03	55.8094456E-01	30.7477936E+03	18.9578574E+00	34.7049533E+03
79.7485395E-03	24.7787484E+04	0.	31.2633690E+03	55.8094456E-01	30.7477936E+03	18.9578574E+00	34.7049533E+03

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDelta
33.6000000E-02	29.2532878E+01	0.	0.	0.	0.	0.	-48.3818660E-01
83.6291031E-03	50.5797895E-02	26.6939812E+02	0.	-32.1501500E+03	28.0687612E+02	0.	79.7485395E-03
83.6291031E-03	50.5797895E-02	26.6939812E+02	0.	-32.1501500E+03	28.0687612E+02	0.	79.7485395E-03

S02	S01	S	S202	S201	S2	ONETD1	ONET
0.	0.	0.	0.	0.	0.	0.	0.
-71.9041473E-01	0.5785885E-02	14.7701977E-01	0.	0.	0.	35.9855900E+01	-27.8566322E+01
-71.9041473E-01	0.5785885E-02	14.7701977E-01	0.	0.	0.	35.9855900E+01	-27.8566322E+01

FIRA	FTR0	FTR3	HTX	HTY	HTZ	FXH	FYN
15.9197474E+03	0.	-62.5267381E+03	0.	-77.6736544E+03	0.	15.9197474E+03	0.

FZH	LH	HH	NH
-63.5096594E+03	0.	-77.0198697E+03	0.

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ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

ENDSOF 2 CASE LROLL STAGE 1 PAGE 65

VPCS
38.748990E+02
TFFS

0.

0.

0.

0.

T(I)

SAC1

32.1012122E-03-49.5283810E-04 45.2095600E-02 0.

0.

20.5249065E-03 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD6F	ZD2T YD6F	XD1F ZD6F
10.000000E-01 0.	0.	42.1406029E-01 0.	0.	48.5740770E+00 0.	85.2945214E-01-28.2359282E+00 0.	0.	-71.6088251E-04
0.89322214E+01 0.	0.	-31.6250896E-02 0.	0.	0.	18.3651000E+00-18.1721599E+00 0.	0.	-12.7956221E-03
0.000000E+00 0.	0.	-11.0876619E-02 0.	0.	48.3465991E+00 0.	0.	0.	59.4178459E-04
0.6823135E+01 0.	0.	0.	0.	0.	92.2606562E-01-26.1346324E+00 0.	0.	-14.1993966E-04
0.000000E+00 0.	0.	43.5497000E-01 0.	0.	46.1825397E+00 0.	0.	0.	0.
0.8912380E+01 0.	0.	-11.0391654E-02 0.	0.	0.	-23.4238270E+00-57.8713336E+00 0.	0.	0.
0.000000E+00 0.	0.	44.1226699E-01 0.	0.	44.6989206E+00 0.	0.	0.	0.
28.8931887E+01 0.	0.	0.	89.5103318E-03 0.	0.	0.	0.	0.

AUTS

ISS = 1

ILR = 1

LANDING ROLL

ICS = 0

IBS = 1

TI

TR

17.1000000E-02 49.0000000E-02

PITCH AUTOPILOT

DELQX	ALPHA	ALPHD1	ALPDD1	ALPHET	DELQDE
30.2904646E-01	21.0562187E-02	39.5701252E-01	0.	21.6562187E-02	45.5154646E-01
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

2SOF

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 66

68.1000000E-02 68.1000000E-02 26.0338019E+01 0. 73.9924394E-01 28.8948013E+01 0. 46.1261444E+00
0. -56.1625577E-03 0. 26.2397697E-02 29.26.6520E+01 10.1732222E+01 29.2599272E+01 0.
-28.5948773E-01 98.0987095E-01 27.7115257E-01 0. -25.3421840E-01 0. 40.3275483E-02 0.
0. 0. 0. -28.6024135E+00 12.4671006E+04 0.
0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
59.4214872E-03	35.2800000E+03	0.	0.	15.5449363E+00	-38.9549765E+02	-78.8562277E+01	0.
59.4214872E-03	23.2179868E+04	0.	18.6594468E+03	12.8135961E+00	-18.2453913E+03	15.2112330E+00	43.3294224E+03
59.4214872E-03	23.2179868E+04	0.	18.6594468E+03	12.8135961E+00	-18.2453913E+03	15.2112330E+00	43.3294224E+03

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.6000000E-02	29.2555109E+01	0.	0.	-0.2292475E+03	0.1306737E+02	0.	-48.3757175E-01
97.3389912E-03	59.2838668E-02	18.7117868E+02	0.	-19.2292475E+03	20.1306737E+02	0.	59.4214872E-03
97.3389912E-03	59.2838668E-02	18.7117868E+02	0.	-19.2292475E+03	20.1306737E+02	0.	59.4214872E-03

SD2	SD1	S	S2D2	S2D1	S2	QHETD1	QHET
0.	0.	0.	0.	0.	0.	0.	0.
-37.1143913E-01	-10.1209497E-01	14.5772370E-01	0.	0.	0.	29.8085561E+01	-27.2371260E+01
-37.1143913E-01	-10.1209497E-01	14.5772370E-01	0.	0.	0.	29.8085561E+01	-27.2371260E+01

FTRA	FTRB	FTRC	MTX	MTY	MTZ	FXH	FYH
10.0214262E+03	0.	-37.3180936E+03	0.	-42.4109999E+03	0.	10.0214262E+03	0.

FZM	LH	HM	NM
-38.1090417E+03	0.	-41.9508532E+03	0.

VPCS

38.7489900E+02

TFFS

0. 0.

0. J.

T(I)

SAC1

32.8609164E-03-43.9075172E-04 44.5380575E-02 0. 0. 21.7746800E-03 0.

FLEX

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OF POOR QUALITY

H-23

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

POINT X01T	X02F Y01F	INDSOF 2 X02T Y01T	CASE LROLL Y02F Z01F	STAGE 1 Y02T Z01T	PAGE 67 X02F X06F	Z02T Y02F	X01F Z00F
10.000000E-01	0.	26.5194196E-01	0.	0.	82.4253550E-01	22.8201092E+00	0.
28.8948673E-01	0.	14.2862451E-02	48.3795529E+01	0.	0.	0.	-11.7417473E-03
20.000000E-01	0.	27.4243689E-01	0.	0.	14.4432741E+00	16.1881451E+00	0.
28.8841100E-01	0.	24.8585609E-02	48.3450978E+01	0.	0.	0.	-11.2861483E-03
30.000000E-01	0.	27.9536124E-01	0.	0.	95.1141237E-01	18.9289262E+00	0.
28.8919150E-01	0.	12.8933439E-02	46.6956548E+01	0.	0.	0.	51.1889375E-04
40.000000E-01	0.	29.2164424E-01	0.	0.	22.1338210E+00	48.8718440E+01	0.
28.8948289E-01	0.	43.4347019E-02	43.8758765E+01	0.	0.	0.	-49.1257914E-04

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.100000E-02 51.000000E-02

PITCH AUTOPILOT

DELQN	ALPHA E	ALPH01	ALPDD1	ALPHET	DELQDE
30.2914646E-01	21.0562187E-02	25.3421840E-01	0.	21.0562187E-02	46.5654646E-01
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

ZSOF

70.100000E-02	70.100000E-02	21.6189596E+01	0.	74.3938158E-01	28.8938328E+01	0.	45.9182552E+00
0.	-54.8123739E-03	0.	26.2060175E-02	29.2564250E+01	10.1702716E+01	29.2557836E+01	0.
-19.3812782E-01	90.2990597E-01	0.	-15.0825969E-01	0.	37.9566097E-02	0.	94.0953165E-01
0.	0.	17.9692713E-01	0.	-23.8543818E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	35.280000E+03	0.	0.	19.5333695E-01	-38.9549765E+12	-78.8562277E+11	0.
37.1160437E-03	21.7387154E+04	0.	10.4988327E+03	-22.5909581E-01	-96.3104105E+02	31.9089490E+00	48.1739875E+03
37.6160437E-03	21.7387154E+04	0.	10.4988327E+03	-22.5909581E-01	-96.3104105E+02	31.9089490E+00	48.1739875E+03
HJVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DELTA
33.620000E-02	29.253344E+11	0.	0.	-10.8739379E+03	15.3132511E+02	0.	-48.3122901E-01
12.869757E-02	78.398667E-02	13.9944945E+02	0.	0.	0.	0.	37.0160437E-03

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 58

12.8697577E-02 78.3996627E-02 13.9944945E+02 0. -10.8739379E+03 15.3132511E+02 0. 37.0160437E-03

SD2 SD1 S S2D2 S2D1 S2 OMETO1 OMET

0. 0. 0. 0. 0. 0. 0. 0.

-20.9124491E-01 -10.6717516E-01 14.3687757E-01 0. 0. 0. 19.6323732E+01 -26.7940119E+01

-20.9124491E-01 -10.6717516E-01 14.3687757E-01 0. 0. 0. 19.6323732E+01 -26.7940119E+01

FTRA FTRB FTRC HTX HTY MTZ FXH FYH

63.1680171E+02 0. -2.9976653E+03 0. -10.886680E+03 0. 63.1680171E+02 0.

FZN LH NM NH

-20.5318193E+03 0. -10.1690656E+03 0.

VPCS

38.7489900E+02

TFFS

0. 0.

T(II)

SAC1

32.0214541E-03 -39.5826770E-04 44.0490521E-02 0. 0. 22.9158559E-03 0.

FLEX

POINT X02F X02T Y02F Y02T Z02F Z02T X01F

X01T Y01F Y01T Z01F Z01T Y01F Y01F Z01F

10.000000E-01 0. 16.6946822E-01 0. 0. 34.2132481E-01 -23.7162357E+00 0.

28.8933000E+01 0. -15.4642922E-03 48.2410273E+03 0. -32.2558120E-01 -29.7845367E+00 -13.1666354E-03

20.000000E-01 0. 17.9795598E-01 0. 0. 0. 0. 0.

28.8633530E+01 0. 37.1352088E-02 48.2122554E+00 0. 0. 0. 0.

30.000000E-01 0. 18.3156139E-01 0. 0. -10.3734877E+00 -34.0110324E+00 0.

28.8903800E+01 0. 12.6006293E-02 45.8886956E+00 0. 0. 0. 93.5569417E-04

28.8903800E+01 0. 18.5626427E-01 0. 0. 10.2196316E+00 -11.1474792E+00 0.

28.8933213E+01 0. 0. -57.9108470E-02 43.5672051E+00 0. 0. -16.1506179E-03

ISS = 1 LANDING ROLL ICS = 0 IBS = 1

ILR = 1

AUTS

TI TR

H-25

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 70

38.7489900E+02

TFFS

0.

0.

0.

0.

T(I)

SAC1

31.9848926E-03-36.1983351E-04 43.6987692E-02 0.

0.

23.9731442E-03 0.

FLEX

POINT XD1T	XD2F YD1F	X02T YD1T	Y02F ZD1F	Y02T ZD1T	Z02F XD0F	Z02T YD0F	XD1F ZD0F
10.003000E-01	0.	97.0243337E-02	0.	0.	-73.1327717E-01	31.5580357E+00	0.
28.4912536E+01	0.	-49.6176095E-03	48.0172686E+00	0.	0.	0.	-13.4519269E-03
20.1000000E+01	0.	11.4917580E-01	0.	0.	-16.7565586E+00	-40.3057253E+00	0.
28.8810000E+01	0.	14.7830168E-02	47.8121304E+00	0.	0.	0.	11.6566985E-04
30.0030000E+01	0.	11.6104733E-01	0.	0.	-14.8139434E+00	-34.8437167E+00	0.
28.8800000E+01	0.	-17.5585320E-02	49.4755215E+00	0.	0.	0.	90.1420992E-04
28.8913000E+01	0.	11.8457233E-01	0.	0.	33.5923133E+00	16.2803981E+00	0.
28.8913000E+01	0.	-86.2943275E-03	43.9990078E+00	0.	0.	0.	-23.6065469E-03

AUTS

ISS = 1

ILR = 1

LANDING ROLL

ICS = 0

IBS = 1

TI

TR

17.1000000E-02 55.0000000E-02

PITCH AUTOPILOT

DELQN	ALPHA	ALP101	ALPBD1	ALPHET	DELQDE
30.2904646E-01	21.0562187E-02	76.0178610E-02	0.	21.0562187E-02	48.6654646E-01

INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03

2SDF

74.1000000E-02	74.1000000E-02	21.7890139E+01	0.	75.0830519E-01	28.8867584E+01	0.	45.7522395E+00
0.	-51.1927319E-03	0.	26.1974251E-02	29.2468372E+01	10.1635859E+01	29.2464688E+01	0.
-14.6966600E-01	90.0000210E-01	0.	-19.9883486E-02	0.	28.7919016E-02	0.	92.8793611E-01

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 71

0. 0. 18.0240735E-02 0. -18.4225605E+00 12.4671000E+04 0. 0.

LGEAR
DELTA P P2 FT SR SF AA FC2

0. 35.281000E+03 0. 0. -16.5788019E-01 -38.9549765E+02 -78.8562277E+01 0. 0.
18.2019808E-04 19.1724125E+04 0. 14.3985854E+01 19.5192103E+00 21.6134884E+01 13.2417435E+00 51.4680970E+03
18.2019808E-04 19.1724125E+04 0. 14.3985854E+01 19.5192103E+00 21.6134884E+01 13.2417435E+00 51.4680970E+03

HUVP VGP FTRX FTRY FTRZ HA HB DDELTA

33.6003500E-02 29.2353357E+01 0. 0. -0. 0. 0. -48.1894118E-01
33.6003500E-02 29.2353357E+01 0. 0. -15.4381825E+01 58.5861138E+00 0. 18.2019808E-04
33.6003500E-02 29.2353357E+01 0. 0. -15.4381825E+01 58.5861138E+00 0. 18.2019808E-04

S02 S01 S S202 S201 S2 OHETO1 OHET

0. 0. 0. 0. 0. 0. 0. 0.
10.0876391E-01 -11.0315933E-01 13.9308167E-01 0. 0. 0. 75.110423E-01 -26.2592978E+01
10.0876391E-01 -11.0315933E-01 13.9308167E-01 0. 0. 0. 75.110423E-01 -26.2592978E+01

FTRA FTRB FTRC MTX HTY HTZ FXH FYH

15.2217693E+01 0. -28.7971708E+01 0. 21.2927187E+01 0. 15.2217693E+01 0.

FZH LH NH NM

-49.7638287E+01 0. -25.6775193E+02 0.

VPCS
38.7489903E+02

TFFS
0. 0.

0. 0.

T(I)

SAC1
31.9527065E-03 -33.4850903E-04 43.4528884E-02 0. 0. 24.9657752E-03 0.

FLEX
POINT XD1F XD2F XD0F XD1T XD2T XD0F XD1F XD0F

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 72

10.000000E-01	0.	93.9492732E-03	0.	2.	-11.2839123E+00	-33.7397308E+00	0.
28.8868426E-01	0.	-26.4411418E-02	47.6720530E+00	0.	0.	0.	-16.4486692E-03
28.8868426E-01	0.	28.6877577E-02	0.	0.	-11.8710242E+00	-33.4150007E+00	0.
28.8868426E-01	0.	-16.9101043E-02	47.3791484E+00	0.	0.	0.	77.8881037E-05
28.8868426E-01	0.	28.5568752E-02	0.	0.	59.3991323E-01	-12.2155809E+00	0.
28.8868426E-01	0.	-28.6777634E-02	49.3201432E+00	0.	0.	0.	36.7752408E-04
28.8868426E-01	0.	21.5692812E-02	0.	0.	14.0120145E+00	-13.5399271E-01	0.
28.8868426E-01	0.	48.3736110E-02	44.5607457E+00	0.	0.	0.	-19.1665537E-03

AUTS

ISS = 1

LANDING ROLL

ILR = 1

ICS = 0

IBS = 1

TI

TR

17.100000E-02 57.000000E-02

PITCH AUTOPILOT

DELQW	ALPHA E	ALPHD1	ALPD01	ALPHET	DELQDE
30.2934646E-01	21.0562187E-02	19.9883486E-02	0.	21.0562187E-02	49.7154646E-01

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 169

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IDS = 1

TI TR

17.1000000E-02 18.6450000E-01

PITCH AUTOPILOT

DELQD	ALPHA	ALPHD1	ALPHD1	ALPHET	DELQDE
30.294646E-01	21.056218E-02	11.191556E+00	0.	21.056218E-02	80.0000000E-01
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			

2SDF

20.5550000E-01	20.5550000E-01	60.0413284E+01	0.	69.8592229E-01	28.9889488E+01	0.	69.3210286E-01
0.	-10.034614E-02	0.	25.9738118E-02	28.9972350E+01	99.9100078E+00	28.9972259E+01	0.
24.2357939E-02	13.0984808E-01	0.	-11.1671868E+00	0.	-47.8868178E-03	0.	13.2196045E-01
0.	0.	-14.0517111E-01	0.	-33.7974475E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
01.7922661E-03	57.6562948E+03	0.	12.8245160E+03	-12.5554962E+00	-12.6709702E+03	31.0821374E+00	-59.0653689E+02
13.2834932E-02	24.4486291E+04	0.	66.3766017E+03	-16.9343500E+01	-65.9287095E+03	23.1461525E+00	-16.1707501E+00
13.2834932E-02	24.4486291E+04	0.	66.3766017E+03	-16.9343500E+01	-65.9287095E+03	23.1461525E+00	-16.1707501E+00
HJVP	VGPT	FTRX	FTRY	FTRZ	HA	HD	ODELTA
33.6001000E-02	15.2671276E+01	-42.7702158E+02	0.	-12.7292369E+03	-41.3213506E+02	0.	81.7922661E-03
01.7810560E-05	55.2299775E-04	-60.6603934E+00	0.	-66.0027935E+01	-61.5042568E+00	0.	13.2834932E-02
91.7810260E-05	55.2299775E-04	-60.6603934E+00	0.	-66.0027935E+01	-60.5642568E+00	0.	13.2834932E-02
SJ2	SJ1	S	S2D2	S2D1	S2	ONEID1	OMET
-13.6387954E+00	05.7133448E-01	56.7512157E-02	0.	0.	0.	-17.2172294E+02	-10.0772319E+01
-28.9536341E+00	19.0859136E-02	14.7314386E-01	0.	0.	0.	-77.6464830E-01	-20.9298086E+01
-28.9536341E+00	19.0859136E-02	14.7314386E-01	0.	0.	0.	-77.6464830E-01	-20.9298086E+01
FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYH
-10.5391220E+02	0.	-14.4977719E+04	0.	60.6772899E+03	0.	-10.5391220E+02	0.

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 170

FZH LH MH NH
-14.5735198E+04 0. 59.4568336E+03 0.
VPCS
38.7489930E+02
TFFS
0. 0.

T(I)

SAC1
32.4577088E-03 27.3828659E-03-92.1238154E-03 0. 0. 66.8353282E-04 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD6F	ZD2T YD6F	XD1F ZD6F
18.0010000E-01 0.	-27.6738317E-01 0.	0. 0.	0. 0.	0. 0.	-10.0066779E+00-46.4665700E+00 0.	-28.4726180E-04 0.	
28.9893028E+01 0.	-44.6954232E-02 0.	14.5684149E+03 0.	-86.5751179E-01-44.7179974E+00 0.	-28.4726180E-04 0.			
28.9526555E+01 0.	-24.5688827E-01 0.	13.3471438E+03 0.	-86.5751179E-01-44.7179974E+00 0.	-14.9213231E-04 0.			
28.9526555E+01 0.	-23.1539479E-02 0.	13.3471438E+03 0.	-86.5751179E-01-44.7179974E+00 0.	-14.9213231E-04 0.			
28.9526555E+01 0.	-14.657697E-01 0.	13.3471438E+03 0.	-86.5751179E-01-44.7179974E+00 0.	-14.9213231E-04 0.			
28.9791444E+01 0.	58.0533831E-02 0.	68.9484367E-01 0.	-15.4730238E+00-49.1117595E+00 0.	79.5512680E-04 0.			
28.9893028E+01 0.	-74.4193809E-03 0.	35.4626263E-02 0.	31.6113317E+00-16.4817856E-02 0.	-15.4673291E-03 0.			

ISS = 1 LANDING ROLL ILR = 1 ICS = 0 IBS = 1

AUTS

TI

TR

17.1000000E-02 18.8450000E-01

PITCH AUTOPILOT

DELQD	ALPHA	ALPHD1	ALPDD1	ALPHET	DELQDE
36.294646E-01 0.	21.0562187E-02-11.1670868E+00 0.	21.0562187E-02 80.0000000E-01			
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

H-30

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 171

INTEG RTN. HT = 1.000000E+03

2SDF

20.755000E+01 20.755000E+01 60.621220E+01 0. 69.813479E+01 28.987009E+01 0. 58.107400E+01
0. -18.817399E+02 0. 25.969857E+02 28.992033E+01 99.879883E+00 28.992825E+01 0.
21.646930E+02 11.483982E+01 0. -10.960638E+00 0. -42.778250E+03 0. 11.056194E+01
0. 0. -14.165270E+01 0. -33.144287E+00 12.467100E+04 0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
84.793341E+03	67.330077E+03	0.	13.383844E+03	-44.232997E+01	-13.262566E+03	23.849781E+00	-54.071881E+02
13.333494E+02	24.440772E+04	0.	60.251949E+03	-23.595740E+00	-64.918855E+03	48.949913E+00	26.463672E+01
13.388549E+02	24.440772E+04	0.	60.251949E+03	-23.595740E+00	-64.918855E+03	48.949913E+00	26.463672E+01

HUVP	VGPT	FTRX	FTRY	FTRZ	MA	HB	ODELTA
33.633100E+02	11.933715E+01	-44.676757E+02	0.	-13.296653E+03	-43.029335E+02	0.	84.793341E+03
50.947100E+04	33.633719E+03	33.762143E+01	0.	-66.258942E+03	33.700173E+01	0.	13.388549E+02
50.947100E+04	33.633719E+03	33.762143E+01	0.	-66.258942E+03	33.700173E+01	0.	13.388549E+02

SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET
-12.741528E+00	62.874255E+01	69.605800E+02	0.	0.	0.	-17.928889E+02	-17.584544E+01
-68.138369E+01	79.096064E+03	14.730534E+01	0.	0.	0.	43.205223E+00	-28.936746E+01
-68.138369E+01	79.096064E+03	14.730534E+01	0.	0.	0.	43.205223E+00	-28.936746E+01

FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYM
-97.777314E+01	0.	-14.588056E+04	0.	80.648177E+03	0.	-97.777814E+01	0.
FZM	LH	HH	NH				
-14.516360E+04	0.	85.228634E+03	0.				

VPCS

38.748994E+02

TFFS

0. 0.

J.

J.

T(I)

SAC1

ORIGINAL PAGE IS
OF POOR QUALITY

H-31

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 172

32.4624287E-03 28.1404872E-03-1L.3796477E-02 0. 0. 69.8650938E-04 0.

FLEX

POINT XJ1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD1F	ZD2T YD1F	XD1F ZD1F
10.000000E-01	0.	-27.7224516E-01	0.	0.	11.6020426E+00	-24.9473108E+00	0.
28.9872383E+01	0.	-41.0614358E-02	13.4246226E+00	0.	0.	0.	-12.1627660E-03
20.000000E-01	0.	-23.7580276E-01	0.	0.	-58.1479965E-02	-36.5930273E+00	0.
28.9511033E+01	0.	-34.3806872E-02	12.0651897E+00	0.	0.	0.	-75.1315033E-04
30.000000E-01	0.	-12.9740044E-01	0.	0.	-22.8208643E+00	-55.7566329E+00	0.
28.9771063E+01	0.	61.2812503E-03	53.3814132E-01	0.	0.	0.	13.7911403E-03
28.9873594E+01	0.	-30.6224987E-02	84.8105792E-03	-18.5502339E-02	17.6827473E+00	-12.8811427E+00	-18.6019265E-03

AUTS

TI

TR

17.100000E-02 19.045000E-01

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

PITCH AUTOPILOT

DELQX

ALPHA E

ALPDD1

ALPDD1

ALPHET

DELQDE

30.294646E-01 21.0562187E-02-16.9606386E+00 0. 21.0562187E-02 80.000000E-01

INTEG RTN. HT = 1.000000E-03
INTEG RTN. HT = 1.000000E-03
INTEG RTN. HT = 1.000000E-03
INTEG RTN. HT = 1.000000E-03

ZSDF

20.955000E-01	20.955000E-01	51.2010446E+01	0.	69.7712021E-01	24.9849584E+01	0.	47.2138386E-01
0.	-18.645607E-02	0.	29.9662478E-02	24.9888035E+01	09.8519337E+00	28.9887957E+01	0.
21.2873019E-02	93.3213165E-02	0.	-10.5340196E+00	0.	-42.0731299E-03	0.	89.1139243E-02
0.	0.	-15.8204176E-01	0.	-31.5481060E+00	12.4671000E+04	0.	0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FG2

90.9370316E-03	80.2981199E+03	0.	14.5466983E+03	82.8204754E-01	-14.4480851E+03	19.9621929E+00	-51.1812095E+02
12.8217694E-02	24.1699563E+04	0.	62.8546452E+03	17.5880997E-01	-62.1616097E+03	25.4831275E+00	23.0253053E+02
12.8217694E-02	24.1699563E+04	0.	62.8546452E+03	17.5380597E-01	-62.1616097E+03	25.4831275E+00	23.0253053E+02

H-33

ORIGINAL PAGE IS
OF POOR QUALITY

ISS = 1 ILR = 1 LANDING ROLL ICS = 0 IBS = 1

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 174

AUTS

TI

TR

17.100000E-02 19.245000E-01

PITCH AUTOPILOT

DELQN	ALPHA	ALP+01	ALP+01	ALPHET	DELQDE
30.2944646E-01	21.0562187E-02	10.5340136E+00	0.	21.0562187E-02	80.0000000E-01
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			
INTEG RTN.	HT =	1.0000000E-03			

2SDF

21.1331000E-01	21.1300000E-01	61.7483148E+01	0.	69.7323817E-01	28.9823225E+01	0.	38.0240418E-01
0.	-18.3812837E-02	0.	25.9626763E-02	28.9848167E+01	99.8244818E+00	28.9848073E+01	0.
23.2964272E-02	75.1662359E-02	0.	-13.2555551E+00	0.	-46.0508458E-03	0.	70.5611107E-02
0.	0.	-21.5084137E-01	0.	-30.8678924E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
10.6144296E-02	36.2956605E+03	0.	16.3314726E+03	11.2671449E+04	-16.2324229E+03	20.4505472E+00	-50.7333807E+02
12.5564121E-02	23.8447507E+04	0.	61.0332972E+03	18.5921402E+00	-60.6217465E+03	15.1328382E+00	29.4036923E+02
12.5564121E-02	23.8447507E+04	0.	61.0332972E+03	18.5921402E+00	-60.6217465E+03	15.1328382E+00	29.4036923E+02

NUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DOELTA
33.6011000E-02	52.9385554E+01	-54.6517533E+02	0.	-16.2654028E+03	-51.7976422E+02	0.	10.0140296E-02
12.5567923E-04	72.9212373E-04	73.5932524E+00	0.	-61.0383321E+03	74.0119891E+00	0.	12.5564121E-02
12.5567923E-04	72.9212373E-04	73.5932524E+00	0.	-61.0383321E+03	74.0119891E+00	0.	12.5564121E-02

S02	S01	S	S202	S201	S2	OMETD1	OMET
-85.3068083E-02	60.923449E-01	92.6532391E-02	0.	0.	0.	-21.5823509E+02	-24.8716125E+01
15.5341814E-01	-26.3651805E-02	14.6527482E-01	0.	0.	0.	94.8871655E-01	28.7127893E+01
15.5341814E-01	-26.3651805E-02	14.6527482E-01	0.	0.	0.	94.8871655E-01	28.7127893E+01

FTRA	FTRD	FTRJ	HTX	HTY	HTZ	FXH	FYH
-36.139096E+02	0.	-13.8398067E+04	0.	19.7218387E+04	0.	-36.139096E+02	0.
FZH	LH	HH	NH				

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 175

-13.9307929E+04 0.
VPCS
38.7489900E+02
TFFS
0. 0.

19.7660530E+04 0.

T(I)

SAC1

32.4711047E-03 29.5587475E-03-12.439990E-02 0.

0.

74.8161385E-04 0.

FLEX

POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F
10.000000E-01 0.	-35.7024372E-01 0.	0.	0.	0.	-22.2741677E-02-37.5187541E+00 0.	0.	-19.3433300E-03
28.9820780E+01 0.	-68.3458128E-03 11.5767454E+00 0.	0.	0.	0.	15.2820319E+00-20.9255690E+00 0.	0.	-15.4678876E-03
28.9820780E+01 0.	-30.5649040E-01 0.	0.	0.	0.	16.8343189E+00-13.5591278E+00 0.	0.	95.3201822E-04
28.9820780E+01 0.	25.5442167E-03 10.2767092E+00 0.	0.	0.	0.	-14.0614410E-02-22.8148590E-01 0.	0.	-14.6501842E-03
28.9820780E+01 0.	-19.7463728E-01 0.	0.	0.	0.	21.3242727E+00-47.2153947E+00 0.	0.	
28.9820780E+01 0.	-36.8352118E-04 32.7693659E-01 0.	0.	0.	0.			
28.9820780E+01 0.	-1.0892534E-01 0.	0.	0.	0.			

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1300000E-02 19.4200000E-01

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHO1

ALPOJ1

ALPHET

DELQDE

30.2904646E-01 21.0562187E-02-1.2555551E+00 0.

21.0562187E-02 80.0000000E-01

STAGE ON--INCR. DELTA1

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ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 176

PRINT .05
AMAXER .01
DELTS .01
INDSTF 1

TRA

ZSOF

21.1300000E-01 21.1300000E-01 61.7083148E+01 0. 69.7321817E-01 28.9823225E+51 0. 38.0246410E-01
0. -18.3812837E-02 0. 29.9626763E-02 28.9849167E+01 99.8244818E+00 28.9848073E+01 0.
23.2964272E-02 79.1662359E-02 -21.5684137E-01 0. -10.2595551E+00 0. -48.0568458E-03 0. 79.5611107E-02
0. 0. 0. 0. 0. 0. 0. 0.

LGEAR

DELTA	P	P2	FT	SQ	SF	AA	FC2
16.6140296E-02	96.2956655E+03	0.	16.3314726E+03	11.2671449E+00	16.2324229E+03	20.0505472E+00	50.7333807E+02
16.5580112E-02	33.804757E+04	0.	61.0332972E+03	18.5921402E+00	60.6217469E+03	15.1328382E+00	29.4036920E+02
12.5560121E-02	23.804757E+04	0.	61.0332972E+03	18.5921402E+00	60.6217469E+03	15.1328382E+00	29.4036920E+02

HJVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDelta
33.6010000E-02	52.338554E+01	54.6517533E+02	0.	-16.2654028E+03	51.7976422E+02	0.	13.141296E-02
102.1507923E-04	72.5312373E-04	73.5932524E+00	0.	-61.0381321E+03	74.0119891E+00	0.	12.5563121E-02
102.0567923E-04	72.5312373E-04	73.5932524E+00	0.	-61.0381321E+03	74.0119891E+00	0.	12.5563121E-02

S02	S01	S	S202	S201	S2	OMETD1	OMET
-85.3868083E-02	66.9023449E-01	92.6532393E-02	0.	0.	0.	-21.5823509E+02	-24.8716129E+01
15.5341814E-01	-26.365185E-02	14.6527483E-01	0.	0.	0.	94.8871655E-01	-28.7127893E+01
15.5341814E-01	-26.365185E-02	14.6527482E-01	0.	0.	0.	94.8871655E-01	-28.7127893E+01

FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYM
-36.139096E+02	0.	-13.8398167E+04	0.	19.7210387E+04	0.	-36.139096E+02	0.
0.	0.	0.	0.	0.	0.	0.	0.

FZM	LH	MM	NM
-13.9337925E+04	0.	19.7660533E+04	0.

VPOS

38.7489940E+02

TFFS

0. 0.

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 177

T(I)

0.

J.

SAC1

32.4711647E-03 29.5587475E-03-12.4390990E-02 0.

0.

74.8161385E-04 0.

FLEX

POINT XD1T	X02F YD1F	X02T YD1T	Y02F ZD1F	Y02T ZD1T	Z02F XD0F	Z02T YD0F	XD1F ZD0F
10.6000000E-01	0.	-35.7024372E-01	0.	0.	-22.2740677E-02	-37.5187541E+00	0.
23.9820780E+01	0.	0.	-68.3458128E-03	11.5767454E+00	0.	0.	-19.3433300E-03
24.0000000E-01	0.	-36.5649040E-01	0.	0.	15.2820319E+00	-20.9255690E+00	0.
25.9473750E+01	0.	0.	25.5442167E-03	10.2767192E+00	0.	0.	-15.4678876E-03
26.0000000E-01	0.	-19.7463728E-01	0.	0.	15.8343189E+00	-13.5591278E+00	0.
28.9727800E+01	0.	0.	-36.8352118E-04	32.7693659E-01	0.	0.	95.3201822E-04
29.0000000E-01	0.	-10.0892534E-01	0.	0.	-21.3242727E+00	-47.2153947E+00	0.
28.9825918E+01	0.	0.	-14.0614410E-02	-22.8148593E-01	0.	0.	-14.6561842E-03

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

17.1030000E-02 19.4200000E-01

PITCH AUTOPILOT

DELQN	ALPHA	ALPHA01	ALPHA001	ALPHET	DELQDE
36.2904646E-01	21.0562187E-02	-16.2555551E+00	0.	21.0562187E-02	80.0800000E-01

INTEG RTN.	HT =	4.0000000E-03
INTEG RTN.	HT =	4.0000000E-03
INTEG RTN.	HT =	4.0000000E-03
INTEG RTN.	HT =	4.0000000E-03
INTEG RTN.	HT =	2.0000000E-03

2SDF

21.6300000E-01	21.6300000E-01	63.1572389E+01	0.	69.6062074E-01	28.9736126E+11	0.	12.3691956E-01
0.	-17.1366115E-02	0.	25.9528758E-02	28.9738766E+01	99.7491772E+00	28.9738653E+01	0.
25.6417159E-02	24.4601325E-02	-98.2366649E-01	0.	0.	-50.7058194E-03	0.	19.3894879E-02
0.	0.	-12.6788353E-01	0.	-32.1912305E+00	12.4671003E+04	0.	0.

LGEAR

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ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INOSOF 2		CASE LROLL	STAGE 1	PAGE 178			
DELTA	P	P2	FT	SR	SF	AA	FG2
14.8816477E-02	26.9111151E+04	0.	26.2864463E+03	-24.3181405E+03	-26.3465149E+03	-12.1596274E+00	-31.8675270E+02
12.6227975E-02	23.1584345E+04	0.	61.4994761E+03	-22.1256733E+03	-60.2529306E+03	49.6887580E+00	15.8192198E+02
12.6227975E-02	23.1584445E+04	0.	61.4954761E+03	-22.1256733E+03	-60.2529306E+03	49.6887580E+00	15.8192198E+02
HUVP	VGPT	FTRK	FTRY	FTRZ	HA	MB	DOELTA
60.6192112E-03	36.4579642E-02	-15.9314534E+02	0.	-26.2812654E+03	-14.3239851E+02	0.	14.8816477E-02
99.1297582E-04	59.5659628E-03	61.912171E+01	0.	-61.4974892E+03	61.257645E+01	0.	12.6227975E-02
99.6297682E-04	59.5659628E-03	61.9012171E+01	0.	-61.4974892E+03	61.257645E+01	0.	12.6227975E-02
S22	SD1	S	S202	S2D1	S2	OMETO1	OMET
-68.6547836E+01	47.6585044E-01	12.155605E-01	0.	0.	0.	-59.6832713E+01	-32.1675815E+01
-86.1673174E-01	-19.3384315E-02	14.5693353E-01	0.	0.	0.	78.4739955E+00	-28.7334419E+01
-78.1673174E-01	-19.3384315E-02	14.5693353E-01	0.	0.	0.	78.4739955E+00	-28.7334419E+01
FIRA	FTRB	FTRC	MTX	MTY	MTZ	FXH	FYH
13.0040424E+01	0.	-14.9277398E+04	0.	57.3297219E+04	0.	13.0040424E+01	0.
FZH	LH	MH	NH				
-14.8774938E+04	0.	58.5663346E+04	0.				
VPCS							
38.7489906E+02							
IFFS							
0.	0.	0.	0.	0.	0.	0.	0.
SAC1							
32.4817894E-03	31.4967163E-03	-15.0125452E-02	0.	0.	80.2509151E-04	0.	0.
FLEX							
POINT XJ1T	X02F YD1F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X0GF	Z02T Y0JF	X01F Z0JF
10.6000000E-01	0.	-25.7354154E-01	0.	0.	65.6372493E-01	-42.5714092E+00	0.
28.9739669E+01	0.	0.	12.9788761E-02	86.7833496E-01	0.	0.	-20.6752775E-03
28.0000000E-01	0.	-10.0148153E-01	0.	0.	-10.3166621E+00	-56.4940768E+00	0.
28.9408337E+01	0.	0.	18.2934499E-02	76.3193889E-01	0.	0.	-41.5913206E-04
30.0000000E-01	0.	-88.8891344E-02	0.	0.	-23.2123723E+00	-54.2914674E+00	0.

GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 179

28.9646371E+01 0. 0. -25.5797450E-02 49.4671263E-02 0. 0. 14.1789583E-03
 40.8000000E-01 0. -38.3515171E-02 0. 0. 37.0534446E+00 17.7002194E+00 0.
 28.9741035E+01 0. 0. 15.6479493E-02 41.4743296E-01 0. 0. -28.9934957E-03

ISS = 1 LANDING ROLL ILR = 1 ICS = 0 IDS = 1

AUTS

YI

TR

17.1000000E-02 19.9200000E-01

PITCH AUTOPILOT

DELQN ALPHAE ALPDO1 ALPDO1 ALPHET DELQDE
 30.2914646E-01 21.0562187E-02 98.2066649E-01 J. 21.0562187E-02 80.0000000E-01
 INTEG RTN. HT = 2.0000000E-03
 INTEG RTN. HT = 2.0000000E-03
 INTEG RTN. HT = 2.0000000E-03
 TIRE DEFLECTION EXCEEDED DELTA(1) = 1.9917309E-01

ZSOF

21.8553040E-01 21.8553040E-01 63.8031144E+01 0. 69.5482273E-01 28.9704782E+01 0. 15.7244624E-02
 0. -15.9786589E-02 0. 25.9498354E-02 28.9704825E+01 99.7258250E+00 28.9704710E+01 0.
 25.9273863E-02 31.0987357E-03 0. -91.6885961E-01 0. -51.2784711E-03 0. -20.1798159E-03
 0. 0. -17.8629617E-01 0. -32.1501550E+00 12.4671000E+04 0.

LGEAR

DELTA P P2 FT SR SF AA FC2
 19.9173088E-02 32.2147444E+04 0. 37.0899260E+03 -28.1332604E+00 -37.1357980E+03 -92.8566483E-01 -12.5131382E+02
 11.8311685E-02 22.7169475E+04 0. 55.1221124E+03 85.3309320E-01 -55.5317656E+03 21.7072375E+00 51.0746433E+02
 11.8311685E-02 22.7169475E+04 0. 55.1221124E+03 85.3309320E-01 -55.5317656E+03 21.7072375E+00 51.0746433E+02
 HJVP VGPT FTRX FTRY FTRZ HA HB DDELTA
 84.4133224E-03 55.7765574E-02 3.3097823E+02 0. -37.0907813E+03 -26.5739777E+02 0. 19.9173088E-02
 12.8033843E-03 77.0070582E-03 71.8415799E+01 0. -55.1221124E+03 72.7711889E+01 0. 11.8311685E-02
 12.8033843E-03 77.0070582E-03 71.8415799E+01 0. -55.1221124E+03 72.7711889E+01 0. 11.8311685E-02
 S02 S01 S S202 S201 S2 QMETD1 QMET
 -69.5922244E+01 30.2461592E-01 13.4365583E-01 0. 0. 0. -11.0724907E+02 -33.9583056E+01
 -19.3363311E-01 -34.7482160E-02 14.5065644E-01 0. 0. 0. 93.2962678E+00 -28.5095365E+01
 -19.3363311E-01 -34.7482160E-02 14.5065644E-01 0. 0. 0. 93.2962678E+00 -28.5095365E+01
 FTRA FTRB FTRC HTX MTY NTZ FXH FYH

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ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 180

-17.4674282E+02 0. -14.9334012E+04 0. 97.0617950E+04 0. -17.4674282E+02 0.

FZH LM NM NM

-15.0122082E+04 0. 98.0392863E+04 0.

VPGS

38.7489900E+02

TFFS

0. 0.

T(I)

SAC1

32.4895541E-03 32.3621948E-03-16.0768728E-02 0. 0. 82.2484753E-04 0.

FLEX

POINT XD1F	XD2F YD1F	XD2I YD1I	YD2F ZD1F	YD2I ZD1I	ZD2F XD0F	ZD2I YD0F	XD1F ZD0F
10.000000E-01 0.	-29.1627213E-01 0.	0.	0.	0.	-95.6925151E-01-69.2378888E+00 0.	0.	-17.4586666E-03
28.9707572E+01 0.	91.9126745E-03 70.6670244E-01 0.	0.	0.	0.	0.	0.	0.
28.600000E-01 0.	-14.3912825E-01 0.	0.	0.	0.	-52.7841694E-01-69.1649461E+00 0.	0.	0.
28.9398944E+01 0.	-26.2787581E-03 57.3678918E-01 0.	0.	0.	0.	0.	0.	-26.2121492E-04
30.600000E-01 0.	-12.2979945E-01 0.	0.	0.	0.	79.1251949E-01-22.4197001E+00 0.	0.	0.
28.9622624E+01 0.	-47.6853089E-02-77.3188444E-02 0.	0.	0.	0.	0.	0.	45.9283742E-04
40.100000E-01 0.	-12.2059032E-01 0.	0.	0.	0.	80.7427623E-01-32.2189691E-01 0.	0.	0.
28.9707545E+01 0.	77.8186613E-02-42.3098033E-01 0.	0.	0.	0.	0.	0.	-17.2630082E-03

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

17.1000000E-02 20.1450000E-01

PITCH AUTOPILOT

DELQN

ALPHA E

ALPHA01

ALPHA01

ALPHET

DELQDE

30.294464E-01 21.0562187E-02-91.6885911E-01 0.

21.0562187E-02 80.0000000E-01

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 181

STOP

APPENDIX I

AIRPLANE B FLEXIBLE BODY EXAMPLE 6

```

SCASE TAB
ATABJ1 N
ATABJ2 N
ATAB8C N
ATAB11 N
ATAB11 N
ATAB12 N
ATAB15 N
ATAB16 N
ATAB51 N
ATAB52 N
ATAB53 N
ATAB56 N
ATAB57 N
CTAB.1 13
CTAB.2 13
FTAB.3 13
TTAB13 13
VTAB.1 5
VTAB.2 5
VTAB.3 5
VTAB4 5
VTAB56 5

TRA BCD 3 SDF2-PLANPLANE
NCASE BCD 1 LROLL
REM BCD 4 INTEGRATION INFORMATION
IVARBH 4.
TMAX 4.
AMINER .1 GJ35
PRTMIN .1 GJ1
AMAXER .8 GJ1
DELTS .5
PRINT BCD 3 REQ FOR SDF-2
REH 3 674.899
AHASS 1.1666
HGC7F 1.1666
GAM7D 296.22476
VG77F 1.3594
THTBO .
RWHGR .
IND4PC 1
IND4DD 1
IND4PA 1
IND4PL 1
IND4CM 2
IND4RT 1
IND4GT 1
REM BCD 5 VEHICLE PHYSICAL PROP. DATA
INDVPC 1
XCGRF 2.
VTAB.1 2.0,0.,5300.,1.5800.,1.59702E+6
VTAB.2 2.0,1.59702E+6,5300.,1.59702E+6
VTAB.3 2.0,1.59702E+6,5300.,1.59702E+6
VTAB.4 2.0,1.59702E+6,5300.,1.59702E+6
INDXZS 1
VTAB.6 2.0,1.1E+5,500.,1.1E+5
REM BCD 4 AERODYNAMIC INPUT DATA
INDAER 1
AREFF 1.05
D1RFF 37.7
D2RFF 56.7
INDA.1 1
ATABJ1 -7.9573427E-3,-5.5941985E-3

```

TRA
BCD 3SDF2-PLANPLANE
BCD 1LROLL
BCD 4INTEGRATION INFORMATION

3
 44.
 0015
 001
 001

BCD 3REQJ FOR SDF-2
3674.899
14.1
-1.1666
296.28176
11.3394

1
1
1
1
2
1
1

BCD 5VEHICLE PHYSICAL PROP. DATA

2,0,0,5300,1.
2,1,1,59722E+6,56565,1,59722E+6
2,1,1,59722E+6,56565,1,59722E+6
2,5,1,59722E+6,56565,1,59722E+6

2.0., 1.E+5, 5.0., 1.E+5
BCD AERODYNAMIC INPUT DATA

16.5,
37.7
56.7
-7.9573427E-3, -5.5941985E-3

I-2

ORIGINAL PAGE IS
OF POOR QUALITY

ATAB12	1.4.2.979E-3,8.8931664E-4
INDA12	1
ATAB13	1
INDA13	4.18951E-2,2.11844E-2
ATAB14	1
INDA14	-3.978321E-2,-3.9650349E-2
ATAB15	1
INDA15	5.7452448E-2,3.7645688E-2
ATAB16	1
INDA16	1.4721279E-3,1.2354312E-3
ATAB17	1
INDA17	-1.725E-2,-1.45E-2
ATAB18	1
INDA18	1.25E-4,5.0E-5
ATAB19	1
INDA19	7.3916484E-3,1.7127972E-3
ATAB20	1
INDA20	-5.2147852E-4,1.0238928E-3
ATAB21	1
INDA21	-3.1368631E-4,1.8165268E-5
ATAB22	1
INDA22	8.7E-3,7.3418182E-3
ATAB23	1
INDA23	2.0E-5,3.6363636E-5
ATAB24	BCD ENGINE THRUST DATA
INDTFF	1
INDTSO	1
IT10X	4
ITAB10	-2.,-1.5,-1.,-5,0.,.5,1.,1.5,2.
ITAB11	0.,.1,.,.2,.,.3
ITAB12	0.,.1,.,.2,.,.3
ITAB13	0.,.1,.,.2,.,.3
ITAB14	0.,.1,.,.2,.,.3
ITAB15	0.,.1,.,.2,.,.3
ITAB16	0.,.1,.,.2,.,.3
ITAB17	0.,.1,.,.2,.,.3
ITAB18	0.,.1,.,.2,.,.3
ITAB19	0.,.1,.,.2,.,.3
ITAB20	0.,.1,.,.2,.,.3
IT10W	0.,.1,.,.2,.,.3
REM	BCD
NSTRUT	3 LANDING GEAR DATA
MASS	4.94,.,.1,27.19587,27.19587
RX	35.8833,-2.83867,-2.83867
RY	1.91567,.,.919583,.,.919583
RZ	1.91567,.,.919583,.,.919583
THETA0	0.
ERDEG	0.
RGR	4.47
NTIRES	2.3,.,.3
RZERO	1.1475167,1.13125,1.13125
W	.384107,.,.384167,.,.384167
DELTAM	.199333,.,.199333,.,.199333
RLT	1.5E+3
IFO	1
AI	1.32.4533E+5,3.8129286E+5,3.8129286E+5
BI	1.2112257,1.412391,1.412391
FTAB12	2.1,.,.1,.,.1,.,.1
FTAB13	6.1,.,.1,.,.1,.,.1
MOMENT	1.2,2.6,2.6
MB	1.7,.,.1
RF	5.48333,6.8792,6.8792
VZ	0.
PZERO	35281.,40323,.,4.321
VZERO	0.1614583,.,.4716435,.,.4716435
A	.1104166,.,.2673611,.,.2673611

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REM BCD 5N, THROTTLE AUTOPILOT DATA
 IF INT 0.0
 NDF 0.0
 IR INT 0.0
 NR 1.0
 NLR 1.0
 NTO 0.0
 K2 1.0
 REM BCD 40. BRAKE AUTOPILOT DATA
 MBC 0.0
 PD 0.0
 DELTA 0.0
 QMECD1 20.0

MBL 0.0
 MBU 0.0
 REM BCD 5P. CONTROL RESPONSE DATA
 DELHS 0.0
 DELRPO 0.0
 DELA 0.0
 NED1 0.0
 REM BCD 40. INITIALIZATION
 IAP 0.0
 HR 0.0
 DELOO 4.55478
 DELODE 4.55478
 DELQN 4.55478
 DELPO 0.0
 DELRD 0.0
 MANLOG 0.0
 PITCHP 0.0

REM BCD 2STAGING DATA
 REM BCD 4A.GEARS INTO PROGRAM
 INDLG 0.0
 ISTAGE 0.0
 DECREES 0.0
 STESTD 0.0
 TRA 0.0
 INDLG 0.0
 REM BCD 4B.SMOOTH IMPACT STAGE
 AINCRS BCD 3CDELTA1DELTA2DELTA3
 STEST -0.05, -0.05, -0.05
 TRA 0.0
 PRINT 0.0
 DELTS 0.0
 AMAXER 0.0
 PRMIN 0.0
 AINCRS BCD 1TIMES
 STEST 0.0
 TRA 0.0

ATAS1 7.3516484E-3, 1.7.27972E-3
 ATAS2 -5.2147852E-4, 1.238928E-3
 ATAS3 -3.1358631E-4, 1.8.69268E-5
 ATAS4 0.0
 ATAS5 0.0
 ATAS6 0.0
 ATAS7 0.0

REM BCD 5C. EFFICIENT AMAXER STAGE
 AINCRS BCD 4DELTA1DELTA2DELTA3
 STEST 0.0
 TRA 0.0
 PRINT 0.0
 AMAXER 0.0
 DELTS 0.0
 REM BCD 4D.SMOOTH IMPACT STAGE
 AINCRS BCD 1DELTA1
 STEST -0.05
 TRA 0.0

ATAS1 7.3516484E-3, 1.7.27972E-3
 ATAS2 -5.2147852E-4, 1.238928E-3
 ATAS3 -3.1358631E-4, 1.8.69268E-5
 ATAS4 0.0
 ATAS5 0.0
 ATAS6 0.0
 ATAS7 0.0

REM BCD 5C. EFFICIENT AMAXER STAGE
 AINCRS BCD 4DELTA1DELTA2DELTA3
 STEST 0.0
 TRA 0.0
 PRINT 0.0
 AMAXER 0.0
 DELTS 0.0
 REM BCD 4D.SMOOTH IMPACT STAGE
 AINCRS BCD 1DELTA1
 STEST -0.05
 TRA 0.0

PRINT 0.0
 AMAXER 0.0
 DELTS 0.0
 REM BCD 4D.SMOOTH IMPACT STAGE
 AINCRS BCD 1DELTA1
 STEST -0.05
 TRA 0.0

```

PRINT      :02
DELTS      :05
AMAXER     :05
REM        BCD 52 EFFICIENT AMAXER STAGE
AINCRS     BCD 10 DELTA1
STEST      :1
          TRA
PRINT      :05
AMAXER     :01
DELTS      :01
INDSTF     1
          TRA

```

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 7

A. GEARS INTO PROGRAM

INITIAL PRINT OUT FOR VPCS

8. XGGRF AREFF D1RFF D2RFF
16.0500000E+02 37.7000000E+00 56.7000000E+00

PRINT CODES IDENTIFYING TIME HISTORY

2SDF	TIMES	XG77F	YG77F	HGC7F	U777F	V777F	W777F
TIME	DI77R	RI77R	AMACH	VA77F	DYNPP	XG77F1	YG77F1
PI77R	ALPHD	BETAD	ALPHD1	BETAD1	GA47D	SIG7D	YH77D
ZG77F1	PHIFD	AX77F	AY77F	AZ77F	WTR7P	FDC	FCX
ESIPD	FCZ						
FCY							
VPCS							
AMASS							
TFFS							
HT	NT						
SAC1							
CAVAH	CA	CN	CY	CL	CH	CNN	

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 8

2SDF

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
0.	0.	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
59.9992281E-01	11.4999986E+00	0.	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.	57.7454851E-01	0.	-31.6515539E+00	12.4671000E+04	0.	0.
0.	0.						

VPCS

38.7489900E+02

TFPS

0. 0.

0.

0.

T(II)

SAC1

29.7745819E-03-20.8749533E-03 60.9750569E-02 0. 0. 15.3281670E-03 0.

FLARE

AUTS

ALPDES

PHIDES

TTO

11.5800000E+00 0. 0.

PITCH AUTOPILOT

DELON

ALPHA

ALPH01

ALP001

ALPHE7

DELODE

26.8544760E-01-14.0024531E-07 0. 0. -14.0024531E-07 26.8544760E-01

INTEG RTN. HT = 1.00000000E-03

2SDF

0.	0.	0.	0.	10.0000000E+00	29.0274042E+01	0.	59.0569126E+00
0.	0.	0.	26.5337670E-02	29.6220760E+01	10.4252977E+01	29.6159990E+01	0.
59.9992281E-01	11.4999986E+00	0.	0.	0.	-11.6059853E-01	0.	10.3393988E+00
0.	0.	90.1422983E-02	0.	-26.3302709E+00	12.4671000E+04	0.	0.
0.	0.						

VPCS

38.7489900E+02

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 9

YFFS

0.

0.

0.

0.

Y(1)

SAC1

29.7745819E-03-20.8749533E-03 60.9750569E-02 0.

0.

15.3281670E-03 0.

FLARE

AUTS

ALPDES

PHIDES

YTD

11.5000000E+00 0.

0.

PITCH AUTOPILOT

DELON

ALPHA E

ALPHD1 .

ALPDD1

ALPHET

DELODE

27.5607208E-01-14.0024531E-07 0.

0.

-14.0024531E-07 27.5607208E-01

STAGE ON--DEGR. HR

I-10

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 10

INDLG -1
REH 800 48. SHOOT THINACT STAGE
ATNCRS 800 300ELT100ELT200ELT3
STEST TRA -.05, -.05, -.05

250F

0. 0. 0. 0. 10.0000000E+00 29.0274042E+01 0. 59.0569126E+00
59.9992281E-01 11.4999986E+00 0. 26.5337670E-02 29.6220760E+01 10.4252977E+01 29.615997 101 10.3393988E+00
0. 0. 90.1422983E-02 0. -26.3102709E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2800000E+03 0. 0. 31.9713310E-01 -38.9549765E+02 -78.8562277E+01 0.
0. 40.3200000E+03 0. 0. 54.9315280E-01 -10.7799996E+03 -39.6383699E+01 0.
0. 40.3200000E+03 0. 0. 54.9315280E-01 -10.7799996E+03 -39.6383699E+01 0.

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DOELTA

33.6000000E-02 29.6159990E+01 0. 0. -0. 0. 0. -79.6899164E-01
33.6000000E-02 29.6159990E+01 0. 0. -0. 0. 0. -10.9046626E-01
33.6000000E-02 29.6159990E+01 0. 0. -0. 0. 0. -10.9046626E-01

SD2

SD1

S

S2D2

S2D1

S2

OHETD1

OHET

0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.

FTRA

FTRB

FTRC

HTX

HTY

HTZ

FXH

FYH

0. 0. 0. 0. 0. 0. 0. 0.

FZH

LH

MM

NH

0. 0. 0. 0.

VPCS

38.7489900E+02

TFFS

0. 0.

I-11

INDSDF 2 CASE LROLL STAGE 1 PAGE 11

Q

Q.

29.7745819E-03-20.0749533E-03 60.9750569E-02 0.

P.

15.3281670E-03 0.

POINT X01T	X02F Y01F	X02Y Y01T	Y02F Z01F	Y02Y Z01T	Z02F X00F	Z02Y Y00F	X01F Z00F
10.0000000E-01	0.	91.2652002E-02	0.	0.	0.	-20.9135646E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	10.5462913E-02
20.0000000E-01	0.	10.2390015E-01	0.	0.	0.	-20.4544208E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	10.7664860E-02
30.0000000E-01	0.	92.5024062E-02	0.	0.	0.	-20.1504011E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	-11.9773242E-02
40.0000000E-01	0.	91.5277229E-02	0.	0.	0.	-20.3726223E+00	0.
29.0274042E+01	0.	0.	0.	59.0569126E+00	0.	0.	22.0022210E-02

FLARE

AUTS

ALPDES

PHIDES

110

11.50000000E+00 0.

1.

PITCH AUTOPILOT

DELOH

ALPHA

AL FHOI

ALP001:

ALPHET

DELQBE

27.5339224E-01-14.0024531E-07 0.

1.

-14.0024531E-07 27.5839224E-09

[illegible]

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OF POOR QUALITY

4-13

[illegible]

50.0000000E+03	50.0000000E+03	14.8031858E+00	0.	95.9255345E-01	29.0027313E+01	0.	59.3321902E+00
	27.2691345E-04	0.	26.5170136E-02	29.6034039E+01	10.4122524E+01	29.5967121E+01	0.
62.9408593E-01	11.5617295E+00	0.	12.6599115E-01	0.	-12.1827675E-01	0.	18.3434516E+00
0.		94.7837143E-02	0.	-2E.7864184E+00	12.4671000E+04	0.	0.

FC2

D.	35.2800000E+03	0.	0.	37.1612726E-01	-38.9549765E+02	-78.6562277E+01	0.
D.	40.3200000E+03	0.	0.	44.6574281E-01	-10.7799996E+03	-39.6383699E+01	0.
D.	40.3200000E+03	0.	0.	44.6574281E-01	-10.7799996E+03	-39.6383699E+01	0.

DELTA

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OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 13

33.6888888E-02 29.5973817E+01 0. 0. -0. 0. 0. -75.5784194E-01
33.6888888E-02 29.5985279E+01 0. 0. -0. 0. 0. -98.1887321E-02
33.6888888E-02 29.5985279E+01 0. 0. -0. 0. 0. -98.1887321E-02

SD2 SD1 S S202 S201 S2 OMEYD1 OMET
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
FTRA FTRB FTRC HTX HTY HTZ FXH FYH
0. 0. 0. 0. 0. 0. 0. 0.
FZH LH MM NM
25.4586471E+00 0. 17.8487823E+01 0.

VPCS
38.7489900E+02
TFFS
0. 0.

T(I)

SAC1
38.8142517E-03-21.9773825E-03 62.1249652E-02 0. 0. 12.2575620E-03 0.

FLEX

POINT YD1T	X02F YD1F	X02T YD1T	Y02F ZD1F	Y02T ZD1T	Z02F X00F	Z02T Y00F	X01F Z00F
18.8888888E-01 0.	95.6591171E-02 0.	0.	51.4324685E-02-28.3408744E+00 0.	0.	0.	0.	0.
29.0027819E+01 0.	13.1318487E-03 0.	59.2289816E+00 0.	59.1828791E-02-27.5350303E+00 0.	0.	0.	0.	18.5681969E-02 0.
20.0000000E-01 0.	18.4579527E-01 0.	16.3322030E-03 0.	59.2528612E+00 0.	0.	0.	0.	10.7952610E-02 0.
29.0032834E+01 0.	0.	0.	59.3247313E+00 0.	0.	0.	0.	0.
30.0000000E-01 0.	96.6655680E-02 0.	0.	-53.6546557E-02-27.1853834E+00 0.	0.	0.	0.	0.
29.0028375E+01 0.	0.	-15.2076542E-03 0.	59.3247313E+00 0.	0.	0.	0.	-12.6042099E-02 0.
40.0000000E-01 0.	95.9324761E-02 0.	0.	87.3935752E-02-24.3453439E+00 0.	0.	0.	0.	0.
29.0027938E+01 0.	0.	24.8658597E-03 0.	59.4452341E+00 0.	0.	0.	0.	22.9254624E-02 0.

FLANE

AUTS

I-14

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INDSOFF 2 CASE LROLL STAGE 1 PAGE 14

ALFDES
11.5000000E+00 0.

PHIDES

INDSOF 2
T

CASE LROL1

STAGE 1

PAGE

14

PITCH - AUTOPILOT

DELOX

ALPHA

ALPHO2

ALP E01

ALPHET

DELODE

28.2700935E-01 61.7294630E-03 12.6599115E-01 0.

61.7294630E-03 20.2700935E-01

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ORIGINAL PHOTO IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 15

INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03
INTEG RTN. HT 1.6000000E-03

2SDF

10.0000000E-02 10.0000000E-02 29.5966769E+00 0. 93.7098797E-01 28.9775545E+02 0. 59.6186786E+00
0. 43.2850607E-04 0. 26.5000497E-02 29.5044962E+01 10.3990553E+01 29.5772144E+01 0.
65.6446534E-01 11.6258534E+00 0. 12.9349867E-01 0. -12.7143277E-01 0. 10.3544256E+00
0. 0. 99.5833827E-02 0. -27.2744307E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FG2

0. 35.2800000E+03 0. 0. 34.9155442E-01 -38.9549765E+02 -78.8562277E+01 0.
0. 40.3200000E+03 0. 0. 39.9567089E-01 -10.7799996E+03 -39.6383699E+01 0.
0. 40.3200000E+03 0. 0. 39.9567089E-01 -10.7799996E+03 -39.6383699E+01 0.

MUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DOELTA

33.6000000E-02 29.5784944E+01 0. 0. -0. 0. 0. -72.4166819E-01
33.6000000E-02 29.5301332E+01 0. 0. -0. 0. 0. -58.8610413E-02
33.6000000E-02 29.5801332E+01 0. 0. -0. 0. 0. -58.8610413E-02

S02

S01

S

S202

S201

S2

OMET01

OMET

0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.
0. 0. 0. 0. 0. 0. 0. 0.

FTRA

FTRB

FTRC

HTX

HTY

HTZ

FXH

FYM

0. 0. 0. 0. 0. 0. 0. 0.

FZN

LM

NH

NH

24.3554817E+00 0. 13.8567145E+01 0.

VPCS

38.7489900E+02

TFFS

I-16

ORIGINAL PAGE IS
OF POOR QUALITY

INOSOF 2 CASE LROLL STAGE 1 PAGE 16

9.

2

T 112

Fig. 2

P.

SAC1

30.2764887E-03-23.1194946E-03 63.3356138E-02 0.

Q.

90.5418689E-04 0.

FLEX

POINT
XDIT

XD2F
YD1F

X02T
Y01T

YD2F
201F

YD2T
201T

ZDZF
XDDF

202T
Y00F

X01F
Z00F

10.	0002000E	-01	0.
20.	9776449E	+01	0.
20.	0000000E	-01	0.
20.	5795323E	+01	0.
30.	0000000E	-01	0.
20.	9777415E	+01	0.
20.	0000000E	-01	0.
20.	9776664E	+01	0.

10.0200456E-01	0.
0.	48.
10.6767046E-01	0.
0.	42.
10.0935864E-01	0.
0.	-43.
10.0557384E-01	0.
0.	72.

0.	48.9324028E-03	0.	59.4615946E+00
42.1630031E-03	0.	59.4014417E+00	0.
43.3613657E-03	0.	59.5890238E+00	0.
72.5014667E-03	0.	59.8473816E+00	0.

86.4210360E-02-27.5360057E+00	0.	15.7159974E-02
37.0598915E-02-28.1584752E+00	0.	10.9455808E-02
0.	0.	0.
-48.1419188E-02-27.6543493E+00	0.	-12.1519492E-02
90.9801357E-02-25.2083722E+00	0.	23.1687110E-02
0.	0.	0.

FLAKE

AUTS

ALPDES

PHIDES

110

11.50000000E+00 0.

Q.

PITCH AUTOPILOT

DELOH

ALPHA

ALFHD1

ALP 001

ALPHET

DELCDE

29.0985706E-01 12.5858422E-02 12.9349867E-01 0.

12.5658422E+02 29.0985706E+01

[illegible]

ORIGINAL PAGE IS
OF POOR QUALITY

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[illegible]

15.0000000E-02	15.0000000E-02	44.3803598E+00	0.	96.3652141E-01	28.9520435E+01	0.	59.9059780E+00
0.	62.8675928E-04	0.	26.4828396E-02	26.5653189E+01	10.3856782E+01	29.5574749E+01	0.
68.1000511E-01	11.6903561E+00	0.	12.8113987E-01	0.	-13.1985334E-01	0.	18.3705021E+00
0.	0.	10.4422113E-01	0.	-27.7778787E+00	12.4671000E+04	0.	0.
0.	0.						

	P	P2	FT	SR	SF	AA	F02
35.2800000E+03	0.	0.	0.	31.4902666E-01	-38.9549765E+02	-78.8562277E+01	0.
40.3200000E+03	0.	0.	0.	5.5811500E-01	-10.7769999E+03	6388699E+01	0.

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2		CASE LROLL		STAGE 1		PAGE 10	
0.	40.3280000E+03 0.	0.	0.	37.5811505E-01-10.7799996E+03-39.6363699E+01	0.	0.	0.
HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.6800000E-02	29.5590914E+01 0.	0.	0.	-0.	0.	0.	-69.1467722E-01
33.6800000E-02	29.5612166E+01 0.	0.	0.	-0.	0.	0.	-24.8322627E-02
33.6800000E-02	29.5612166E+01 0.	0.	0.	-0.	0.	0.	-24.8322627E-02
S02	S01	S	S202	S201	S2	ONETD1	ONET
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
0.	0.	0.	0.	0.	0.	0.	0.
FTRA	FTRB	FTRC	HTX	HTY	MTZ	FXH	FYN
0.	0.	0.	0.	0.	0.	0.	0.
FZH	LH	MH	NH				
92.4689028E-01 0.	0.	40.7664789E+00 0.	0.				
VPCS							
38.7489900E+02							
TFFS							
0.	0.						
	0.	0.					
SAC1							
30.5566271E-03-24.2740905E-03	64.5784391E-02 0.	0.		57.8052216E-04 0.			
FLEX							
POINT	X02F	X02T	Y02F	Y02T	Z02F	Z02T	X01F
X01T	Y01F	Y01T	Z01F	Z01T	X00F	Y00F	Z00F
10.0000000E-01 0.	0.	10.4805605E-01 0.	0.	0.	86.1109423E-02-27.8883618E+00 0.	0.	0.
28.9521634E+01 0.	0.	0.	93.9243789E-03 59.7316679E+00 0.	0.	0.	0.	19.0731982E-02 0.
20.0000000E-01 0.	0.	10.8968562E-01 0.	0.	77.4745869E-03-28.4993856E+00 0.	0.	0.	0.
28.9533183E+01 0.	0.	0.	52.2996503E-03 59.7377182E+00 0.	0.	0.	0.	11.1680365E-02 0.
30.0000000E-01 0.	0.	10.5236131E-01 0.	0.	-17.7023431E-02-27.8902810E+00 0.	0.	0.	0.
28.9522853E+01 0.	0.	0.	-59.5530950E-03 59.8642718E+00 0.	0.	0.	0.	-12.4158096E-02 0.
40.0000000E-01 0.	0.	10.5231357E-01 0.	0.	74.2456941E-02-26.2991382E+00 0.	0.	0.	0.
28.9521921E+01 0.	0.	0.	11.3863919E-02 60.2231144E+00 0.	0.	0.	0.	23.6383140E-02 0.

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INUSOF 2 CASE LROLL STAGE 1 PAGE 19
FLARE

AUTS
ALPDES PHIDES TTD
11.5000000E+00 0. 0.

PITCH AUTOPILOT

DELQN ALPHAE ALPHD1 ALPDD1 ALPHET DELQDE
29.9899793E-01 19.0356113E-02 12.8113987E-01 0. 19.0356113E-02 29.9899793E-01

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INUSDF 2 CASE LROLL STAGE 1 PAGE 58

ISS = 1 ILR = 1 LANDING RCLL ICS = 0 IBS = 1

AUTS

TI

TR

18.9500000E-02 41.8300000E-02

PITCH AUTOPILOT

DELON ALPHAE ALPHD1 ALPOD1 ALPHET DELODE
30.6287623E-01 23.4068797E-02 93.2446600E-01 0. 23.4068797E-02 41.6537623E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SDF

61.9500000E-02 61.9500000E-02 18.2354785E+01 0. 71.5142415E-01 28.8715473E+01 0. 47.9608893E+00
0. -57.4163149E-03 0. 25.2156271E-02 29.2671939E+01 10.1778455E+01 29.2660206E+01 0.
-14.7805606E-01 94.3172749E-01 0. -84.3673478E-01 0. 28.9358045E-02 0. 97.2108469E-01
0. 0. 76.1005372E-01 0. -58.0029239E+00 12.4671000E+04 0. 0.

LGEAR

DELTA P P2 FT SR SF AA FC2
0. 35.2800000E+03 0. 0. -22.7121132E+00 -38.9549765E+02 -78.8562277E+01 0.
14.4163498E-02 30.0659738E+04 0. 72.8463829E+03 -20.9261388E+00 -71.5387212E+03 48.8830984E+00 74.3252619E+02
14.4163498E-02 30.0659738E+04 0. 72.8463829E+03 -20.9261388E+00 -71.5387212E+03 48.8830984E+00 74.3252619E+02

HUVP VGPT FTRX FTRY FTRZ HA HG DDELTA
33.6000000E-02 29.2507029E+01 0. 0. -74.1916000E+03 0. -46.5120153E-01
22.3454122E-03 13.6150710E-02 16.5784190E+02 0. -74.1916000E+03 16.3643336E+02 0. 14.4163498E-02
22.3454122E-03 13.6150710E-02 16.5784190E+02 0. -74.1916000E+03 16.3643336E+02 0. 14.4163498E-02

S02 S01 S S202 S201 S2 OMETO1 OMET
0. 0. 0. 0. 0. 0. 0.
-10.5552666E+00 -41.9177575E-02 15.2750648E-01 0. 0. 0. 20.9799148E+01 -20.6428320E+01
-10.5552666E+00 -41.9177575E-02 15.2750648E-01 0. 0. 0. 20.9799148E+01 -20.6428320E+01

FTRA FTRD FTRC HTX HTY HTZ FXH FYH
28.3228910E+03 0. -14.5692756E+04 0. -24.6930903E+04 0. 28.3228910E+03 0.

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ORIGINAL PAGE
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 59

F2M LM MM NM
-14.6248357E+04 0. -24.8450452E+04 0.
VPCS
38.7489900E+02
TFFS
0. 0.

T(I)

SAC1

32.3808941E-03-71.3372381E-04 48.0572603E-02 0. 0. 16.4362625E-03 0.

FLEX

POINT XD1T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01 0.		75.0560723E-01 0.		0.	-12.2771290E-01-55.2968182E+00 0.		
28.8706559E+01 0.		0.	-43.4240241E-02 49.9763338E+00 0.		0.		14.8119548E-02 0.
28.0000000E-01 0.		73.6289264E-01 0.		0.	35.0469081E-02-54.4240641E+00 0.		0.
28.4500062E+01 0.		0.	-46.0705511E-02 49.5144576E+00 0.		0.		63.6497008E-03 0.
30.0000000E-01 0.		75.2719122E-01 0.		0.	-37.2775762E-02-58.6386750E+00 0.		0.
28.8691540E+01 0.		0.	46.8997422E-02 48.2668208E+00 0.		0.		-93.4361560E-03 0.
40.0000000E-01 0.		77.7685962E-01 0.		0.	-11.8980239E-01-62.1731148E+00 0.		0.
28.8705045E+01 0.		0.	-67.0176070E-02 45.4341743E+00 0.		0.		18.1617486E-02 0.

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

18.9500000E-02 43.0000000E-02

PITCH AUTOPILOT

DELON

ALPHA E

ALPHO1

ALPDD1

ALPHET

DELODE

38.6287623E-01 23.4068797E-02-34.3673478E-01 0. 23.4068797E-02 42.7037623E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM
INOSDF 2 CASE LROLL STAGE 1 PAGE 60

250F

63.9500000E-02 63.9500000E-02 18.8267719E+01 0. 71.8580541E-01 28.8806971E+01 0. 47.1654653E+00
0. -58.8548507E-03 0. 26.2121385E-02 29.2632957E+01 18.1751242E+01 29.2626548E+01 0.
-19.3679560E-01 92.7517313E-01 0. -71.5439120E-01 0. 37.9216068E-02 0. 96.5438886E-01
0. 0. 67.6663454E-01 0. -51.0686601E+00 12.4671000E+04 0.
0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	35.2800000E+03	0.	0.	-12.5647480E+00	-38.9549765E+02	-78.8562277E+01	0.
12.6841829E-02	28.7971062E+04	0.	60.6639297E+03	-23.8480199E+00	-59.4149457E+03	45.9240317E+00	16.3155628E+03
12.6841829E-02	28.7971062E+04	0.	60.6639297E+03	-23.8480199E+00	-59.4149457E+03	45.9240317E+00	16.3155628E+03

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DOELTA
33.6000000E-02	29.2470994E+01	0.	0.	-0.	0.	0.	-46.5256174E-01
36.3758033E-03	22.2836144E-02	22.6479980E+02	0.	-61.9207126E+03	22.7478343E+02	0.	12.6841829E-02
36.3758033E-03	22.2836144E-02	22.6479980E+02	0.	-61.9207126E+03	22.7478343E+02	0.	12.6841829E-02

SD2	SD1	S	S2D2	S2D1	S2	OMETO1	OMET
0.	0.	0.	0.	0.	0.	0.	0.
-96.4231701E-01	-62.1056120E-02	19.1707475E-01	0.	0.	0.	29.1638901E+01	-29.1375858E+01
-96.4231701E-01	-62.1056120E-02	19.1707475E-01	0.	0.	0.	29.1638901E+01	-29.1375858E+01

FTRA	FTRD	FTPD	HTX	HTY	HTZ	FXH	FYH
25.2342301E+03	0.	-12.1327859E+04	0.	-19.3822051E+04	0.	25.2342301E+03	0.

FZH	LH	HH	NH
-12.1640261E+04	0.	-19.3778949E+04	0.

VPCS

38.7489900E+02

TFFS

0. 0.

0. 0. T(1)

SAC1

32.2692174E-03 -60.3650629E-04 46.6857194E-02 0. 0. 10.1059538E-03 0.

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM
INDSDF 2 CASE LROLL STAGE 1 PAGE 61

FLEX		X02F		X02T		Y02F		Y02T		Z02F		Z02T		X01F	
POINT	X01T	Y01F	Y01T	Z01F	Z01T	X00F	Y00F	Z00F	X00T	Y00T	Z00T	X00F	Y00F	Z00F	X00T
10.000000E-01	0.	0.	66.6487637E-01	0.	0.	-49.2169613E-02	-49.3619608E+00	0.	0.	0.	0.	0.	0.	0.	0.
28.4798776E+01	0.	0.	0.	20.45461E-02	49.2245621E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	13.9231086E-02
20.0000000E-01	0.	0.	65.9032029E-01	0.	0.	49.6357584E-01	-44.3036722E+00	0.	0.	0.	0.	0.	0.	0.	0.
28.8689762E+01	0.	0.	0.	6.457985E-02	48.8238297E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	7.8231520E-03
30.0000000E-01	0.	0.	67.0503001E-01	0.	0.	-43.4929999E-01	-55.5660188E+00	0.	0.	0.	0.	0.	0.	0.	0.
28.8781947E+01	0.	0.	0.	4.0742187E-02	47.4191380E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	-8.4052197E-03
40.0000000E-01	0.	0.	69.4647305E-01	0.	0.	31.9664664E-01	-49.5383407E+00	0.	0.	0.	0.	0.	0.	0.	0.
28.4797069E+01	0.	0.	0.	6.9999634E-02	44.6124942E+00	0.	0.	0.	0.	0.	0.	0.	0.	0.	16.5268183E-02

ISS = 1 ILR = 1 LANDING RCLL ICS = 0 IBS = 1

TI TR
18.9500000E-02 45.0000000E-02

PITCH AUTOPILOT

DELQN	ALPHA	ALPHD1	ALPCD1	ALPHET	DELQDE
30.6287623E-01	23.4066797E-02	71.5439120E-01	0.	23.4066797E-02	43.7537623E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

2SDF

65.9500000E-02	65.9500000E-02	19.4059891E+01	0.	72.2785761E-01	28.8878639E+01	0.	46.5181050E+00
0.	-59.4341048E-03	0.	26.2091966E-02	29.2600072E+01	10.1728249E+01	29.2591494E+01	0.
-22.4047323E-01	31.4780197E-01	0.	-55.4879583E-01	0.	43.8724858E-02	0.	95.8652978E-01
0.	0.	55.6082684E-01	0.	-42.7895583E+00	12.4671800E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FG2
0.	35.2800000E+03	0.	0.	-28.7261411E-01	-38.9549765E+02	-78.8562277E+01	0.
10.3936698E-02	27.2238325E+04	0.	45.6512758E+03	-18.0207715E+00	-44.5268494E+03	41.3454840E+00	27.2235437E+03
10.3936698E-02	27.2238325E+04	0.	45.6512758E+03	-18.0207715E+00	-44.5268494E+03	41.3454840E+00	27.2235437E+03

HUVP VGPT FTRX FTRY FTRZ MA HQ ODELTA

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INOSDF 2 CASE LROLL STAGE 1 PAGE 62

S02		S01		S		S2D2		S2Q1		S2		OHEYD1		OHEY	
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01	-83.5998454E-01
0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.	0.
FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA	FTRA
20.7108987E+03	0.	-91.3025517E+03	0.	-13.3510929E+04	0.	20.7108987E+03	0.	20.7108987E+03	0.	20.7108987E+03	0.	20.7108987E+03	0.	20.7108987E+03	0.
FZH	LM	MM	NH												
-91.4210290E+03	0.	-13.2360062E+04	0.												
VPCS															
38.7489900E+02															
TFFS															
0.	0.														
SAG1															
32.2293161E-03	-51.2492268E-04	45.5342832E-02	0.												
FLEX															
POINT	XD2F	XD2T	YD2F	YD2T	ZD2F	ZD2T	XD1F								
XD1T	YD1F	YD1T	ZD1F	ZD1T	XDDF	YDDF	ZDDF								
10.0000000E-01	0.	54.6301552E-01	0.	46.6010531E+00	46.6010531E+00	46.6010531E+00	46.6010531E+00								
28.8870903E+01	0.	-45.2909000E-02	48.3293365E+00	79.3735706E-01	79.3735706E-01	79.3735706E-01	79.3735706E-01								
20.0000000E-01	0.	54.5525513E-01	0.	0.	0.	0.	0.								
28.3760000E+01	0.	-27.3913030E-02	48.3293365E+00	0.	0.	0.	0.								
30.0000000E-01	0.	55.3150664E-01	0.	0.	0.	0.	0.								
28.8852532E+01	0.	30.4978460E-02	48.3293365E+00	0.	0.	0.	0.								
40.0000000E-01	0.	57.3941032E-01	0.	0.	0.	0.	0.								
28.8869358E+01	0.	-55.0920948E-02	48.3293365E+00	0.	0.	0.	0.								

AUTS

ISS = 1

ILR = 1 LANDING ROLL

$$L_{ICS} = 0$$

TDS = 1

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 63

TI TR

18.950000E-02 47.000000E-02

PITCH AUTOPILOT

DELON ALPHAE ALPHD1 ALPOD1 ALPHET DELODE
30.6247823E-01 23.4068797E-02 55.4879583E-01 0. 23.4068797E-02 44.8837623E-01

INTEG RTN: HT = 1.0000000E-03
INTEG RTN: HT = 1.0000000E-03
INTEG RTN: HT = 1.0000000E-03
INTEG RTN: HT = 1.0000000E-03

250F

67.9500000E-02 67.9500000E-02 13.9911401E+01 0. 72.7426981E-01 28.8924035E+01 0. 46.8403188E+00
0. -59.1354466E-03 0. 26.2864466E-02 29.2569324E+01 10.1706711E+01 29.2559709E+01 0.
-23.7185012E-01 90.5401394E-01 0. -38.3742142E-01 0. 46.480926E-02 0. 95.1851368E-01
0. 0. 41.5011413E-01 0. -34.2416663E+00 12.4671000E+04 0.

LGEAR

DELTA P P2 FT SR SF AA FC2
0. 35.2800000E+03 0. 0. 44.8110571E-01 -38.9549755E+02 -78.4562277E+01 0.
77.3022365E-03 25.5042306E+04 0. 29.9077142E+03 -97.8952900E-01 -28.9593522E+03 34.8715447E+00 38.4609593E+03
77.3022365E-03 25.5042306E+04 0. 29.9077142E+03 -97.8952900E-01 -28.9593522E+03 34.8715447E+00 38.4609593E+03

MUVP VGPT FTRX FTRY FTRZ MA MB DDELTA
33.8000000E-02 29.2449656E+01 0. 0. -0. -30.7660965E+03 0. -46.6661967E-01
85.4617159E-03 52.0561062E-02 26.2932340E+02 0. -30.7660965E+03 27.7116952E+02 0. 77.3022365E-03
85.4617159E-03 52.0561062E-02 26.2932340E+02 0. -30.7660965E+03 27.7116952E+02 0. 77.3022365E-03

SD2 SD1 S S2D2 S2D1 S2 ONETD1 ONET
0. 0. 0. 0. 0. 0. 0. 0.
-66.4901969E-01 -95.3542100E-02 14.8515505E-01 0. 0. 0. 35.5278143E+01 -27.7903985E+01
-66.4901969E-01 -95.3542100E-02 14.8515505E-01 0. 0. 0. 35.5278143E+01 -27.7903985E+01

FTRA FTRB FTRC MTX MTY MTZ FXM FYM
15.3615974E+03 0. -59.8154284E+03 0. -74.6776193E+03 0. 15.3615974E+03 0.

FZN LM MH NM
-59.8165043E+03 0. -73.1378558E+03 0.

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 64

VPCS

38.7489980E+02

TFFS

0.

0.

0.

0.

T(1)

SAC1

32.1844233E-03-44.0877188E-04 44.6352003E-02 0.

0.

21.0374867E-03 0.

FLEX

POINT XD1T	X02F YD1F	X02T Y01T	Y02F ZD1F	Y02T ZD1T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01	0.	40.5635029E-01	0.	0.	16.1407074E-01	34.1325170E+00	0.
20.8916865E+00	0.	0.	-43.2606656E-02	40.1308265E+00	0.	0.	12.1255697E-02
30.0000000E+00	0.	41.1003538E-01	0.	0.	02.3333095E-01	27.2524810E+00	0.
40.0000000E+00	0.	0.	-10.7744051E-02	40.0072413E+00	0.	0.	64.0925864E-03
50.0000000E+00	0.	41.5674268E-01	0.	0.	-73.7496943E-01	41.5182934E+00	0.
60.0000000E+00	0.	0.	15.0263162E-02	46.0307159E+00	0.	0.	-72.4137631E-03
70.0000000E+00	0.	43.1654775E-01	0.	0.	75.2851995E-01	25.5727002E+00	0.
80.0000000E+00	0.	0.	-40.7502886E-02	43.7707718E+00	0.	0.	14.6523810E-02

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

18.9500000E-02 49.0000000E-02

PITCH AUTOPILOT

DELQX

ALPHA E

ALPH01

ALPDD1

ALPHET

DELODE

30.6287623E-01 23.4868797E-02-38.3742142E-01 0.

23.4868797E-02 45.8537623E-01

INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03

ZSDF

I-27

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 65

69.950000E-02 69.950000E-02 20.5762277E+01 0. 73.2162278E-01 28.8940484E+01 0. 45.7297021E+00
0. -58.8556228E-03 0. 26.2035421E-02 29.2536851E+01 18.1684014E+01 29.2527518E+01 0.
-23.3775828E-01 99.9342769E-01 0. -22.6879500E-01 0. 45.7874529E-02 0. 94.5130197E-01
0. 0. 27.3446602E-01 0. -26.6753115E+00 12.4671000E+04 0.
0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

0. 35.2800000E+03 0. 0. 84.5784705E-01 -38.9549765E+02 -78.8562277E+01 0.
49.3319335E-03 23.7767555E+04 0. 15.8041840E+03 -38.8027115E-02 -15.0525910E+03 27.6362912E+00 48.8190304E+03
49.3319335E-03 23.7767555E+04 0. 15.8041840E+03 -38.8027115E-02 -15.0525910E+03 27.6362912E+00 48.8190304E+03

HUVP

VGPT

FTRX

FTRY

FTRZ

MA

MB

DDelta

33.5000000E-02 29.2440577E+01 0. 0. -0. 0. 0. -46.7255999E-01
14.1331083E-02 86.0777598E-02 23.1891768E+02 0. -16.4076977E+03 29.0841515E+02 0. 49.3319335E-03
14.1331083E-02 86.0777598E-02 23.1891768E+02 0. -16.4076977E+03 29.0841515E+02 0. 49.3319335E-03

SQ2

SD1

S

S2D2

S2D1

S2

OMETD1

OMET

0. 0. 0. 0. 0. 0. 0. 0.
-44.3099076E-01 -10.6545843E-01 14.6492302E-01 0. 0. 0. 32.1591686E+01 -27.1055037E+01
-44.3099076E-01 -10.6545843E-01 14.6492302E-01 0. 0. 0. 32.1591686E+01 -27.1055037E+01

FTRA

FTRB

FTRC

MTX

MTY

MTZ

FXH

FYM

99.6347103E+02 0. -31.6033631E+03 0. -26.3904757E+03 0. 99.6347103E+02 0.

FZH

LH

HM

NH

-31.5743247E+03 0. -25.1960146E+03 0.

VPCS

38.7489900E+02

TFFS

0. 0.

0.

0.

T(1)

SAC1

32.1379569E-03 -38.7438832E-04 43.9855243E-02 0.

0.

22.2808682E-03 0.

FLEX

I-28

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
18.0000000E-01	0.	26.4365212E-01	0.	0.	28.5394264E-01	26.1107399E+00	0.
28.8933923E+01	0.	0.	-38.8203020E-02	47.8185409E+00	0.	0.	11.3805968E-02
20.0000000E+01	0.	27.5069491E-01	0.	0.	58.5737511E-01	23.2824492E+00	0.
28.8825626E+01	0.	0.	36.6804113E-03	47.8031653E+00	0.	0.	63.4614578E-03
30.0000000E+01	0.	27.7185595E-01	0.	0.	-56.3633393E-01	32.1144763E+00	0.
28.3915001E+01	0.	0.	25.2491887E-03	45.5901505E+00	0.	0.	-79.6367478E-03
40.0000000E+01	0.	28.8413366E-01	0.	0.	63.4357727E-01	18.0663557E+00	0.
28.5932366E+01	0.	0.	-23.6059955E-02	43.5665123E+00	0.	0.	13.9832406E-02

AUTS ISS = 1 ILR = 1 LANDING RCLL ICS = 0 IRS = 1

II TR
18.9500000E-02 51.0000000E-02

PITCH AUTOPILOT

DELON	ALPHA E	ALFHD1	ALPD01	ALPHET	DELODE
30.6287623E-01	23.4068797E-02	22.6879500E-01	0.	23.4068797E-02	46.9037623E-01
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

2SDF

71.9500000E-02	71.9500000E-02	21.1612473E+01	0.	73.6687401E-01	28.8929026E+01	0.	45.5599224E+00
0.	-56.3997577E-03	0.	26.2001595E-02	29.2499041E+01	10.1657596E+01	29.2491003E+01	0.
-21.6836915E-01	83.6093032E-01	0.	-10.5881588E-01	0.	42.4753271E-02	0.	93.8563226E-01
0.	0.	14.4739581E-01	0.	-21.1149502E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
0.	35.2000000E+03	0.	0.	92.4161051E-01	-38.9549765E+02	-78.8562277E+01	0.
23.5065123E-03	22.1446045E+04	0.	53.8731842E+02	84.2208139E-01	-48.0952364E+02	21.2456808E+00	54.1445551E+03
23.5065123E-03	22.1446045E+04	0.	53.8731842E+02	84.2208139E-01	-48.0952364E+02	21.2456808E+00	54.1445551E+03
MUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA
33.6000000E-02	29.2417017E+01	0.	0.	-0.	0.	0.	-46.7514655E-01
28.0730979E-02	17.0961197E-01	16.0750057E+02	0.	-57.2612463E+02	17.8069829E+02	0.	23.5065123E-03

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INSDOF 2 CASE LROLL STAGE 1 PAGE 67

28.8738979E-02 17.8961197E-01 16.8758057E+02 0. -57.2612463E+02 17.8869829E+02 0. 23.5065123E-03

S02 S01 S S202 S201 S2 ONEYD1 OMEY

-20.7552266E-01-11.3137665E-01 0.4287467E-01 0. 0. 0. 22.8294653E+01-26.5425009E+01

-20.7552266E-01-11.3137665E-01 14.4287467E-01 0. 0. 0. 22.8294653E+01-26.5425009E+01

FYRA FTRR FTRC HTX HTY HTZ FXH FYH

50.3958793E+02 0. -10.7746368E+03 0. 25.8257522E+02 0. 50.3958793E+02 0.

FZH LM HM NM

-10.7625333E+03 0. 29.6276249E+02 0.

VPCS

38.7489900E+02

TFFS

0. 0.

T(I)

SAC1

32.8938338E-03-34.8708621E-04 43.5476730E-02 0. 0. 23.3977329E-03 0.

FLEX

POINT XD1T	X02F YD1F	X02Y YD1T	YD2F ZD1F	Y02Y ZD1T	Z02F XD0F	Z02Y YD0F	X01F ZD0F
10.0000000E-01 0.		13.5744266E-01 0.		0.	48.2825272E-01-21.8109614E+00 0.		18.5890094E-02 0.
20.8923054E+01 0.		0. -31.9359205E-02 0.	47.6469557E+00 0.		0.		0.
20.0000000E-01 0.		15.0512498E-01 0.	0.	18.4342371E-01-22.5044050E+00 0.			0.
20.4817254E+01 0.		0. 11.4317076E-02 0.	47.6534291E+00 0.		0.		65.1108622E-03 0.
30.0000000E-01 0.		15.0318179E-01 0.	0.	-24.6314256E-01-23.3186274E+00 0.			0.
20.8904294E+01 0.		0. -56.9083326E-03 0.	45.3429137E+00 0.		0.		-71.8595375E-03 0.
40.0000000E-01 0.		15.8118619E-01 0.	0.	38.3877955E-01-14.3023198E+00 0.			0.
28.8921377E+01 0.		0. -16.3677711E-02 0.	43.5720544E+00 0.		0.		13.5619304E-02 0.

AUTS

ISS = 1 ILR = 1 LANDING ROLL ICS = 0 IBS = 1

TI TR

I-30

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INCSDF 2 CASE LROLL STAGE 1 PAGE 66

18.9500000E-02 53.0000000E-02

PITCH AUTOPILOT

DELON ALPHAE ALPHD1 ALPDD1 ALPHET DELODE
38.6287623E-01 23.4068797E-02 10.5881588E-01 0. 23.4058797E-02 47.9537623E-01

INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03
INTEG RTN. HT = 1.0000000E-03

ZSDF

73.9500000E-02 73.9500000E-02 21.7461237E+01 0. 74.0776766E-01 28.8889985E+01 0. 45.4856156E+00
0. -54.5157802E-03 0. 26.1656639E-02 29.2448811E+01 10.1622563E+01 29.2442567E+01 0. 93.2213195E-01
-19.1093306E-01 89.4774447E-01 0. -36.2965044E-02 0. 37.4388092E-02 0. 0.
0. 0. 17.2006213E-02 0. -18.2789816E+00 12.4671000E+04 0. 0.

LGEAR

DELTA P P2 FT SR SF AA FC2
0. 35.2800000E+03 0. 0. 79.5363441E-01 -38.9549765E+02 -78.8562277E+01 0.
17.5786541E-04 20.6726346E+04 0. 13.7027887E+01 14.6862970E+00 34.7646702E+01 17.8216247E+00 55.6189763E+03
17.5786541E-04 20.6726346E+04 0. 13.7027887E+01 14.6862970E+00 34.7646702E+01 17.8216247E+00 55.6189763E+03

HUVP VGPT FTRX FTRY FTRZ HA HO DDELTA
33.6000000E-02 29.2368394E+01 0. 0. -0. 0. 0. -46.7395140E-01
33.6000000E-02 49.6348940E+01 49.3812058E+00 0. -14.6867875E+01 55.7756836E+00 0. 17.5786541E-04
33.6000000E-02 49.6348940E+01 49.3812058E+00 0. -14.6867875E+01 55.7756836E+00 0. 17.5786541E-04

SD2 SD1 S S2D2 S2D1 S2 OHETD1 OHET
0. 0. 0. 0. 0. 0. 0. 0.
75.8836669E-02 -11.4669509E-01 14.2000440E-01 0. 0. 0. 71.5072867E-01 -26.3162531E+01
75.8836669E-02 -11.4669509E-01 14.2000440E-01 0. 0. 0. 71.5072867E-01 -26.3162531E+01

FTRA FTRH FTRG MTX MTY HTZ FXH FYM
14.5071263E+01 0. -27.4055774E+01 0. 18.8984778E+01 0. 14.5071263E+01 0.
FZH LH MH NH

-27.3567183E+01 0. -22.4830244E+01 0.

VPCS

I-31

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2 CASE LROLL STAGE 1 PAGE 69

38.7489900E+02

TFFS

0.

0.

0.

0.

T(I)

SAC1

32.0520491E-03-31.9694618E-04 43.2573447E-02 0.

0.

24.4246761E-03 0.

FLEX

POINT XD1T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01	0.	74.6239913E-03	0.	0.	49.4288288E-01	17.3425829E+00	0.
20.0000000E-01	0.	0.	-22.9260696E-02	47.5823634E+00	0.	0.	18.8373818E-02
30.0000000E-01	0.	24.2118824E-02	0.	0.	-22.1775364E-01	23.7968199E+00	0.
40.0000000E-01	0.	0.	10.9484098E-02	47.5076932E+00	0.	0.	57.4895687E-03
50.0000000E-01	0.	22.9240048E-02	0.	0.	95.2503512E-02	17.0614360E+00	0.
60.0000000E-01	0.	0.	-71.0813420E-03	45.2597820E+00	0.	0.	-72.4535831E-03
70.0000000E-01	0.	29.2898734E-02	0.	0.	14.0104714E-01	13.8417762E+00	0.
80.0000000E-01	0.	0.	-11.2959371E-02	43.6099812E+00	0.	0.	13.2934238E-02

AUTS

ISS = 1

LANDING ROLL

ILR = 1

ICS = 0

IBS = 1

TI

TR

1A.9500000E-02 55.0000000E-02

PITCH AUTOPILOT

DELQX

ALPHA

ALPHD1

ALPDD1

ALPHET

DELQDE

38.6287623E-01 23.4068797E-02-36.2965044E-02 0.

23.4068797E-02 49.0037623E-01

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 171

INTEG RYN. HY = 1.00000000E-03

2SOF

20.6425000E-01 20.6425000E-01 60.2928534E+01 0. 69.8211664E-01 20.9863837E+01 0. 56.7672733E-01
0. -10.8595998E-02 0. 25.9690593E-02 20.9019414E+01 99.8735400E+00 20.9919355E+01 0.
19.1827569E-02 11.2194384E-01 0. -11.0753996E+00 0. -37.9090005E-03 0. 10.8403361E-01
0. 0. -15.8768114E-01 0. -33.5759979E+00 12.4671000E+04 0. 0.

LGEAR

DELTA

P

P2

FT

SR

SF

AA

FC2

84.6327626E-03 67.7673702E+03 0. 13.3485730E+03 -70.4168274E-01 -13.2161225E+03 26.8118420E+00 -53.1400445E+02
13.3633280E-02 24.5896209E+04 0. 66.6420522E+03 10.8773436E-01 -65.8765536E+03 28.1476030E+00 -45.1707663E-01
13.3633280E-02 24.5896209E+04 0. 66.6420522E+03 10.8773436E-01 -65.8765536E+03 28.1476030E+00 -45.1707663E-01

HUVP

VGPT

FTRX

FTRY

FTRZ

HA

HB

DDELTA

33.6000000E-02 11.7638308E+01 -44.5758270E+02 0. -13.2668152E+03 -42.9391781E+02 0. 84.6327626E-03
42.8115357E-03 25.7579812E-04 28.5358243E+00 0. -66.6545217E+03 28.4678155E+00 0. 13.3633280E-02
42.8115357E-03 25.7579812E-04 28.5358243E+00 0. -66.6545217E+03 28.4678155E+00 0. 13.3633280E-02

S02

S01

S

S202

S201

S2

OHETD1

OHET

-12.3980823E+00 62.3301353E-01 70.0890735E-02 0. 0. 0. -17.8913242E+02 -17.7539341E+01
-29.3290416E-01 10.0871334E-02 14.7481197E-01 0. 0. 0. 36.4971993E-01 -28.9439227E+01
-29.3290416E-01 10.0871334E-02 14.7481197E-01 0. 0. 0. 36.4971993E-01 -28.9439227E+01

FTRA

FTRB

FTRC

MTX

MTY

HTZ

FXM

FYM

-16.2668395E+02 0. -14.6632677E+04 0. 72.9137976E+03 0. -16.2668395E+02 0.

FZM

LH

HM

NM

-14.6964050E+04 0. 73.7311167E+03 0.

VPCS

38.7489900E+02

TFFS

0.

0.

0.

0.

Y(J)

SAC1

I-33

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 172

32.4617859E-03 24.2314695E-03-10.5182680E-02 0. 0. 70.2123958E-04 0.

FLEX								
POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F	
10.0000000E-01	0.	-28.9778415E-01	0.	13.1674010E+00	-75.8103141E-03	36.7544404E+00	0.	
20.0000000E-01	0.	-56.6094368E-02	0.	0.	0.	0.	-31.1939446E-03	
30.0000000E-01	0.	-25.5366099E-01	0.	0.	-30.1346752E-01	39.2094796E+00	0.	
40.0000000E-01	0.	0.	-38.0662438E-02	11.9126349E+00	0.	0.	-15.3454387E-03	
50.0000000E-01	0.	-16.0632484E-01	0.	0.	23.0670235E-01	31.8809453E+00	0.	
60.0000000E-01	0.	0.	41.8824181E-02	55.6018971E-01	0.	0.	17.8862535E-03	
70.0000000E-01	0.	-13.3067549E-02	0.	0.	-30.0229703E-01	34.2264796E+00	0.	
80.0000000E-01	0.	0.	-68.1836081E-02	-11.0303975E-01	0.	0.	-35.9502801E-03	

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

18.9500000E-02 18.7475000E-01

PITCH AUTOPILOT

DELON	ALPHA	ALFND1	ALPDD1	ALPHET	DEL00E
30.6287623E-01	23.4068797E-02	11.8753996E+00	0.	23.4068797E-02	88.0800000E-01

INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03
INTEG RTN.	HT =	1.0000000E-03

2SDF

20.8425000E-01	20.8425000E-01	60.8726461E+01	0.	69.7854823E-01	28.9836896E+01	0.	45.6862738E-01
0.	-18.6971369E-02	0.	25.9648810E-02	28.9872775E+01	39.8414171E+00	28.9872720E+01	0.
16.5289200E-02	98.1483344E-02	0.	-10.9684351E+00	0.	-32.6706463E-03	0.	88.6812549E-02
0.	0.	-18.9492869E-01	0.	-33.5019935E+00	12.4671000E+04	0.	0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FG2
90.1960707E-03	80.7130024E+03	0.	14.4014684E+03	-46.4000902E-01	-14.2788476E+03	24.8139243E+00	-49.0712489E+02
13.4331966E-02	24.6947871E+04	0.	67.1405815E+03	-13.8833018E-01	-66.1208338E+03	37.4953144E+00	-14.1072509E-01
13.4331966E-02	24.6947871E+04	0.	67.1405515E+03	-13.8833028E-01	-66.1208338E+03	37.4953144E+00	-14.1072509E-01

ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSDF 2		CASE LROLL		STAGE 1		PAGE 173			
HUVP	VGPT	FTRX	FTRY	FIRZ	HA	HA	HA	DELTA	
33.6800000E-02	83.1762762E+00	44.1491595E+02	0.	-14.3301070E+03	-46.1134434E+02	0.	0.	90.1960707E-03	
99.0059402E-05	59.5503465E-04	-66.4797792E+00	0.	-67.1472631E+03	-66.2748908E+00	0.	0.	13.4331966E-02	
99.0059402E-05	59.5603465E-04	-66.4797792E+00	0.	-67.1472631E+03	-66.2748908E+00	0.	0.	13.4331966E-02	
SD2	SD1	S	S2D2	S2D1	S2	OMETD1		OMET	
-11.9963858E+00	59.8963928E-01	82.3102637E-02	0.	0.	0.	-19.2130347E+02		-21.4544500E+01	
39.1668316E-01	59.3727005E-03	14.7604381E-01	0.	0.	0.	-84.9678087E-01		-28.9646837E+01	
39.3668316E-01	59.3727005E-03	14.7604381E-01	0.	0.	0.	-84.9678087E-01		-28.9646837E+01	
FTRA	FTRD	FTRC	HTX	HTY	HTZ	FXH		FYM	
-26.9370268E+02	0.	-14.0682571E+04	0.	10.0504880E+04	0.	-26.9370268E+02		0.	
FZH	LH	HH	NH						
-14.8511332E+04	0.	10.3237483E+04	0.						
VPCS									
38.7489900E+02									
TFFS									
0.	0.								
	0.	0.	T(1)						
SAC1									
32.4655039E-03	29.0114487E-03	-11.6661575E-02	0.	0.	73.0142175E-04				
FLEX									
POINT XD1T	XD2F YD1F	XD2T YD1T	YD2F ZD1F	YD2T ZD1T	ZD2F XD0F	ZD2T YD0F	XD1F ZD0F		
10.0000000E-01	0.	-31.8627919E-01	0.	0.	94.2098128E-02	-36.4964898E+00	0.	0.	
28.9844794E+01	0.	0.	-54.5811035E-02	11.9922676E+00	0.	0.	-42.2437705E-03		
20.0000000E-01	0.	0.	0.	0.	-39.9336497E-04	-36.8099111E+00	0.	0.	
28.5432899E+01	0.	0.	-40.9808535E-02	10.7103914E+00	0.	0.	-23.3463081E-03		
30.0000000E-01	0.	0.	0.	0.	-30.1132952E-02	-33.5590340E+00	0.	0.	
28.9736658E+01	0.	0.	43.7369993E-02	44.6724726E-01	0.	0.	26.5309036E-03		
40.0000000E-01	0.	0.	-50.4619520E-02	0.	30.0652809E-02	-30.2181456E+00	0.	0.	
28.9846235E+01	0.	0.	-70.7596929E-02	-21.9237101E-01	0.	0.	-49.9495211E-03		
<p>ISS = 1 LANDING ROLL ILS = 0 IDS = 1</p>									

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LROLL STAGE 1 PAGE 174

AUTS

TI

TR

18.950000E-02 18.947500E-01

PITCH AUTOPILOT

DELQ	ALPHA	ALFND1	ALPDD1	ALPHET	DELCOE
30.6287623E-01	23.4068797E-02	18.9684351E+00	0.	23.4068797E-02	80.0900000E-01
INTEG RYN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				
INTEG RYN.	HT = 1.0000000E-03				
INTEG RTN.	HT = 1.0000000E-03				

250F

21.0425000E-01	21.0425000E-01	61.4523430E+01	0.	69.7550737E-01	28.9803104E+01	0.	34.5525434E-01
0.	18.4812946E-02	0.	25.9604850E-02	28.9823701E+01	99.8076236E+00	28.9823668E+01	0.
13.8392165E-02	68.3091758E-02	0.	-10.8662930E+00	0.	-27.3585315E-03	0.	65.5732755E-02
0.	0.	-21.7719282E-01	0.	-33.6050494E+00	12.4671000E+04	0.	0.
0.	0.						

LGAR

DELTA	P	P2	FT	SR	SF	AA	FG2
98.7389096E-03	98.8670493E+03	0.	16.0505505E+03	-18.9885149E-01	-15.9470205E+03	20.9558630E+00	-45.1153230E+02
13.4350047E-02	24.7995384E+04	0.	67.1556837E+03	-48.4679888E-01	-66.3807705E+03	28.4934121E+00	-61.6310781E-03
13.4350047E-02	24.7995384E+04	0.	67.1556837E+03	-48.4679888E-01	-66.3807705E+03	28.4934121E+00	-61.6310781E-03

HUVP	VGPT	FTRX	FTRY	FTRZ	MA	MO	DOELTA
33.6000000E-02	46.7284306E+00	-53.7267709E+02	0.	-15.9901104E+03	-50.9962577E+02	0.	98.7389096E-03
68.6025531E-06	41.2548849E-05	-46.0734947E-01	0.	-67.1600292E+03	-45.9306647E-01	0.	13.4350047E-02
68.6025531E-06	41.2548849E-05	-46.0734947E-01	0.	-67.1600292E+03	-45.9306647E-01	0.	13.4350047E-02

S02	S01	S	S202	S201	S2	OMETD1	OMET
-13.1118814E+00	57.4313668E-01	94.0466013E-02	0.	0.	0.	-21.2484407E+02	-25.4864310E+01
-85.2527966E-01	11.7827734E-03	14.7725041E-01	0.	0.	0.	-58.8854675E-02	-28.9620568E+01
-85.2527966E-01	11.7827734E-03	14.7725041E-01	0.	0.	0.	-58.8854675E-02	-28.9620568E+01

FTRA	FTRD	FTRG	MTX	MTY	MTZ	FXH	FYM
-36.6132276E+02	0.	-15.0361518E+04	0.	15.2459765E+04	0.	-36.6132276E+02	0.
FZH	LH	MH	NH				

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSDF 2 CASE LRQLL STAGE 1 PAGE 175

-15.8786078E+04 0.

15.4689198E+04 0.

VPCS

38.7489900E+02

TFFS

0.

0.

0.

0.

T(II)

SAG1

32.4686926E-03 29.8086255E-03-12.7908838E-02 0.

0.

75.6016797E-04 0.

FLEX

POINT X01T	X02F Y01F	X02T Y01T	Y02F Z01F	Y02T Z01T	Z02F X00F	Z02T Y00F	X01F Z00F
10.0000000E-01 0.	-34.5196111E-01 0.	0.	0.	0.	24.5300393E-01-36.5045950E+00 0.	0.	-52.8737759E-03
28.5812875E+00 0.	-51.1817691E-02 0.	10.8267952E+00 0.	0.	0.	40.0442350E-01-34.0673019E+00 0.	0.	-31.2744970E-03
20.0000000E-01 0.	-30.0255340E-01 0.	-36.9062254E-02 95.7004011E-01 0.	0.	0.	37.5280182E-01-37.0191445E+00 0.	0.	34.9872614E-03
28.5454650E+00 0.	-21.5836879E-01 0.	39.6210272E-02 33.2684165E-01 0.	0.	0.	49.0289439E-01-24.6459329E+00 0.	0.	-63.7351253E-03
20.0000000E-01 0.	-83.4744917E-02 0.	-65.4513425E-02-31.7527150E-01 0.	0.	0.			
28.9702460E+00 0.							
20.0000000E-01 0.							
28.5814893E+01 0.							

ISS = 1

LANCING RCLL
ILR = 1

ICS = 0

IBS = 1

AUTS

II

TR

18.9500000E-02 19.1475000E-01

PITCH AUTOPILOT

DELQX

ALPHA E

AL FHO1

ALPDD1

ALPHET

DELODE

30.6287623E-01 23.4068797E-02-10.8662930E+00 0.

23.4068797E-02 80.0000000E-01

INTEG RTN. HT * 1.0000000E-03

2SDF

21.0675000E-01 0.	21.0675000E-01 61.5247981E+01 0.	69.7516575E-01 28.9798256E+01 0.	33.1795692E-01 0.
-18.4492319E-02 0.	25.9599071E-02 28.9817250E+01 99.8031812E+00 28.9817218E+01 0.		

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

INDSOF 2 CASE LROLL STAGE 1 PAGE 176

13.4948912E-02 65.5961928E-02 0. -18.8350368E+00 0. -26.6785915E-03 0. 62.9283835E-02
0. 0. -22.2610644E-01 0. -33.5385479E+00 12.4671000E+04 0.
0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FG2
10.0053082E-02	16.1656153E+04	0.	16.3131488E+03	19.2133218E-01	16.2120061E+03	20.4742237E+00	44.5922465E+02
13.4384135E-02	24.8001022E+04	0.	67.1302277E+03	48.1766433E-01	66.2333653E+03	34.8164070E+00	33.5524644E-02
17.4384135E-02	24.8001022E+04	0.	67.1802277E+03	48.1766433E-01	66.2333653E+03	34.8164070E+00	33.5524644E-02

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	DDelta
33.6000000E-02	41.9970000E+00	54.6139357E+02	0.	-16.2541475E+03	51.7649242E+02	0.	18.0083082E-02
24.7372289E-02	14.8793682E-04	16.6194838E+00	0.	-67.1840973E+03	16.5673961E+00	0.	13.4384135E-02
24.7372289E-02	14.8793682E-04	16.6194838E+00	0.	-67.1840973E+03	16.5673961E+00	0.	13.4384135E-02

SD2	SD1	S	S2D2	S2D1	S2	QHETD1	QHET
-13.6191680E+00	57.0974600E-01	95.4782416E-02	0.	0.	0.	-21.5687184E+02	-26.0216104E+01
-21.7331681E-01	28.1638904E-04	14.7726693E-01	0.	0.	0.	-21.2402519E-01	-28.9624781E+01
-21.7331681E-01	28.1638904E-04	14.7726693E-01	0.	0.	0.	-21.2402519E-01	-28.9624781E+01

FTRA	FTRB	FTRC	HTX	HTY	HTZ	FXH	FYH
-38.4004004E+02	0.	-15.0673604E+04	0.	16.0406606E+04	0.	-38.4004004E+02	0.
FZH	LH	MH	NH				
-15.0672379E+04	0.	16.3730353E+04	0.				

VPCS

38.7489900E+02

IFFS

0. 0.

0.

0.

T(1)

SAC1

32.4694054E-03 29.9097614E-03 -12.9297512E-02 0. 0. 75.9107567E-04 0.

FLEX

POINT	X02F	X02T	Y02F	Y02T	Z02F	Z02T	X01F
XD1T	YD1F	YD1T	ZD1F	ZD1T	XD0F	YD0F	ZD0F

ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INDSO 2 CASE LROLL STAGE 1 PAGE 177

18.80000000	0.	-34.9888331E-01	0.	0.	24.1990600E-01	-36.7176720E+00	0.
28.80000000	0.	0.	-50.5692372E-02	10.6839430E+00	0.	0.	-54.1456883E-03
38.80000000	0.	-30.4054562E-01	0.	0.	41.2149001E-01	-34.0861784E+00	0.
48.80000000	0.	0.	-35.8849573E-02	94.3170673E-01	0.	0.	-32.1843903E-03
58.80000000	0.	-22.0057782E-01	0.	0.	-38.1980995E-01	-37.0031921E+00	0.
68.80000000	0.	0.	38.6691460E-02	31.8093557E-01	0.	0.	35.9658674E-03
78.80000000	0.	-89.7090109E-02	0.	0.	50.2130542E-01	-24.2742351E+00	0.
88.80000000	0.	0.	-64.2441212E-02	-32.8972980E-01	0.	0.	-65.3568100E-03

AUTS

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

18.9500000E-02 19.1725000E-01

PITCH AUTOPILOT

DELQD	ALPHA E	ALPHO1	ALPOD1	ALPHET	DELQDE
30.6287623E-01	23.4068797E-02	10.8350368E+00	0.	23.4068797E-02	80.0000000E-01

STAGE ON--INCR. DELTA1

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

INOSOF 2 CASE LROLL STAGE 1 PAGE 178

PRINT .05
AMAXER .01
DELTS .01
INOSTF 1
TRA

250F

21.0675000E-01 21.0675000E-01 61.5247981E+01 0. 59.7516575E-01 28.9798256E+01 0. 33.1795692E-01
0. -18.4492319E-02 0. 25.9599071E-02 28.9817290E+01 99.8031812E+00 28.9817218E+01 0.
13.4948912E-02 69.5961928E-02 0. -10.8350368E+00 0. -26.6789915E-03 0. 62.9283035E-02
0. 0. -22.2610644E-01 0. -33.5385479E+00 12.4671000E+04 0.
0. 0.

LGEAR

DELTA	P	P2	FT	SR	SF	AA	FC2
10.0083002E-02	10.1656153E+04	0.	16.3131485E+03	-19.2133218E-01	-16.2120061E+03	20.4742237E+00	-44.5922465E+02
13.4384135E-02	24.8001022E+04	0.	67.1802277E+03	-48.1766433E-01	-66.2333653E+03	34.8164070E+00	33.5524644E-02
13.4384135E-02	24.8001022E+04	0.	67.1802277E+03	-48.1766433E-01	-66.2333653E+03	34.8164070E+00	33.5524644E-02

HUVP	VGPT	FTRX	FTRY	FTRZ	HA	MB	DOELTA
33.5000000E-02	41.9970000E+00	-54.6139357E+02	0.	-16.2541475E+03	-51.7649242E+02	0.	10.0083082E-02
24.7372288E-02	14.8793642E-04	-16.6194838E+00	0.	-67.1840973E+03	-16.5673961E+00	0.	13.4384135E-02
24.7372288E-02	14.8793642E-04	-16.6194838E+00	0.	-67.1840973E+03	-16.5673961E+00	0.	13.4384135E-02

SD2	SD1	S	S202	S201	S2	OMET01	OMET
-13.6181680E+00	57.0974600E-01	95.4782416E-02	0.	0.	0.	-21.5687184E+02	-26.0216104E+01
-21.7331681E-01	-28.1638504E-04	14.7726693E-01	0.	0.	0.	-21.2402515E-01	-28.9624781E+01
-21.7331681E-01	-28.1638504E-04	14.7726693E-01	0.	0.	0.	-21.2402515E-01	-28.9624781E+01

FTRA	FTR0	FTRC	MTX	MTY	MTZ	FXH	FYN
-38.4004004E+02	0.	-15.0673604E+04	0.	16.0406606E+04	0.	-38.4004004E+02	0.

FZH	LH	MH	NH
-15.0672379E+04	0.	16.3730353E+04	0.

VPCS
38.7489900E+02

TFPS
0.

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM
INDSOF 2 CASE LROLL STAGE 1 PAGE 179

T(1)

SAC1

32.4694054E-03 29.9097614E-03-12.9297512E-02 0. 0. 75.9107567E-04 0.

FLEX

POINT XD1T	X02F YD1F	XD2T YD1T	Y02F Z01F	YD2T Z01T	Z02F X00F	ZD2T Y00F	X01F Z00F
10.0000000E-01 0.		-34.9888331E-01 0.	0.	0.	24.1990600E-01-36.7176720E+00 0.		-54.1456083E-03 0.
20.9808246E+01 0.		0.	-50.5692372E-02 10.6839430E+30 0.	0.	41.2149001E-01-34.0861784E+00 0.		0.
30.0000000E-01 0.		-30.4054562E-01 0.	0.	0.	0.		0.
40.9450583E+01 0.		0.	-35.8349573E-02 94.3170673E-01 0.	0.	-38.1980995E-01-37.0031921E+00 0.		-32.1843983E-03 0.
50.0000000E-01 0.		-22.0057782E-01 0.	0.	0.	0.		0.
60.9697607E+01 0.		0.	38.6691460E-02 31.8093557E-01 0.	0.	50.2130542E-01-24.2742351E+00 0.		35.9658674E-03 0.
70.0000000E-01 0.		-89.7090109E-02 0.	0.	0.	0.		0.
80.9810314E+01 0.		0.	-64.2441212E-02-32.8972980E-01 0.	0.	0.		-65.3568100E-03 0.

AUTS

ISS = 1

LANDING RCLL
ILR = 1

ICS = 0

IBS = 1

TI

TR

18.9500000E-02 19.1725000E-01

PITCH AUTOPILOT

DELON

ALPHA E

ALPHD1

ALPDD1

ALPHET

DELODE

30.6267623E-01 23.4068797E-02-10.8350368E+00 0. 23.4068797E-02 80.0000000E-01

INTEG RTN.	HT =	2.00000000E-03
INTEG RTN.	HT =	4.00000000E-03
INTEG RTN.	HT =	2.00000000E-03
INTEG RTN.	HT =	4.00000000E-03
INTEG RTN.	HT =	4.00000000E-03

2SOF

21.5675000E-01 21.5675000E-01 62.9736031E+01 0.	69.7018358E-01 28.9718678E+01 0.	64.1566597E-02 0.
0.	25.9511409E-02 28.9719388E+01 99.7358071E+00 28.9719382E+01 0.	0.
63.1051099E-03 12.6878268E-02 0.	-10.2219518E+00 0.	11.4399411E-02 0.
0.	-14.9026962E-01 0.	0.
0.	-33.7704377E+00 12.4671000E+04 0.	0.

LGEAR

I-47

ORIGINAL PAGE IS
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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY GENERALIZED COMPUTER PROGRAM

DELTA	P	INDSDF 2	CASE LROLL	STAGE 1	PAGE 180			
P2	FT	SR	SF	AA	FG2			
14.7549808E-02	21.8555862E+04	0.	26.0137060E+03	-84.0357874E-01	-26.0402750E+03	-53.7833859E-01	-26.3785748E+02	
13.1049272E-02	24.4403636E+04	0.	64.8406385E+03	-59.7437837E-01	-63.8864657E+03	35.0852115E+00	14.1194492E+02	
13.1049272E-02	24.4403636E+04	0.	64.8406385E+03	-59.7437837E-01	-63.8864657E+03	35.0852115E+00	14.1194492E+02	
HUVP	VGPT	FTRX	FTRY	FTRZ	HA	HB	ODELTA	
61.0323709E-03	36.7834593E-02	-15.8746787E+02	0.	-26.0105883E+03	-14.2932152E+02	0.	14.7549808E-02	
50.1812982E-04	30.3003565E-03	32.6679498E+01	0.	-64.8414200E+03	32.6745072E+01	0.	13.1049272E-02	
50.3812992E-04	30.3003565E-03	32.6679498E+01	0.	-64.8414200E+03	32.6745072E+01	0.	13.1049272E-02	
SD2	SD1	S	S2D2	S2D1	S2	OMETD1	OMET	
-45.9558532E+00	43.9149888E-01	12.1725279E-01	0.	0.	0.	-59.5558634E+01	-32.6196011E+01	
-40.6310273E-01	-18.2700061E-02	14.7304548E-01	0.	0.	0.	41.8903939E+00	-28.8659956E+01	
-40.6310273E-01	-18.2700061E-02	14.7304548E-01	0.	0.	0.	41.8903939E+00	-28.8659956E+01	
FTRA	FTRB	FTPC	HTX	HTY	HTZ	FXH	FYH	
-62.3265216E+01	0.	-15.5694983E+04	0.	53.9761547E+04	0.	-62.3265216E+01	0.	
FZH	LH	NH						
-15.5825061E+04	0.	54.9198671E+04	0.					
VPCS								
3A.7489900E+02								
TFFS								
0.	0.							
				T(I)				
0.	0.							
SAC1								
32.4740443E-03	31.9584782E-03	-15.5999937E-02	0.	0.	81.3424488E-04	0.		
FLEX								
POINT	X02F	X02T	Y02F	Y02T	Z02F	Z02T	X01F	
X01T	Y01F	Y01T	Z01F	Z01T	X00F	Y00F	Z00F	
10.0000000E-01	0.	-26.8621334E-01	0.	0.	52.0443808E-01	-44.5501221E+00	0.	
28.9731687E+01	0.	0.	-31.2409478E-02	77.0712491E-01	0.	0.	-75.2283216E-03	
20.0000000E-01	0.	-18.2126043E-01	0.	0.	63.7688256E-01	-40.5940384E+00	0.	
23.9394659E+01	0.	0.	-45.4585788E-03	66.6170683E-01	0.	0.	-42.8599949E-03	
30.0000000E-01	0.	-12.2857373E-01	0.	0.	-64.1191925E-01	-39.1341503E+00	0.	

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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28.8622156E+01 0. 0. 93.3717172E-03 24.4072809E-02 0. 0. 3830095E-01-13.3271829E+00 48.5894487E-03
40.0800000E-01 0. -46.7671489E-02 0. -25.7293336E-02-52.0683265E-01 0. 0. 0. -86.6326757E-03
23.9734005E+01 0.

ISS = 1 ILR = 1 LANDING ROLL ICS = 0 IBS = 1

AUTS

TI

TR

18.9500000E-02 19.6725000E-01

PITCH AUTOPILOT

DELQX ALPHAE ALPHD1 ALPOD1 ALPHET DELODE
30.6287623E-01 23.4068797E-02-10.2219518E+00 0. 23.4068797E-02 80.0000000E-01
INTEG RTN. HT = 4.00000000E-03
INTEG RTN. HT = 4.00000000E-03
INTEG RTN. HT = 4.00000000E-03 TIRE DEFLECTION EXCEEDED DELTA(1) = 1.9851551E-01

2SOF

21.7975000E-01 21.7975000E-01 63.6399140E+01 0. 69.6921565E-01 28.9679579E+01 0. -52.2063271E-02
0. -16.1657556E-02 0. 25.9476171E-02 28.9680049E+01 99.7087269E+00 28.9680049E+01 0.
17.3451870E-03-10.3258883E-02 0. -97.6940394E-01 0. -34.3054527E-04 0. -18.6690377E-02
0. 0. -19.1914853E-01 0. -34.6742941E+00 12.4671000E+04 0. 0.

LGEAR

DELTA P P2 FT SR SF AA FC2
19.8515506E-02 31.7986145E+04 0. 36.6323315E+03-20.1305943E+00-36.6393341E+03-14.1752777E-01-12.2416074E+02
12.7079334E-02 24.0289790E+04 0. 62.0851985E+03-55.2885932E-01-61.0777885E+03 37.0427561E+00 31.3247865E+02
12.7079334E-02 24.0289790E+04 0. 62.0851985E+03-55.2885932E-01-61.0777885E+03 37.0427561E+00 31.3247865E+02

MUVP VGPT FTRX FTRY FTRZ HA HB DDELTA
81.3367200E-03 48.9196841E-02-29.7997004E+02 0. -36.6374604E+03-25.3119011E+02 0. 19.8515506E-02
71.2619046E-04 43.0435137E-03 44.4288748E+01 0. -62.0845338E+03 44.6141728E+01 0. 12.7079334E-02
71.5619046E-04 43.0435137E-03 44.4288748E+01 0. -62.0845338E+03 44.6141728E+01 0. 12.7079334E-02

S02 S01 S S202 S2D1 S2 ONET01 ONET
-53.7220752E+00 29.9161937E-01 13.0307516E-01 0. 0. 0. -10.5466255E+02-33.9242808E+01
-66.0056317E-02-27.2128405E-02 14.6779439E-01 0. 0. 0. 57.1976575E+00-28.7499972E+01
-66.0056317E-02-27.2128405E-02 14.6779439E-01 0. 0. 0. 57.1976575E+00-28.7499972E+01

FTRA FTRD FTRC MIX NTY MTZ FXM FYM

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ORIGINAL PAGE IS
OF POOR QUALITY

SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
GENERALIZED COMPUTER PROGRAM

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-23.9082638E+02 0. -16.0802345E+04 0. 91.6673590E+04 0. -23.9082638E+02 0.

FZN LM MM NH

-16.0871776E+04 0. 92.7250028E+04 0.

VPCS

38.7489900E+02

TFFS

0. 0.

0.

0.

T(I)

SAC1

32.4756652E-03 31.4782995E-03-16.7418423E-02 0.

0.

83.4035137E-04 0.

FLEX

POINT
XD1T

XD2F
YD1F

XD2T
YD1T

YD2F
ZD1F

YD2T
ZD1T

ZD2F
XD0F

ZD2T
YD0F

XD1F
ZD0F

10.0000000E-01	0.	-30.2521441E-01	0.	0.	57.5920501E-01	-55.0322660E+00	0.
20.9692663E+01	0.	0.	-18.0918797E-02	61.9441236E-01	0.	0.	-80.9378365E-03
20.0000000E-01	0.	-17.1282435E-01	0.	0.	33.0058761E-01	-52.8998147E+00	0.
20.9376594E+01	0.	0.	74.5418512E-03	52.2395910E-01	0.	0.	-42.4284041E-03
30.0000000E-01	0.	-14.9072448E-01	0.	0.	-41.6198318E-01	-37.1119852E+00	0.
20.6580256E+01	0.	0.	-37.8307236E-03	-10.1878645E-01	0.	0.	49.1455111E-03
40.0000000E-01	0.	-11.0338983E-01	0.	0.	57.3910599E-01	-91.4330084E-01	0.
20.9694528E+01	0.	0.	-84.7199163E-03	-58.3370543E-01	0.	0.	-92.4719438E-03

ISS = 1

LANDING ROLL
ILR = 1

ICS = 0

IBS = 1

AUTS

TI

TR

18.9500000E-02 19.9025000E-01

PITCH AUTOPILOT

DELON

ALPHA E

ALPH01

ALP001

ALPH EY

DELQDE

30.6287623E-01 23.4068797E-02-97.6940394E-01 0.

23.4068797E-02 80.0000000E-01

ORIGINAL PAGE 18
OF POOR QUALITY

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SIX DEGREES OF FREEDOM FLIGHT PATH STUDY
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STOP